# BRICK INSTALLATION GUIDE

# **TECHNICAL INFORMATION**



### Harbison-Walker Brick Installation Guide

Please contact your Harbison-Walker Representative at any time for more specific information on the use of refractory products in your applications.

NOTE: Technical data within this brochure are subject to reasonable variations and should not be used for specification purposes. ASTM procedures, where applicable, are used for determination of data.

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**DISCLAIMER:** The information presented in this book is for general educational use only. It does not contain recommendations for any particular refractory for any particular use. It is not intended as, and should not be taken as, a warranty of any kind, including but not limited to a warranty of fitness.

**WARNING:** Some materials which are present in refractory products are harmful. One such group is classified as substances known to cause cancer to humans. Other substances may be classified as probably or possibly carcinogenic. These materials include minerals used in or formed during the manufacture of these products. The primary threat presented by many of these materials comes from inhaling respirable dust. The use of proper respiratory equipment, as well as other personal protective equipment is mandatory where required by applicable law. Please refer to the applicable Material Safety Data Sheet for such product.



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### **Out of the Fire**

The history of high heat manufacturing and refractory technology began with the discovery of fire. Nature provided the first refractories, crucibles of rock where metals were softened and shaped into primitive tools. Modern refractories are customized, high-temperature ceramics designed to withstand the destructive and extreme service conditions needed to manufacture metals, glass, cement, chemicals, petroleum and other essentials of contemporary life.

### The History of Harbison-Walker

The refractories company known as Harbison-Walker opened on March 7, 1865, as the Star Fire Brick Company. The firm was founded by J.K. Lemon, a Pittsburgh entrepreneur who hoped to build a fortune on America's growing demand for refractory brick following the Civil War.

In 1866, Lemon hired Samuel Pollock Harbison as a part-time bookkeeper. Within four years, the ambitious accountant had acquired enough stock and refractory expertise to be named General Manager of Star Fire Brick. In 1875, Harbison teamed with another stockholder, Hay Walker, to purchase the underachieving company, and renamed it Harbison-Walker.

Almost immediately, Harbison and Walker realized a major opportunity to grow their business and its reputation. Through an ongoing relationship with Thomas Carnegie, the fledging company landed a contract from Kloman, Carnegie, and Company to build the Lucy Furnace, the largest blast furnace ever designed.

The company garnered acco-

lades for the superior performance of the Lucy Furnace and began to expand rapidly, pushed in large measure by the explosive growth of the steel industry. In 1910, a 10company merger created Harbison-Walker

Refractories Company, a 33-plant operation that was the largest of its kind in the world. Harbison-Walker also thrived on its vertical structure, exerting control over every stage of its production process, through mining and raw materials

management to manufacturing, transportation and distribution.

In the decades that followed, Harbison-Walker established and fortified its position of industry leadership by building new facilities and acquiring related organizations.

- In 1916, Harbison-Walker organized the Northwest Magnesite Company near Chewelah, WA. This gave the company a secure domestic source of magnesite, a material of choice for industrial furnaces in short supply during World War I.
- In 1927, Harbison-Walker acquired majority ownership of

Northwest Magnesite, and following World War II, commissioned the company to build and operate a sea-water magnesite facility at Cape May, NJ.

- In 1945, the company purchased Canadian Refractories Limited, makers of MAGNECON, an outstanding refractory for rotary cement kilns.
- In the 1950's, Harbison-Walker built a high-quality magnesite facility at Ludington, Michigan. This keyed the development of several industry standard products, including direct-bonded magnesitechrome brick, pitch-bonded and pitch-impregnated magnesite products, and magnesitecarbon refractories.
- In 1954, Harbison-Walker became the first U.S. company to produce refractories for the basic oxygen furnace.
- In 1962, the company discovered massive deposits of high purity bauxitic kaolins at

Eufaula, AL. This permitted the company's Bessemer and Fairfield, Alabama, plants to manufacture significantly improved high-alumina brick that became a refractory of choice for much of the refractory consuming industries.

- In 1967, Harbison-Walker was purchased by Dresser Industries, prompting an accelerated diversification into non-steel related industries.
- In 1994, the company became a part of Global Industrial Technologies, a major manufacturer of technologically advanced industrial products. This development enabled Harbison-Walker to strengthen its presence in several key markets through alliances with other Global Industrial Technologies companies. They included Refractories Mexicanos (REFMEX) and **Refractorios Chileanos** (RESCA), two of Latin America's leading refractory producers; and Magnesitwerk Aken, a German refractory maker.
- In 1998, Harbison-Walker acquired A.P. Green Industries, Inc. With 22 plants in six countries, A.P. Green, a major

refractory producer in its own right, expanded considerably the global resources at Harbison-Walker's disposal.

 In 2000, RHI AG, an Austrian company with many holdings in the global refractories industry, completed its acquisition of Global Industrial Technologies, Inc., the parent company of Harbison-Walker. RHI AG subsequently combined North American Refractories Company (NARCO) and Harbison-Walker, at the time naming the resulting organization RHI Refractories America.

Today, the U.S. and export operations have been reorganized and operate independently under the name ANH Refractories. Because of the strong reputations that Harbison-Walker and NARCO established over their long histories, the companies have retained their names and are continuing to be the refractory suppliers of choice in their respective market places. Harbison-Walker continues to provide outstanding refractory materials to meet the needs of the industrial markets, while NARCO serves the needs of the steel industry.

### Harbison-Walker Today

Following World War II and the subsequent proliferation of technological advances, Harbison-Walker recognized the need for additional research capacity. In 1958, the company opened Garber Research Center, now known as the Technical Center West Mifflin. The new facility vastly enhanced Harbison-Walker's ability to test products under simulated service conditions and to conduct "post-mortem" analyses of used refractory samples.

Today, the Technical Center West Mifflin, ranks among the world's largest and most wellequipped refractory research facilities. A staff of outstanding physicists, chemists, metallurgists and engineers work closely with Harbison-Walker customers to develop new products and to solve process or production problems.

In the mid-1990s, Harbison-Walker completed a multi-milliondollar investment in the Technical Center West Mifflin aimed at providing the company's engineers and scientists with the very latest testing and analytical equipment. This commitment, made at a time when many refractory companies were diminishing their internal research capability, aggressively positioned Harbison-Walker for the new century of refractory industry leadership.

The capabilities and equipment at the Technical Center West Mifflin have been further enhanced by its additional staff and equipment acquired through its acquisition of A.P. Green and merger with NARCO.

### Application Focused Technical Marketing and Sales Support

Harbison-Walker has adopted a marketing structure that enables it to function more like a network of smaller, industry-focused companies. Throughout each of its markets, Harbison-Walker employs application focused technical marketing support, each with specific training in a particular industry or series of related industries. Individual market segments include glass, industrial metals, minerals processing and environmental, energy and chemicals markets.

Over the long term, this structure is specifically designed to promote innovation through a continuous dialogue between Harbison-Walker and the individual industries the company serves. On a daily basis, this structure allows Harbison-Walker to respond more quickly to customer requests and to serve as a reliable and ever present problemsolving partner.

Over the years, this studied, individualized approach to customer service has yielded an unending stream of innovative refractory products and application strategies for the entire range of heat-processing industries.

### **Broad Based Expertise**

Harbison-Walker's sales and technical support staff consists of chemical, ceramic, metallurgical, industrial and mechanical engineers. With strong technical educations and practical knowledge of the industries they serve, these individuals are highly skilled at working with customers to identify and select refractories that can extend service life and improve process efficiencies.

Typical consultations explore specific operating conditions in a customer's furnace and why those conditions suggest the implementation of one refractory type over another in a particular furnace zone. This process can be further aided through interactive CAD systems that allows customers to select and preview refractory linings and configurations.

Another valuable service Harbison-Walker offers is performance assessments. This process is usually aimed at identifying causes for deteriorating refractory performance resulting from changing operating conditions within a customer's plant. Most often, diagnoses are based on postmortem analyses of used refractories to determine the modes of refractory wear.

Test results may point to the adaptation of existing refractories, applying refractories in new combinations, the selection of different refractory brands or the custom design of new refractories to better meet the altered service conditions.

Helping customers understand and implement a proper refractory management strategy is the first step in an on-going relationship between Harbison-Walker and the refractory user. Sales and technical representatives are often on-site for refractory installation and furnace startup. Follow-up technical support can include orientation and training programs, troubleshooting, and service and performance assessments.

### **Quality Control**

Harbison-Walker's quality control programs encompass every facet of the organization, from the acquisition of raw materials to the packaging and shipment of the finished material.

The company operates an aggressive program of mineral land acquisition, permitting it to control a significant percentage of the raw materials it consumes. This program also helps ensure the uniform quality of raw materials while insulating the company from fluctuating supplies of key refractory minerals. Imported minerals, such as chrome ore, also are examined and tested for quality by Harbison-Walker engineers.

At the processing stage, manufacturing sites are dedicated to a single product or single class of products. This enables Harbison-Walker to maintain a high degree of chemical purity, resulting in uniform products, free of contaminants and capable of tight dimensional tolerances. In addition, each plant maintains a laboratory and a staff of quality control engineers to measure product characteristics against stated specifications.

The company also operates a centralized Quality Control Department in West Mifflin, PA., which is responsible for monitoring quality standards for all Harbison-Walker brands.

### **Industry Dialogue**

Harbison-Walker encourages a continuous dialogue among its industry "partners" by communicating continuously with contractor/ installers and soliciting regular customer input and feedback about all aspects of refractory performance.

Every year, the company brings together its engineers and select installers to disseminate technical information in an educational forum. This presents opportunities for installers to discuss their goals and expectations of refractory performance, as well as plant safety requirements.

In turn, Harbison-Walker engineers offer refractory product updates, and a comprehensive review of installation and construction techniques. This mutual information exchange leaves participants more prepared to work cooperatively throughout the year

As the refractory industry continues to evolve and expand, Harbison-Walker pledges to maintain this dialogue, seeking ways to better ways to contain the heat of industrial progress.

### Harbison-Walker Distribution Centers

Harbison-Walker offers the only nation-wide refractories and insulation distribution system. Our 26 locations continue to stock the best refractories in the industry, including fireclay and high alumina brick, mortars, plastics, and castables as well as a full line of ceramic fiber and mineral wool products. Kiln liners, anchoring systems and special shapes are also available.

### Harbison-Walker Distribution Centers

· /
(863) 669-1040
(562) 942-2151
(732) 388-8686
(215) 364-5555
(412) 741-3200
(503) 656-2854
(540) 375-2107
(801) 886-0545
(510) 236-7415
(253)872-2552
(314) 521-3314
(203) 934-7960



Visit our website at <u>www.hwr.com</u> or Call (800) 887-5555 to reach the location nearest you. For your convenience we accept, American Express, MasterCard and VISA.

### Harbison-Walker Manufacturing Facilities

As part of the ANH Refractories Family of Companies, Harbison-Walker maintains a number of manufacturing facilities. 20 ANH Refractories plants, spread across 9 U.S. states, 1 Canadian province and 4 foreign countries, manufacture Harbison-Walker brand refractory materials. Below is a list of ANH Refractories manufacturing locations:

- Acton, Ontario
- Bromborough, England
- Calle, Colombia
- Cilegon, Indonesia
- Fairfield, AL
- Fulton, MO
- Gary, IN
- Minerva, OH
- Monterrey, Mexico
- Oak Hill, OH

- Pryor, OK
- Smithville, Ontario
- Solon, OH
- South Shore, KY
- Sproul, PA
- Thomasville, GA
- Vandalia, MO
- West Mifflin, PA
- White Cloud, MI
- Windham, OH



### Harbison-Walker on the Web

Since the rise of the internet as a viable business tool, Harbison-Walker has realized the importance of providing relevant information to its customers via the World Wide Web. By accessing <u>www.hwr.com</u> users can view all of the most up-to-date Material Data Sheets, MSDS and Mixing & Using Instructions. Users may also request literature materials detailing refractory use in many of the industry's most relevant applications.



Optimum use of refractories is achieved by careful study of furnace design and evaluation of operating conditions prior to selection of refractory products which meet the design and operating requirements.

From the multiple factors listed below, it may appear that the choice of most suitable material would be exceedingly difficult. Sometimes this is true. However, there are usually data on hand from previous experience under similar conditions. Moreover, the best refractory selection often depends on a few requirements so important that other factors play a minor role. In some cases, just refractoriness alone, i.e., maximum service temperature, will be the deciding factor. In others cases high refractoriness will have to be coupled with resistance to thermal shock. Under other circumstances, resistance to metals, slags, or disintegration by reducing gases may be the governing factors. Sometimes high insulating value is desirable, but in other situations high thermal conductivity may be needed. When selecting refractories, the following major factors must be identified.

### **OPERATING FACTORS**

- Function of the furnace
- Nature of material being processed
- Rate and continuity of operation
- Range and rapidity of temperature changes
- Chemical attack by metals, slags, ash, etc.
- Fluidity of molten metal or slag
- Velocity of furnace gases
- Abrasion from contained solids or gases
- Impact from charging
- Erosion by molten furnace contents
- Impinging flames or hot spots

# FURNACE DESIGN AND CONSTRUCTION

- Type of furnace
- Design and dimensions of walls and arches
- · Loads imposed on the lining
- Conditions of heating (one or more sides)
- Amount of insulation
- Air- or water-cooling
- Type of refractory construction (brick or monoliths)
- Methods of bonding or support
- Provision for thermal expansion
- Mechanics of any moving furnace parts

### REFRACTORY-RELATED FACTORS

### Properties at room temperature –

- Workmanship and physical strength
- Density, porosity, permeability
- Chemical and mineral composition
- Uniformity
- · Size and design

### Properties at high temperatures –

- Refractoriness or maximum service temperature
- Reversible thermal expansion
- Resistance to thermal shock
- Resistance to chemical attack
- Resistance to mechanical impact or stress
- · Resistance to abrasion or erosion
- · Permeability to gases or liquids
- Volume stability (bloating or shrinkage)
- Resistance to gases and fumes
- · Thermal conductivity
- Heat capacity
- · Electrical resistance

### Economic factors –

- Delivered cost
- Cost of installation (brick vs. monoliths)
- Special shapes or forming required
- Service life

### ORDERING REFRACTORIES

Refractory technology is becoming increasingly specialized, year after year, so that it is often necessary to thoroughly understand an application area before making refractory selections. Harbison-Walker Marketing Representatives have been trained to do this work and are ready as an accommodation to discuss your application with you. Acess our website www.hwr.com for contact information.

In most cases, careful specification of your requirements and operation will help Harbison-Walker fill your order correctly and without delay. When you order various shapes and sizes, provide a complete description and correct dimensions for the shapes that you need. If you order circle brick or other shapes designed to fit a circular lining, provide both the inside and outside diameter of the lining.

Orders for brick should include enough mortar material of the right kind to lay the brick. Information required to specify the number, shape and size of brick as well as the quantity of mortar appears in the following tables and in the Brick Sizes and Shapes Section of the Handbook.

### **Special Shapes**

On initial orders for special shapes, send a drawing of the shape and the assembly into which it fits. The assembly drawing will help Harbison-Walker engineers evaluate the design and verify that the combination of refractories and design produces the best results. On subsequent orders the Harbison-Walker drawing number or your drawing and shape number will ensure that the order is properly filled. Refer to the previous order by number and date.

When filling orders for special shapes, Harbison-Walker makes a slightly larger number of shapes than specified to cover possible breakage in firing. In some cases, all of the extra pieces will come from the kilns in perfect condition. Then, Harbison-Walker will ship a limited quantity of extra pieces in accordance with the following table, unless special instructions are entered on the order. This standard procedure also helps avoid shortages resulting from breakage during transit and handling.

#### Standard Packaging

Standard packaging for monolithic refractories are 55 lb. sacks, pails, and cartons, and 2,000 lb., 3,000 lb., and 4,000 lb. bulk bags. Non standard palletizing for brick or monoliths and non standard packaging options including export palletizing are available for additional charges.

Approximate Pounds of Mortar per 1000 9-Inch Brick (9 X 4¹/₂ X 2¹/₂ Inch)*			
Mortar Materials	Brick Laid Dry and Grouted	Brick Laid with Dipped or Thinly Trowelled Joints	
Heat-Setting Mortars			
SATANITE®	250 - 300	350 - 450	
Air-Setting Mortars			
HARWACO BOND®	250 - 300	350 - 450	
'SAIRSET®	250 - 300	350 - 450	
H-W® PERIBOND™	300 - 400	500 - 600	
'SAIRBOND®	250 - 300	350 - 450	

<sup>\*</sup> This is for 9-inch straights. Normally, for larger sizes the quantities required are reduced in porportion to the decrease in surface area covered by the mortar per 1000 9-inch equivalent.

NOTE: Minimum figures are used ordinarily for estimating.

TYPICAL BRICK GROSSING CHARTS				
Quantity Specified	Overage	Quantity Specified	Overage	
1-100 101-1,000 1,001-5,000	10% 7% 3%	5,001 - 10,000 Over 10,000	2% 1%	
Note: Not less than one shape. If in sets, one complete set.				

Number of Refractory Straights Required Per Square Foot of Wall or Floor			
Wall or Floor	9 X 4 <sup>1</sup> / <sub>2</sub> X 3 Inch		
Thickness, Inches	Brick		
3	3.6		
4½	5.3		
6	7.2		
7½	8.9		
9	10.7		
12	14.2		
13½	21.4		
18	21.4		
27	32.1		

### Overview

Sound furnace refractory lining and construction — whether carried out by experienced masonry specialists working on a high production furnace or a contractor building a municipal incinerator — begins with a few fundamental ideas required to produce satisfactory performance.

### FOUNDATION

The foundation must function at the temperature produced by the furnace. For many industrial furnaces, contractors build foundations of concrete, consisting of a crushed stone aggregate, sand and binder of hydrated Portland cement. Under normal conditions, Portland cement concrete has been safely used for furnace foundations up to 700°F (371°C). When the temperature reaches 900°F (483°C), dehydration of the cement reaches a point where the concrete retains little mechanical strength.

Ordinary aggregates include quartz pebbles, silica gravel, crushed silica rock and/or crushed limestone. An aggregate of silica rock in any form will expand sufficiently at temperatures up to 1,000°F (538°C) to set up stresses in the concrete and weaken the foundation. Limestone or dolomite rock in an aggregate will calcine at somewhat higher temperatures and weaken considerably. For temperatures above 700°F (371°C), good practice points to the choice of a castable refractory for the foundation. Calcined fireclay, in sizes up to 1 inch, can be substituted for conventional aggregate. Its thermal expansion is low, and it will not shrink at the highest temperature to which concrete can be subjected.

High temperature furnace operation also calls for ventilation in the lower courses of brickwork or the upper part of the foundation. Good furnace design often requires placement of the furnace on plates, girders or low brick piers, so that air circulates under the vessel. Sometimes, cross flues are formed in the top of the concrete foundation. At others, pipes, 3 inches in diameter or larger, are embedded in the foundation.

Building furnaces is a specialized branch of masonry, best placed in the

hands of bricklayers experienced in furnace construction. Walls, arches and other furnace details should be designed and constructed to assure structural stability. Otherwise, a return on your refractory investment may not be realized.

### WALL CONSTRUCTION

Courses of brick laid in a wall so that the lengths parallel the face of the wall are called stretchers. Brick with lengths running at right angles to the face are headers. In soldier courses, the brick stand on end, and in row-lock courses, they lie on one edge (See illustration, p. 11).

Header courses tend to spall less than stretchers at the hot face of a furnace wall because they expose a smaller area to high temperature. However, stretcher courses expose fewer joints than headers, and this provides an advantage in applications where joints tend to wear more rapidly than brick.

Bonding, or tightening construction through combinations of headers and stretchers and off-setting vertical joints, strengthens and stabilizes furnace walls. The type of bond selected for any particular furnace will depend upon the design of the furnace, thickness of the walls, the need for gastight construction, severity of operating conditions and the need for easy maintenance.

In any case, the wall should be bonded so that loads will be transferred to the cooler part of the wall when the inner, hotter portion loses its ability to carry them. Walls must be designed to carry structural loads at high temperatures.

Stretcher walls — one brick thick — usually have the least structural stability, but they are sometimes used in smaller furnaces and in furnaces where heat must pass through the walls. Double tongue and groove brick provide stability for thin walls.

Alternate header and stretcher courses probably provide the most common arrangement for standard industrial furnaces. Large 9-inch brick break joints, start ends of walls and turn corners.

Courses consisting mostly of headers are often used advantageously in 9 and 13<sup>1</sup>/<sub>2</sub>-inch walls subject to high temperatures, heavy loads and slag attack. This construction is usually preferred for basic brick walls. The bond provides stability and easy replacement, but most expansion joints pass entirely through 9-inch walls.

Courses consisting mainly or entirely of headers on the inner face and mainly stretchers on the cold face are sometimes considered desirable when spalling conditions are severe. Three or four stretcher courses to one header provide a wall to which a 4½-inch skin wall can be tied for repairs. However, it should not be used where stretcher courses may fall into the furnace.

In composite wall construction consisting of two or more kinds of brick in inner and outer courses, the courses are sometimes tied together. Usually, the more refractory brick go into the interlocking courses.

However, when brick have marked differences in rates of thermal expansion, the backup courses should not be tied to the inner courses. This is especially true when the temperature gradient through the wall makes a significant difference in total expansion.

The number of refractory straights required to build a simple wall can be determined from the chart on p.12. Multiply brick per square foot from the appropriate row, depending on wall thickness, by the area of the wall to provide the brick count. For walls not of simple rectangular shapes, determine the volume in cubic feet from the appropriate formula on this page and multiply by the number of brick per cubic foot.

Wall thickness must bear some relation to height and unsupported

### BONDING OF WALLS BUILT WITH RECTANGULAR BRICK



length. In unsupported straight walls, a  $4\frac{1}{2}$ -inch thickness will carry heights up to 3 feet; 9 inches will carry heights of 3 to 8 feet;  $13\frac{1}{2}$  inches, 8 to 12 feet; and 18 inches, walls higher than 12 feet.

Walls with unsupported length more than one and one half times their heights should be somewhat thicker, and thermal spalling conditions may indicate additional thickness. Walls of cylindrical furnaces and stacks, with adequate backing, may be somewhat thinner for a given height than straight walls.

Cylindrical walls, arches and domes are built with brick tapered to turn circles. Arch brick slope from edge to edge so that the length of the brick parallels the furnace wall like a stretcher, while the wedge tapers from end to end so that it faces into the furnace like a header. A  $9 \times 4\frac{1}{2} \times 2\frac{1}{2}$ -inch arch brick makes a  $4\frac{1}{2}$ -inch lining, while the same wedge shape makes a 9-inch lining. In basic brick, key brick shapes may also taper along the edges. Combinations of these shapes taper in two dimensions to turn domes.

### JOINT CONSIDERATIONS

In many cases, brick sizes and shapes or the type of bond will be chosen to minimize the number of joints in the lining. Monoliths — not without construction or thermal expansion joints – present the fewest joints and opportunities for penetration by metal, slag or furnace gases.

Ramming mixes or castable refractory materials are often used to fill places where brick would be cut to fit. For example, ramming mixes or dry refractory materials can be used to protect the toe of the skewback (See discussion of Arch Construction, UR - 22). On many installations, the irregular space between electric furnace roof brick and electrode ports is filled with ramming mix or castable refractories.

The thickness of joints between refractory brick depends on the brick, the mortar, the need for preventing gas leakage or slag penetration, and the requirements for thermal expansion. When there is no need for an especially strong bond, the brick are laid without mortar. In some cases, the fusion that takes place on the hot face will provide the bond required. Generally, however, the use of mortar is desirable to level courses and to provide smooth bedding for the brick.

Brickwork laid with heat-setting mortars should have thin joints, either dipped or poured. The brick should be rubbed or tapped into place to produce as much brick-to-brick contact as possible. Joints made with an air-setting mortar generally can be somewhat thicker, but such joints should be completely filled.

In furnace construction, proper allowance must be made for thermal expansion. Usually, vertical expansion allowances permit walls to move freely upward and horizontal expansion allowances appear at joints in the brick.

### HEARTHS

The construction of furnace hearths presents special problems. Some furnace bottoms must withstand impact and abrasion from a charge of scrap metal. Liquid pressure may tend to float brick. Many hearths must resist penetration by metal or slag accompanied by corrosion or erosion.

Furnace hearths, in many cases, are built of refractory brick, usually seated on a monolithic refractory bed. Others have sub-bottoms built of brick with working hearths composed of monolithic refractories, such as dead-burned magnesite or a ramming mix.

Construction details, as well as the refractories themselves, depend on applications. Even different furnaces within the same application area may perform more efficiently with a different refractory design.

Sophisticated applications for refractories call for specialists in refractories design. A number of engineering firms specialize in high temperature process design, and many contractor/installer organizations concentrate on refractory construction.

Harbison-Walker maintains close contact with these organizations, lending its engineering skills and applications know-how to the search for solutions to any problem involving the use of refractories.

Number of Refractory Straights Required Per Square Foot of Wall or Floor			
Thickness,	9 x 4½ x 3" Brick		
Inches			
3	3.6		
41⁄2	5.3		
6	7.2		
7½	8.9		
9	10.7		
12	14.2		
13½	16.0		
18	21.4		
27	32.1		

Rammed plastic refractories used for arch construction minimize the number of joints.



### Overview

Arches form the roofs of most furnaces, combustion chambers and flues. Providing the standard solution to the problem of spanning the high temperature process with refractories. In some application, arches span wall openings, and sometimes they carry the weight of walls or checkerwork. Most arches are built of brick, but monolithic materials are gaining popularity throughout the industry.

### **TYPES OF ARCHES**

### **Sprung Arches**

In a true arch, the design of the whole determines the shape of each block or structural unit. Theoretically, each joint is a small piece of the radius of the circle of which the arch is a segment. Each end of the arch rests on a skewback. The arch becomes self-supporting after all of the pieces go into place, but it must be supported until the final, center shapes the keys go into place. When it is complete, the arch springs from the sloping faces of the skewback shapes. The skewbacks cut off the arc of the circle on the outside radii of the arc.

The sprung arch exerts a downward vertical force and an outward horizontal force on the skewbacks, essentially a distribution of its weight. The vertical force may be carried by steel beams or by the furnace walls or a combination of walls and steel buttresses. The horizontal thrust of a roof arch travels through the skewbacks to a steel supporting system known as the binding which is composed of beams and tie rods. The tie rods, usually above the furnace, link one side of the furnace to the other, and balance opposing forces, one against the other.

In traditional furnace design, the binding consists of:

- 1. Horizontal buttress beams running lengthwise to the furnace in contact with the skewbacks where possible;
- 2. Vertical beams, or backstays, spaced at intervals along the concrete; and
- 3. Horizontal tie rods, I-beams, or channels extending across the furnace above the roof to connect the upper ends of opposite buckstays.

### **Ring Arches**

In ring arches, each course of brick forms a separate ring running across the roof and the joints are continuous across the roof. Ring arches require somewhat less labor for initial construction. Cold repairs are easier to make and they offer better resistance to spalling. However, ring arches require support at the end of the furnace to forestall outward displacement.

In bonded construction, all joints are broken and the rings help bond one another in a stronger construction. Bonded roofs are better adapted for hot repairs but they demand more skill of the brick masons and more uniformity in the brick.

Sometimes, furnace designers strengthen ring arch roofs by using a longer brick in every third or fourth ring. This construction creates ribs across the roof, which remain strong when the thinner parts of the roof wear away. The strength of the ribs also helps when roofs must be patched.

### **Suspended Arches**

In suspended arches, a steel superstructure helps carry the weight of the roof, otherwise distributed through the arch to the walls and binding. Suspended arches are often used with dense, heavy basic brick. Harbison-Walker has basic brick brands to provide a method for attaching the brick to an overhead steel superstructure.

In suspended construction, refractories carry smaller loads and therefore, suffer less deformation at high temperatures than they otherwise might. Using suspended construction, it is also easier to make allowance for thermal expansion to avoid thermal stresses and pinch spalling.

### **Monolithic Arches**

Monolithic arches–cast over forms much like those required for brick arches–have replaced brick in some applications. Skews may be eliminated in monolithic arches, but design considerations remain the same as those for brick arches. A monolithic arch provides all of the advantages monolithic construction, including reduced cost and downtime.

### **ARCH GEOMETRY**

Arch geometry determines all design characteristics. From the viewpoint of arch design, the outside and inside arcs, or surfaces of the roof, are segments of concentric circles separated by the thickness of the roof. The skewback slope cuts the arc, and its angular value equals half the included central angle of the arch. The rise of the arch measures the distance from the inner chord - equal to the span and cutting the inside arc to the center of the roof at midspan.



Hypothetical position of thurst in a simple sprung arch, when the bricks are in full contact at joints.



When span, thickness and rise are established, all other dimensions can be calculated using the formulas in this section.

The stability of any arch will depend on its rise, thickness and weight, as well as the thermal properties of the refractories. Hot strength and thermal expansion are particularly important. Good arch design must take these factors into consideration.

Rise is normally expressed in inches per foot of span, or in terms of the central angle. They are directly related. It should be easy to visualize a larger angle including a higher rise and a shorter radius. On the other hand, the flatter roof with a smaller rise indicates a smaller included central angle and a longer radius.

Experiences suggests that a simple roof arch should rise not less than one nor more than three inches per foot of span. For any particular furnace, the rise selected should depend on operating conditions, chiefly temperature, thermal cycling and the refractories used.

Typically, stable fireclay arches rise from  $1^{1/2}$  to three inches per foot of span. High temperatures and soaking heat call



for higher values. Silica roofs made with brick that maintain dimensional stability and hot strength almost to their melting point, normally rise from one to two inches per foot.

High-alumina refractories used in arch construction call for at least 1.608 inch per rise per foot of span. Basic refractories need 2<sup>1</sup>/<sub>4</sub> to three inches of rise in sprung arches. Insulating firebrick, which give up hot strength in exchange for low thermal conductivity, call for two to three inches of rise per foot of span.

For many applications, a 1.608 inch rise, about 1<sup>5</sup>/s-inch, is a logical standard in that it meets normal requirements for strength and stability. The 60° central angle equals one sixth of a circle and the span equals the inside radius, so the number of brick required to build the roof is easy to calculate.

The reaction of refractory brick to furnace operation, i.e., heat-up, establishes the practical limit for roof rise. Operation and thermal expansion tend to push the brick upward, opening joints at the top and pinching brick at the bottom. Brick that soften at operating temperatures may become permanently deformed, shortening the radius of the arc and increasing the rise.

As the arch rises on heat-up, the line of thrust, the line of force along which the arch distributes the vertical and horizontal elements of its weight, shifts downward. As the line of thrust approaches a horizontal position in the arch, the horizontal force approaches its maximum value.

In some furnaces allowance for thermal expansion of the brick will limit upward movement of the arch. Steel casings can provide an allowance for expansion. Paperboard placed between brick will burn out and make room for expansion. In some cases, horizontal tie rods arc spring loaded or manually adjusted to permit thermal expansion of the refractories.

Without adequate provision for thermal expansion, the relationship between arch thickness and rise\* of the cold arch must be such that the line of thrust does not drop out of the arch when it is heated. If it does, the arch will not be stable.

The line of thrust in a cold arch should lie within the middle third of the brick. Generally, selecting the proper combination of brick shapes and doing a professional job to assure face-to-face contact between brick will keep the thrust where it belongs.

In practical construction problems, the vertical and horizontal components are more important than the resultant force. The walls, with or without steel supports, must carry the vertical force, and the horizontal binding, including buckstays and tie rods, must contain the horizontal force.

\* Assuming that the absolute lower limit for the rise of the line of thrust is  $^{1}/_{4}$  inch ( $^{1}/_{48}$ ) per foot of span, the rise (h) must exceed thickness (T) times the of the cosine of the central angle ( $\theta$ )plus  $^{1}/_{48}$ span (S). This implies that T should not exceed:

 $\frac{h^{-1/48}S}{Cosine \theta/2}$ 

For a more complete discussion of arch stresses see: J. Spotts Mcdowell, "Sprung-Arch Roots for High Temperature furnaces," Blast Furnace and Steel Plant, September 1939.

Arch Constants for Given Rises per Foot of Span

## ARCH CONSTRUCTION CALCULATIONS

The brick count for many sizes can be calculated from the tables of brick combinations for rings, since simple sprung arches are segments of circles.

Calculation of arch parameters, the arch numbers, is sometimes lengthy, but not difficult, especially when carried out with a pocket calculator. Equations required to produce the necessary values are included in this section.

Suppose that a furnace design calls for an arch with a 12 foot span,  $13^{1/2}$  inches thick built of NARMAG<sup>®</sup> 60DB brand brick, on a furnace 20 feet long. NARMAG<sup>®</sup> 60DB basic brick, requires a minimum rise of  $2^{1/4}$  inches per foot of span.

The table of Arch Constants below provides data to develop the required design values. For a  $2^{1/4}$  inch rise, multiply the span by 0.76042 to determine the inside radius, in this case, 9.125 or 9 feet,  $1^{1/2}$  inches. That means the arch is a segment of a circle with an 18 foot, three inch inside diameter, twice the inside radius.

The table also indicates that the central angle for this arch will be  $82^{\circ}$  13.4', equal to 2,284 ten thousandths of a circle.



On page IR - 45 the tables of brick combinations for rings for 13½ inch linings show that an 18 foot, 3 inch ring can be built with:

82 pieces, No. 2 Wedge and 176 pieces, No. 1 Wedge

If this design calls for 2,284 ten thousandths of a ring, then:  $0.2284 \times 82 = 18.73$  or 19 pieces, No. 2 Wedge  $0.2284 \times 176 = 40.2$  or 41 pieces, No. 1 Wedge

If the design specifies  $13\frac{1}{2} \ge 6 \ge 3$  inch shapes, then two rings will cover a running foot on the 20 foot roof, and 40 rings will roof the furnace. Thus, the design calls for 40 times 19, a total of 760 pieces, No. 2 Wedge, and 40 times 41, a total of 1,640 pieces, No. 1 Wedge.

#### Central Angle $\boldsymbol{\theta}$ Difference Rise Skewback Inside Inches Inside Retween v F Per Foot Radius Degress Part of Arc Outside & н of Span (r) Circle Inside Arc (a<sub>a</sub>) (d) $(A_a \cdot a_a)$ (1)(2) (3) (4)(5)(6)(7)(8) (9) 1.54167S 37° 50.9' 0.10514 1.01840S 0.66059T 0.32432T 0.94595T 0.34286Q 1 1<sup>1</sup>/4 1.25208S 47° 4.4' 0.13076 1.02868S 0.82157T 0.39933T 0.91681T 0.43557Q 1<sup>1</sup>/2 1.06250S 56° 8.7' 0.15596 1.04117S 0.97992T 0.47059T 0.88235T 0.53333Q 1.608 1.00000S 60° 0.0' 0.16667 1.04720S 1.04720T 0.50000T 0.86603T 0.57735Q 1<sup>3</sup>/<sub>4</sub> 0.93006S 65° 2.5' 0.18067 1.05579S 1.13519T 0.53760T 0.84320T 0.63757Q 2 0.83333S 73° 44.4' 0.20483 1.07251S 1.28701T 0.60000T 0.80000T 0.75000Q 21/4 82° 13 4' 0 760425 0 22840 1.09125S 0.65753T 0.75342T 0.87273Q 1.43507T 2.302 0.74742S 83° 58.5' 0.23326 1.09544S 1.46563T 0.66896T 0.74329T 0.9000Q 90° 28.8' 21/2 0.70417S 0.25133 1.11200S 1.57918T 0.71006T 0.70414T 1.00840Q 2<sup>3</sup>/<sub>4</sub> 0.66004S 98° 29.7 0.27360 1.13464S 1.71906T 0.75753T 0.65280T 1.160444Q 1.15912S 0.80000T 1.333334Q 3 0.62500S 106° 15.6 0.29517 1.85459T 0.60000T

NOTE: The factors in the above tables are the following functions of  $\theta$ : Column 2, 1/2 cosecant 1/2 $\theta$ ; column 4, Ø divided by 360°; column 5; 1/2 cosecant 1/2 $\theta$ 

### SKEWBACK DESIGN

Skewbacks may be built-up combinations of rectangular brick sizes, as previously illustrated, or one-piece special skews designed to fit the arch. Built-up skews satisfy the requirements of narrow spans, four feet or less, but the one-piece skewback generally provides greater strength and better support at the buttress.

The slope of the skewback must be designed to match the central angle of the arch, determined by the rise and span. When the skewback is carried on a channel or angle, the line of thrust should pass through, or slightly above, the corner of the supporting steel.

Skewback dimensions can be determined from the table of Arch Constants below. From the example above, a  $2\frac{1}{4}$  inch rise produces a central angle of  $82^{\circ}$  13.4'. The slope equals half the central angle, amounting to  $41^{\circ}$  6.6' in this example. Other dimensions can be calculated from constants in the same table.

The V dimension is 0.75342 times the thickness of an arch with a 2<sup>1</sup>/<sub>4</sub> inch rise. In this example above, 0.75342 times 13.5 equals approximately 10.17 inches. Other skewback dimensions can be determined in the same way.

The amount of stress in a furnace can be only approximated because of the following variables: (1) the exact position of the line of thrust, even when the arch is cold, is not known, (2) workmanship in construction of the arch may be less than perfect, (3) the position of the line of thrust will change when the furnace is heated, (4) tie rods can stretch and the furnace can settle, changing arch parameters, and (5) arch stresses can be increased by the weight of material adhering to, or absorbed by the bricks. The force acting against the skewbacks depends primarily on the span, rise and thickness of the arch, the weight of the brick, and conditions in the furnace. Vertical force equals one half the weight of the arch per running foot.

The horizontal force depends on the weight of the arch and on the span and rise.

The resultant thrust (F) acting at the skewback equals the square root of the sum of the squares of horizontal (H) and vertical (W) forces, that is:

### $F = \sqrt{H^2 + (W/2)^2}$

However, the stresses of a cold arch, in which all adjoining brick are in full contact, can be approximately determined from the table below. The limiting value which the horizontal thrust approaches in a heated arch,  $H_{max}$ , can be calculated approximately from the constants in the table of Maximum Values on the following page. Consider the NARMAG<sup>®</sup> 60DB brick arch design described earlier in this chapter. Its design parameters are:

Span (S) = 12 ft Thickness (T)= 1.125 ft Inside Radius (r) = 9.125 ft Density of NARMAG<sup>®</sup> 60DB (D) = 192 lb/ft<sup>3</sup> Rise (h) = 2.25 inches per foot of span=12 x 2.25 = 27 inches=2.25 ft Outside radius (R+T) = 10.25 ft

Central Angle ( $\Theta$ ) = 82°13.4'

The following calculations are based on the assumption that the line of thrust passes from the center of arch thickness at midspan to the center of arch thickness at the skewbacks.

As shown in the table below, the weight of the arch equals 1.17 DST. That is, for this arch, 1.17 times 192 times 12 times 1.125 equals 3032.64 pounds per foot of arch length. Since W/2 equals 1516.32, the vertical force that the walls and buttresses must carry amounts to 1516.32 pounds per foot of arch length.

From the same table, the horizontal thrust of cold arch with a 2<sup>1</sup>/<sub>4</sub> inch rise per foot of span equals 0.64 time its weight (W). For the arch under consideration, 0.64 times 3032.64 equals 1940.89 pounds per foot of arch length.

Pise in			Forces Per Foot of Arch Len	gth
Inches Per Foot of Span	Central Angle ( <del>0</del> )	W Weight	H Horizonal Thrust	F Resultant Thrust at Skewback
1	37° 50.9'	1.05 DST	1.49 W	1.57 W
1 <sup>1</sup> / <sub>4</sub>	47° 4.4'	1.07 DST	1.18 W	1.28 W
1 <sup>1</sup> / <sub>2</sub>	56° 8.7'	1.09 DST	0.98 W	1.10 W
1.608	60° 0.0'	1.10 DST	0.91 W	1.04 W
1 <sup>3</sup> / <sub>4</sub>	65° 2.5'	1.11 DST	0.83 W	0.97 W
2	73° 44.4'	1.14 DST	0.72 W	0.88 W
2 <sup>1</sup> / <sub>4</sub>	82° 13.4'	1.17 DST	0.64 W	0.81 W
2.302	83° 58.5'	1.17 DST	0.62 W	0.80 W
2 <sup>1</sup> / <sub>2</sub>	90° 28.8'	1.19 DST	0.57 W	0.76 W
2 <sup>3</sup> / <sub>4</sub>	98° 29.7'	1.22 DST	0.51 W	0.71 W
3	106° 15.6'	1.25 DST	0.46 W	0.68 W

#### **Constants for Calculation of Stresses in Unheated Arches**

D= Density of brick in pounds per cubic foot. S=Span in feet. T=Thickness of arch in feet. W=Weight of brick per foot of arch length. The constants given in this table are based on the assumption that the line of thrust passes from the center of the arch thickness at the point of midspan, to the center of arch thickness at the skewbacks.

The resultant force, also determined from the table above, is 0.81 times 3032.64 equals 2546.44 pounds per foot of arch length.

Maximum values approached by horizontal thrust can be determined from the factors listed in the table. These data indicate that the maximum value approached by horizontal thrust for a heated arch free to rise can be determined by multiplying the cold arch horizontal thrust by a factor dependent on the ratio of thickness to span. In the example considered earlier, thickness equals 9% of span, that is, 1.125/12 equals 0.09. For a  $2\frac{1}{4}$  inch rise, maximum thrust approaches 1.84H, or 1.84 times 1940.89 equals 3571.24 pounds per foot of arch length. This value is an approximation, but it lies well within the requirements of practical furnace design.

The safety factor used in furnace binding design is ordinarily higher than that used in conventional steel structural design because the furnace binding may become overheated. For ordinary structural steel bindings, many furnace designers limit tensile stress to 12,000 pounds per square inch.

### COMPLEX REFRACTORY DESIGN PROBLEMS

Customers who design or build refractory structures often tap Harbison-Walker resources, e.g., engineering skills and advanced refractories technology, for solutions to complex problems involving refractory applications. Harbison- Walker engineers have developed computer programs, which are used with customers, that can produce complex arch or dome design parameters in a few minutes, often saving many man-hours of calculation. For assistance with your difficult design problems, please call your Harbison-Walker representative.

#### **Initial Heat-Up Considerations**

In most cases, a new furnace should be heated slowly with enough air circulating over the walls to remove moisture. Steam trapped in the pores of brick or mortar may damage the brickwork. Good practice permits a furnace to dry out thoroughly at a temperature not over 250°F(121°C) for 24 hours or longer, depending on the size of the vessel and the refractories in use. Temperatures above 400°F to 600°F (205°C to 316°C) should be avoided until all steaming ceases.

Furnace builders and refractory consumers should understand the requirements of the brands that line their furnaces. Careful drying of linings built of magnesia and some of its compounds is especially important. Water vapor or steam under pressure can cause hydration of the magnesia.

Flame impingement on brickwork during heat-up can cause rapid, localized expansion with consequent spalling. Silica and basic brick, especially, tend to spall when subjected to excessively rapid changes in temperature.

In low temperature furnaces, it is often good practice to heat the refractories to a higher temperature than that required for operation for a short period of time. This preliminary heat-up develops the ceramic bond in mortared joints and increases their mechanical strength.

#### Hmax Per Foot of Arch Length Thickness of Arch in Precent of Span Inches Per Foot Central of Span Angle (O) 4% 5% 6% 7% 8% 9% 10% 37° 50.9' 1.88 H\* 2.41 H 3.29 H 5.0 H \*\* 1 \*\* **1**<sup>1</sup>/<sub>4</sub> 47° 4.4' 1.61 H 1.86 H 2.29 H 2.80 H 3.73 H 5.34 H 56° 8.7' 1.47 H 1.63 H 1.94 H 2.14 H 2.55 H 3.88 H 11/2 3.06 H 1.608 60° 0.0' 1.43 H 1.59 H 1.79 H 1.98 H 2.31 H 2.75 H 3.30 H **1**<sup>3</sup>/<sub>4</sub> 65° 2.5' 1.39 H 1.52 H 1.67 H 1.93 H 2.17 H 2.41 H 2.77 H 2 73° 44.4' 1.33 H 1.43 H 1.56 H 1.69 H 1.86 H 2.04 H 2.22 H 2<sup>1</sup>/<sub>4</sub> 82°13.4' 1.29 H 1.38 H 1.47 H 1.58 H 1.70 H 2.00 H 1.84 H 1.95 H 2.302 83° 58.5' 1.28 H 1.37 H 1.46 H 1.57 H 1.69 H 1.81 H 2<sup>1</sup>/<sub>2</sub> 90° 28.8' 1.26 H 1.33 H 1.42 H 1.51 H 1.60 H 1.72 H 1.82 H 98° 29.7' **2**<sup>3</sup>/<sub>4</sub> 1.53 H 1.73 H 1.24 H 1.29 H 1.37 H 1.45 H 1.63 H

1.33 H

1.41 H

1.48 H

1.57 H

1.63 H

### Maximum Value Approached by Horizonal Thrust in Heated Arch Free to Rise

1.26 H

\* H = Horizonal thrust, as determined from the previous table.

106° 15.6'

\*\* Stress excessive.

3

1.22 H

### REFRACTORY CONSTRUCTION CALCULATIONS

Calculations to determine the dimensions or numerical characteristics of refractory structures are not difficult. Generally, they involve three steps: (1) pick out the formula that produces the dimension or other number that you need; (2) substitute the numbers in your problem that fit the letter-variables in the formula; and (3) perform the arithmetic operations required by the formula. Remember, once the span and rise of an arch are decided, all other dimensions follow.

To use these formulas, all the algebra you need to know is that parentheses tell you to perform the arithmetic operation inside before carrying out the other operations.

All you have to know about trigonometry is that each sine, cosine or tangent is a *particular number* associated with one *particular angle*, and that an arcsine, arccosine or arctangent is a particular *angle* associated with a particular number. That allows you to go from number to angle, or from angle to number, or back and forth, depending on the requirements of the problem. Sines, cosines or tangents are found in tables of trigonometric functions or in pocket calculators.



### Arches

Many pocket calculators will make calculation of arch parameters, i.e. numerical characteristics such as dimensions, quick and easy. Sine, cosine and tangent values are literally at your fingertips on many models. Solutions to arch problems involve nothing more than substituting numbers into the formulas and pushing buttons on the calculator. For example in the design previously specified:

Sine  $\frac{1}{20} = \frac{S}{2r} = 12 (2 \times 9.125)$ = 0.6575 Arcsine 0.6575 = 41.11° =  $\frac{1}{2}$  The Central Angle The Central Angle = 82.22° = 82° 13'

The problem is no more difficult with paper, pencil and a table of trigonometric functions, but the multiplication, division and reference to the table take more time.

### **Arch Formulas**

- 1.  $r = S^2/8h + h/2$
- $2. \quad R = r + T$
- 3.  $h = r \sqrt{r^2 (S/2)^2}$
- 4. Sine  $\frac{1}{2}\theta = S/2r$
- 5. Tan  $\frac{1}{4}\theta = 2h/S$
- 6. Tan  $\frac{1}{4}\theta = d/6$
- 7. Part of circle =  $\theta/360^\circ$
- 8.  $H = T \operatorname{Sine} \frac{1}{2} \theta$
- 9.  $d = 6 \operatorname{Tan} \frac{1}{4} \theta$
- 10.  $a_a = 6.2832r (\theta/360^\circ)$
- 11.  $A_a = 6.2832 R (6/360^\circ)$
- 12. V=T Cos<sup>1</sup>/<sub>2</sub>θ
- 13. P=QTan  $\frac{1}{2}\theta$

#### Arch Symbols

The following symbols and variables are used in the arch formulas:

- $a_a$  = Length of inside arc
- $A_a =$  Length of outside arc
- R = Outside radius of arch
- r = Inside radius of arch
- S = Span of arch
- d = Rise in inches per foot of span
- h = Total rise of arch
- T = Thickness of arch
- $\theta$  = Central Angle (Theta)
- H, V, P, Q = Skewback dimensions indicated in the Arch Constants table.

### Rings

The number of brick of two sizes to form a ring can be calculated from formulas listed below. When one brick, E, is a straight, and the other, F, is a radial, use Formulas 1-a, 1-b and 1-c. When both brick, E and F, are radial with outside chord dimensions and inside chord dimensions unequal, use Formulas 2-a, 2-b, and 2-c. When both brick, E and F. are radial and the inside and outside chord dimensions of E differ from those of F, use Formulas 3-a, 3-b and 3-c for a single combination, and 4-a, 4-b, and 4-c for a series of combinations.

### **Ring Formulas**

- (1-a)  $N_{f} = \frac{2\pi T}{C_{f}-C_{f}}$
- (2-a) N<sub>t</sub> =  $\frac{\pi D_g}{C_e} = \frac{\pi D_g}{C_f}$
- (3-a)  $N_{e}C_{e} + N_{f}C_{f} = \pi D_{g}$
- (4-a)  $N_{e} = \frac{N_{x}}{D_{e} D_{f}} (D_{g} D_{f})$
- (1-b)  $N_{e} = \frac{\pi D_{g} N_{f}C_{f}}{C_{e}}$
- (2-b)  $N_{e} = \frac{\pi D_{g} N_{f} C_{f}}{C_{e} C_{f}}$
- (3-b)  $N_{e}c_{e}+N_{f}c_{f} = \pi d_{g}$
- (4-b)  $N_{f} = \frac{N_{v}}{D_{e}-D_{f}} (D_{e}-D_{g})$
- (1-c)  $N_t = N_e + N_f$
- (2-c)  $N_{f} = N_{t} N_{e}$
- (3-c)  $N_t = N_e + N_f$
- (4-c)  $N_t = N_e + N_f$



### **Ring Symbols**

- E = Either a straight brick or a radial brick used with a companion brickF; when brick E is radial it turns a larger diameter than brick F.
- F = A radial brick, used with a companion brick E which may be either straight or radial; in the latter case, brick F turns a smaller diameter than brick E.
- T = Radial dimension common to both brick E and F.
- D<sub>e</sub> = Outside diameter of ring formed by brick E.
- $D_f = Outside diameter of ring formed by brick F.$

 $D_g = A$  given outside diameter larger than  $D_{f}$ , if brick E is radial  $D_g$  must lie between  $D_e$  and  $D_{f}$ .

- $d_g = A$  given inside diameter.
- $C_e^{=}$  Outside chord dimension of brick E.

- $C_f = Outside chord dimension of brick F.$
- $c_e =$  Inside chord dimension of brick E.
- $c_f =$  Inside chord dimension of brick F.
- N<sub>e</sub>=Number of pieces of brick E, when used in combination with brick F, to form a ring having a given outside diameter D<sub>e</sub>.
- N<sub>f</sub>=Number of pieces of brick F, when used in combination with brick E, to form a ring having a given out side diameter D<sub>e</sub>.
- N<sub>t</sub>=Total number of pieces of brick E and F used in combination to form a ring having a given outside diameter D<sub>a</sub>.
- $N_x$ =Number of pieces of brick E required to form a complete ring having an outside diameter  $D_e$ .
- $N_y$ =Number of pieces of brick F required to form a complete ring having an outside diameter  $D_r$ .

Wherever furnace construction and operating conditions permit, refractory linings are typically constructed with brick of standard sizes and shapes. Standard materials cost less than larger, more intricate shapes and frequently are more serviceable. They are also more accessible, in that they are likely to be routinely stocked by the manufacturer.

The most widely used standard size for all types of refractory brick is 9 x  $4^{1/2}$  by 3 inches. Most brands offer larger sizes, as well. Special shapes, such as skewback brick, are important in the construction of numerous kinds of furnaces having sprung arches.

This section provides a comprehensive listing of standard brick sizes and shapes for a variety of furnace applications, as well as ring and arch combinations for standard size refractory brick. Additional sections address special shapes such as semi-universal ladle brick, brick counts for rotary kilns and rotary kiln brick shapes, including ISO, VDZ and CR two-shape systems for combination linings. Together, offer refractory users a ready reference of information governing furnace refractory lining and construction.

If you require a special shape which is not included in this booklet, please contact your Harbison-Walker representative. Harbison-Walker manufactures special shapes based on customer designs showing shape details and assembly in the furnace lining.

### OVERVIEW

Refractory brick are classified on the basis of their form as Rectangular Shapes or Special Shapes.

Rectangular Sizes are brick of relatively simple design, with certain definite shapes, that are marketed in sufficient amounts to permit quantity production. Rectangular sizes are preferred wherever furnace construction and operating conditions permit. These brick cost less than longer and more intricate shapes.

Special Shapes are refractory brick of special design of either simple or intricate form. Some special shapes may be considered as modifications of rectangular tile having the same overall dimensions.

For initial orders of special shapes, drawings showing complete details of the shapes, as well as their assembly in the furnace, should be included. The drawing and shape numbers should be provided on all subsequent orders.



### Nine-Inch Sizes (9 X 4<sup>1</sup>/<sub>2</sub> X 3)

### Nine-Inch Sizes (9 X 4<sup>1</sup>/<sub>2</sub> X 3)



### High-Alumina, Basic and Silica Brick

TYPICAL ST	RAIGHT, ARCH, W	EDGE AND KEY BRI	СК	
				Siz 9 x
Straight	Arch	Wedge	Key	
Sizes	Name	Dimensions (In.)	Equivalent	
9 x 41/2 x 21/2 9 x 31/2 x 21/2 9 x 21/4 x 21/2 9 x 41/2 x 21/2	Straight Soap 2" Split Split	9 x 41/2 x 21/2 9 x 21/4 x 21/2 9 x 41/2 x 21/2 9 x 41/2 x 21/2 9 x 41/2 x 11/4	1.00 0.50 0.80 0.50	
9 x 41/2 x 21/2	No. 1-X Wedge No. 1 Wedge No. 2 Wedge No. 1 Arch No. 2 Arch No. 3 Arch No. 1 Key No. 2 Key No. 3 Key No. 4 Key	9 x $41/2$ x $(21/2.21/4)$ 9 x $41/2$ x $(21/2.21/8)$ 9 x $41/2$ x $(21/2.17/8)$ 9 x $41/2$ x $(21/2.21/8)$ 9 x $41/2$ x $(21/2.13/4)$ 9 x $41/2$ x $(21/2.13/4)$ 9 x $41/2$ x $(21/2.1)$ 9 x $(41/2.4)$ x $21/2$ 9 x $(41/2.31/2)$ x $21/2$ 9 x $(41/2.3)$ x $21/2$ 9 x $(41/2.21/4)$ x $21/2$	0.95 0.88 0.80 0.93 0.85 0.70 0.94 0.89 0.83 0.75	9 x 9 x
9 x 41/2 x 21/2	48° End Skew 60° End Skew 48° Side Skew 60° Side Skew Edge Skew Featheredge Neck Jamb	$\begin{array}{c} (9{\text{-}}63/4) \times 41/2 \times 21/2 \\ (9{\text{-}}79/16) \times 41/2 \times 21/2 \\ 9 \times (41/2{\text{-}}21/4) \times 21/2 \\ 9 \times (41/2{\text{-}}21/4) \times 21/2 \\ 9 \times (41/2{\text{-}}11/2) \times 21/2 \\ 9 \times (41/2{\text{-}}11/2) \times 21/2 \\ 9 \times 41/2 \times (21/2{\text{-}}1/8) \\ 9 \times 41/2 \times (21/2{\text{-}}5/8) \\ 9 \times 41/2 \times 21/2 \end{array}$	0.88 0.92 0.75 0.84 0.67 0.53 0.63 0.89	12
9 x 4 <sup>1</sup> / <sub>2</sub> x 3 9 x 3 <sup>1</sup> / <sub>2</sub> x 3 9 x 2 <sup>1</sup> / <sub>4</sub> x 3 9 x 4 <sup>1</sup> / <sub>2</sub> x 1 <sup>1</sup> / <sub>2</sub>	Straight Sm. Straight Soap Split	9 x 4 <sup>1</sup> / <sub>2</sub> x 3 9 x 3 <sup>1</sup> / <sub>2</sub> x 3 9 x 2 <sup>1</sup> / <sub>4</sub> x 3 9 x 4 <sup>1</sup> / <sub>2</sub> x 1 <sup>1</sup> / <sub>2</sub>	1.20 0.93 0.60 0.60	
9 x 41/2 x 3	No. 1 Arch No. 2 Arch No. 3 Arch No. 4 Arch No. 1-X Wedge No. 1 Wedge No. 2 Wedge	9 x $41/2$ x $(3-23/4)$ 9 x $41/2$ x $(3-21/2)$ 9 x $41/2$ x $(3-2)$ 9 x $41/2$ x $(3-2)$ 9 x $41/2$ x $(3-1)$ 9 x $41/2$ x $(3-27/8)$ 9 x $41/2$ x $(3-23/4)$ 9 x $41/2$ x $(3-23/4)$	1.15 1.10 1.00 0.80 1.17 1.15 1.10	12
	No. 3 Wedge No. 1 Key No. 2 Key No. 3 Key No. 4 Key	9 x 41/2 x (3-2) 9 x (41/2-4) x 3 9 x (41/2-31/2) x 3 9 x (41/2-3) x 3 9 x (41/2-3) x 3 9 x (41/2-21/4) x 3	1.00 1.13 1.07 1.00 0.90	12
9 x 4 <sup>1</sup> / <sub>2</sub> x 3	48° End Skew 60° End Skew 48° Side Skew 60° Side Skew Edge Skew Featheredge Neck Jamb	$\begin{array}{c} (9-65/16) \times 41/2 \times 3 \\ (9-71/4) \times 41/2 \times 3 \\ 9 \times (41/2-113/16) \times 3 \\ 9 \times (41/2-23/4) \times 3 \\ 9 \times (41/2-23/4) \times 3 \\ 9 \times (41/2-11/2) \times 3 \\ 9 \times 41/2 \times (3-1/8) \\ 9 \times 41/2 \times (3-5/8) \\ 9 \times 41/2 \times 3 \end{array}$	1.02 1.08 0.84 0.97 0.80 0.63 0.73 1.07	12
9 x 6 Flat Back	Straight Split No. 1 Arch No. 2 Arch	9 x 6 x 2 <sup>1</sup> / <sub>2</sub> 9 x 6 x 1 <sup>1</sup> / <sub>4</sub> 9 x 6 x (3 <sup>1</sup> / <sub>2</sub> -2 <sup>1</sup> / <sub>2</sub> ) 9 x 6 x (3 <sup>1</sup> / <sub>2</sub> -2)	1.33 0.67 1.60 1.47	

Sizes	Name	Dimensions (In.)	Equivalent
9 x 6 x 3	Straight	9 x 6 x 3	1.60
	No. 1 Arch	9 x 6 x (3-2 <sup>3</sup> / <sub>4</sub> )	1.53
	No. 2 Arch	9 x 6 x (3-2 <sup>1</sup> / <sub>2</sub> )	1.47
	No. 3 Arch	9 x 6 x (3-2)	1.33
	No. 1-X Wedge	9 x 6 x (3-2 <sup>7</sup> /8)	1.57
	No. 1 Wedge	9 x 6 x (3-2 <sup>3</sup> /4)	1.53
	No. 2 Wedge	9 x 6 x (3-2 <sup>1</sup> /2)	1.47
	No. 3 Wedge	9 x 6 x (3-2)	1.33
	No. 1 Key	9 x (6-5 <sup>3</sup> /8) x 3	1.52
	No. 2 Key	9 x (6-4 <sup>13</sup> /16) x 3	1.44
	No. 3 Key	9 x (6-3) x 3	1.20
9 x 6³/4 x 3	Straight	9 x 6 <sup>3</sup> / <sub>4</sub> x 3	1.80
	No. 1-X Wedge	9 x 6 <sup>3</sup> / <sub>4</sub> x (3-2 <sup>7</sup> / <sub>8</sub> )	1.76
	No. 1 Wedge	9 x 6 <sup>3</sup> / <sub>4</sub> x (3-2 <sup>3</sup> / <sub>4</sub> )	1.72
	No. 2 Wedge	9 x 6 <sup>3</sup> / <sub>4</sub> x (3-2 <sup>1</sup> / <sub>2</sub> )	1.65
	No. 3 Wedge	9 x 6 <sup>3</sup> / <sub>4</sub> x (3-2)	1.50
9 x 9 x 3	Straight No. 1-X Wedge No. 1 Wedge No. 2 Wedge No. 3 Wedge	9 x 9 x 3 9 x 9 x (3-2 <sup>7</sup> / <sub>8</sub> ) 9 x 9 x (3-2 <sup>3</sup> / <sub>4</sub> ) 9 x 9 x (3-2 <sup>1</sup> / <sub>2</sub> ) 9 x 9 x (3-2 <sup>1</sup> / <sub>2</sub> ) 9 x 9 x (3-2)	2.40 2.35 2.30 2.20 2.00
12 x 41/2 x 3	Straight	12 x 4 <sup>1</sup> / <sub>2</sub> x 3	1.60
	No. 1 Arch	12 x 4 <sup>1</sup> / <sub>2</sub> x (3-2 <sup>3</sup> / <sub>4</sub> )	1.53
	No. 2 Arch	12 x 4 <sup>1</sup> / <sub>2</sub> x (3-2 <sup>1</sup> / <sub>2</sub> )	1.47
	No. 3 Arch	12 x 4 <sup>1</sup> / <sub>2</sub> x (3-2)	1.33
	No. 1-X Wedge	12 x 4 <sup>1</sup> / <sub>2</sub> x (3-2 <sup>7</sup> / <sub>8</sub> )	1.57
	No. 1 Wedge	12 x 4 <sup>1</sup> / <sub>2</sub> x (3-2 <sup>3</sup> / <sub>4</sub> )	1.53
	No. 2 Wedge	12 x 4 <sup>1</sup> / <sub>2</sub> x (3-2 <sup>1</sup> / <sub>2</sub> )	1.47
	No. 3 Wedge	12 x 4 <sup>1</sup> / <sub>2</sub> x (3-2)	1.33
12 x 6 x 3	Straight	12 x 6 x 3	2.13
	No. 1 Arch	12 x 6 x (3-2 <sup>3</sup> /4)	2.04
	No. 2 Arch	12 x 6 x (3-2 <sup>1</sup> /2)	1.96
	No. 3 Arch	12 x 6 x (3-2)	1.78
	No. 1-X Wedge	12 x 6 x (3-2 <sup>7</sup> /8)	2.09
	No. 1 Wedge	12 x 6 x (3-2 <sup>3</sup> /4)	2.04
	No. 2 Wedge	12 x 6 x (3-2 <sup>1</sup> /2)	1.96
	No. 3 Wedge	12 x 6 x (3-2)	1.78
	No. 1 Key	12 x (6-51/2) x 3	2.04
	No. 2 Key	12 x (6-5) x 3	1.96
	No. 3 Key	12 x (6-3) x 3	1.87
12 x 6 <sup>3</sup> /4 x 3	Straight	12 x 6 <sup>3</sup> /4 x 3	2.40
	No. 1-X Wedge	12 x 6 <sup>3</sup> /4 x (3-2 <sup>7</sup> /8)	2.35
	No. 1 Wedge	12 x 6 <sup>3</sup> /4 x (3-2 <sup>3</sup> /4)	2.30
	No. 2 Wedge	12 x 6 <sup>3</sup> /4 x (3-2 <sup>1</sup> /2)	2.20
	No. 3 Wedge	12 x 6 <sup>3</sup> /4 x (3-21/2)	2.00
12 x 9 x 3	No. 1 Arch	12 x 9 x (3-2 <sup>3</sup> /4)	3.07
	No. 2 Arch	12 x 9 x (3-2 <sup>1</sup> /2)	2.93
	No. 3 Arch	12 x 9 x (3-2)	2.67
	Straight No. 1-X Wedge No. 1 Wedge No. 2 Wedge No. 3 Wedge	12 x 9 x 3 12 x 9 x (3-27/8) 12 x 9 x (3-23/4) 12 x 9 x (3-21/2) 12 x 9 x (3-21/2) 12 x 9 x (3-2)	3.20 3.13 3.07 2.93 2.67

## BRICK SIZES AND SHAPES

Sizes	Name	Dimensions (In.)	Equivalent
13 <sup>1</sup> /2 x 4 <sup>1</sup> /2 x 3	Straight	13 <sup>1</sup> / <sub>2</sub> x 4 <sup>1</sup> / <sub>2</sub> x 3	1.80
	No. 1 Arch	13 <sup>1</sup> / <sub>2</sub> x 4 <sup>1</sup> / <sub>2</sub> x (3-2 <sup>3</sup> / <sub>4</sub> )	1.72
	No. 2 Arch	13 <sup>1</sup> / <sub>2</sub> x 4 <sup>1</sup> / <sub>2</sub> x (3-2 <sup>1</sup> / <sub>2</sub> )	1.65
	No. 3 Arch	13 <sup>1</sup> / <sub>2</sub> x 4 <sup>1</sup> / <sub>2</sub> x (3-2)	1.50
	No. 1 Key	131/2 x (41/2-4) x 3	1.70
	No. 2 Key	131/2 x (41/2-31/2) x 3	1.60
	No. 3 Key	131/2 x (41/2-3) x 3	1.50
	No. 4 Key	131/2 x (41/2-3) x 3	1.35
13 <sup>1</sup> /2 x 6 x 3	Straight No. 1 Arch No. 2 Arch No. 3 Arch	131/2 x 6 x 3 131/2 x 6 x (3-23/4) 131/2 x 6 x (3-21/2) 131/2 x 6 x (3-21/2) 131/2 x 6 x (3-2)	2.40 2.30 2.20 2.00
	No. 1-X Wedge	13 <sup>1</sup> / <sub>2</sub> x 6 x (3-2 <sup>7</sup> / <sub>8</sub> )	2.35
	No. 1 Wedge	13 <sup>1</sup> / <sub>2</sub> x 6 x (3-2 <sup>3</sup> / <sub>4</sub> )	2.30
	No. 2 Wedge	13 <sup>1</sup> / <sub>2</sub> x 6 x (3-2 <sup>1</sup> / <sub>2</sub> )	2.20
	No. 3 Wedge	13 <sup>1</sup> / <sub>2</sub> x 6 x (3-2)	2.00
	No. 1 Key	13 <sup>1</sup> / <sub>2</sub> x (6-5) x 3	2.20
	No. 2 Key	13 <sup>1</sup> / <sub>2</sub> x (6-4 <sup>3</sup> / <sub>8</sub> ) x 3	2.07
	No. 3 Key	13 <sup>1</sup> / <sub>2</sub> x (6-3) x 3	1.80
13 <sup>1</sup> /2 x 6 <sup>3</sup> /4 x 3	Straight	13 <sup>1</sup> / <sub>2</sub> x 6 <sup>3</sup> / <sub>4</sub> x 3	2.70
	No. 1-X Wedge	13 <sup>1</sup> / <sub>2</sub> x 6 <sup>3</sup> / <sub>4</sub> x (3-2 <sup>7</sup> / <sub>8</sub> )	2.64
	No. 1 Wedge	13 <sup>1</sup> / <sub>2</sub> x 6 <sup>3</sup> / <sub>4</sub> x (3-2 <sup>3</sup> / <sub>4</sub> )	2.59
	No. 2 Wedge	13 <sup>1</sup> / <sub>2</sub> x 6 <sup>3</sup> / <sub>4</sub> x (3-2 <sup>1</sup> / <sub>2</sub> )	2.47
	No. 3 Wedge	13 <sup>1</sup> / <sub>2</sub> x 6 <sup>3</sup> / <sub>4</sub> x (3-2)	2.25
13 <sup>1</sup> /2 x 9 x 3	Straight	131/2 x 9 x 3	3.60
	No. 1 Arch	131/2 x 9 x (3-23/4)	3.45
	No. 2 Arch	131/2 x 9 x (3-21/2)	3.30
	No. 3 Arch	131/2 x 9 x (3-21/2)	3.00
	No. 1-X Wedge No. 1 Wedge No. 2 Wedge No. 3 Wedge	131/2 x 9 x (3-27/8) 131/2 x 9 x (3-23/4) 131/2 x 9 x (3-21/2) 131/2 x 9 x (3-21/2) 131/2 x 9 x (3-2)	3.52 3.45 3.30 3.00
15 x 41/2 x 3	Straight	15 x 4 <sup>1</sup> / <sub>2</sub> x 3	2.00
	No. 1 Arch	15 x 4 <sup>1</sup> / <sub>2</sub> x (3-2 <sup>3</sup> / <sub>4</sub> )	1.92
	No. 2 Arch	15 x 4 <sup>1</sup> / <sub>2</sub> x (3-2 <sup>1</sup> / <sub>2</sub> )	1.83
	No. 3 Arch	15 x 4 <sup>1</sup> / <sub>2</sub> x (3-2)	1.67
	No. 1-X Wedge	15 x 4 <sup>1</sup> / <sub>2</sub> x (3-2 <sup>7</sup> / <sub>8</sub> )	1.96
	No. 1 Wedge	15 x 4 <sup>1</sup> / <sub>2</sub> x (3-2 <sup>3</sup> / <sub>4</sub> )	1.92
	No. 2 Wedge	15 x 4 <sup>1</sup> / <sub>2</sub> x (3-2 <sup>1</sup> / <sub>2</sub> )	1.83
	No. 3 Wedge	15 x 4 <sup>1</sup> / <sub>2</sub> x (3-2)	1.67
15 x 6 x 3	Straight No. 1-X Wedge No. 1 Wedge No. 2 Wedge No. 3 Wedge	15 x 6 x 3 15 x 6 x (3-27/8) 15 x 6 x (3-23/4) 15 x 6 x (3-23/4) 15 x 6 x (3-21/2) 15 x 6 x (3-2)	2.67 2.61 2.56 2.44 2.22
	No. 1 Key	15 x (6-5) x 3	2.56
	No. 2 Key	15 x (6-4 <sup>3</sup> /8) x 3	2.31
	No. 3 Key	15 x (6-3) x 3	2.00
15 x 9 x 3	Straight	15 x 9 x 3	4.00
	No. 1-X Wedge	15 x 9 x (3-2 <sup>7</sup> /8)	3.92
	No. 1 Wedge	15 x 9 x (3-2 <sup>3</sup> /4)	3.83
	No. 2 Wedge	15 x 9 x (3-2 <sup>1</sup> /2)	3.67
	No. 3 Wedge	15 x 9 x (3-2)	3.33

Sizes	Name	Dimensions (In.)	Equivalent
18 x 41/2 x 3	Straight No. 1-X Wedge No. 1 Wedge No. 2 Wedge No. 3 Wedge	18 x 41/2 x 3 18 x 41/2 x (3-27/8) 18 x 41/2 x (3-23/4) 18 x 41/2 x (3-21/2) 18 x 41/2 x (3-21/2) 18 x 41/2 x (3-2)	2.40 2.35 2.30 2.20 2.00
18 x 6 x 3	Straight No. 1-X Wedge No. 1 Wedge No. 2 Wedge No. 3 Wedge	18 x 6 x 3 18 x 6 x (3-2 <sup>7</sup> /8) 18 x 6 x (3-2 <sup>3</sup> /4) 18 x 6 x (3-2 <sup>1</sup> /2) 18 x 6 x (3-2)	3.20 3.13 3.07 2.93 2.67
18 x 9 x 3	Straight No. 1-X Wedge No. 1 Wedge No. 2 Wedge No. 3 Wedge	18 x 9 x 3 18 x 9 x (3-27/8) 18 x 9 x (3-23/4) 18 x 9 x (3-21/2) 18 x 9 x (3-21/2) 18 x 9 x (3-2)	4.80 4.70 4.60 4.40 4.00
21 x 6 x 3	Straight No. 1-X Wedge No. 1 Wedge No. 2 Wedge No. 3 Wedge	21 x 6 x 3 21 x 6 x (3-27/8) 21 x 6 x (3-23/4) 21 x 6 x (3-21/2) 21 x 6 x (3-21/2) 21 x 6 x (3-2)	3.73 3.65 3.58 3.42 3.11
21 x 9 x 3	Straight No. 1-X Wedge No. 1 Wedge No. 2 Wedge No. 3 Wedge	21 x 9 x 3 21 x 9 x (3-27/8) 21 x 9 x (3-23/4) 21 x 9 x (3-21/2) 21 x 9 x (3-21/2) 21 x 9 x (3-2)	5.60 5.48 5.37 5.13 4.67
Misc. Straights	Straight Straight Straight Straight Straight Straight Straight Straight	9 x 6 x 2 9 x 7 x 2 9 x 7 <sup>1/2</sup> x 2 10 <sup>1/2</sup> x 4 <sup>1/2</sup> x 3 10 <sup>1/2</sup> x 4 <sup>1/2</sup> x 4 <sup>1/2</sup> 13 <sup>1/2</sup> x 4 <sup>1/2</sup> x 4 <sup>1/2</sup> 18 x 6 <sup>3/4</sup> x 3 18 x 9 x 4 <sup>1/2</sup>	1.07 1.24 1.33 1.39 2.10 2.70 3.60 7.20

### METALKASE DOOR JAMB BRICK



Name	A (In)	B (In)	C (In)	D (In)
DJ-1-3	9	<b>4</b> 1/2	11/2	3
DJ-2-3	9	6 <sup>3</sup> /4	3 3/4	3
DJ-3-3	9	9	6	3
BS-115-3	<b>13</b> 1/2	6 <sup>3</sup> /4	2 <sup>3</sup> /4	3
BS-116-3	<b>13</b> 1/2	9	5	3
DJ-18-1-3	18	6 <sup>3</sup> /4	2 3/4	3
DJ-18-2-3	18	9	5	3

### BLAST-FURNACE BOTTOM BLOCKS

(18 X 9 X 4 <sup>1</sup>/<sub>2</sub> Inches) Number per course for blocks laid on end

Diamete Hearth J (Ft	er of acket In)	No. of Blocks	Diameter of Hearth Jacket (Ft In)		No. of Blocks
17 18 18 19 19	6 0 6 0 6	897 947 999 1053 1108	27 28 28 29 29	6 0 6 0	2176 2255 2335 2417 2500
20 20 21 21 22	0 6 0 6 0	1164 1222 1281 1342 1403	30 30 31 31 32	0 6 0 6 0	2584 2669 2756 2845 2935
22 23 23 24 24	6 0 6 0 6	1467 1531 1598 1665 1734	32 33 33 34 34	6 0 6 0	3026 3119 3213 3308 3405
25 25 26 26 27	0 6 0 6 0	1804 1876 1949 2023 2099	35 35 36 36 37	0 6 0 6 0	3503 3603 3704 3806 3909

### High-Alumina Circle Brick

Nine-Inch Sizes (9 X 4 1/2 X 3)	Circle Brick Number* (3 Inch)	Chord (Inch)	Number Per Ring	* The first two numbers of the Circle Number indicate the inside and outside diame- ters,respectively, of the ring
	24 - 33 - 3	6 <sup>17</sup> / <sub>32</sub>	12	
9*	36 - 45 - 3	<b>7</b> <sup>3</sup> /16	16	example. 24 - 33 - 3 Circle
	48 - 57 - 3	<b>7</b> 19/32	20	Brick will produce a ring with a 24-inchinside diame- ter and 33-inch outside diameter for a 41½inch lining
	60 - 69 - 3	<b>7</b> <sup>13</sup> /16	24	
TR N	72 - 81 - 3	8	29	
× ~5	84 - 93 - 3	8 1/8	33	
	96 - 105 - 3	8 <sup>7</sup> / <sub>32</sub>	37	
	108 - 117 - 3	8 <sup>5</sup> /16	41	
	120 - 129 - 3	8 <sup>3</sup> /8	45	



NOTE: Blast Furnace keys X-1 and X-2 are also regulary manufactured in 6, 10<sup>1</sup>/<sub>2</sub> and 15-inch lengths. The brick combinations for rings (see Brick Combinations for All-Key Linings table) are applicable for X-1 and X-2 keys of all lengths.

### BRICK COMBINATIONS FOR ALL-KEY LININGS

Diameter Inside	Number Required Per Ring		
(Ft In)	X-2	X-1	Total
13 3	98	—	98
13 6	96	3	99
13 9	95	6	101
14 0	95	8	103
14 6	93	13	106
15 0	91	18	109
15 6	89	23	112
16 0	87	28	115
16 6	85	33	118
17 0	84	37	121
17 6	82	42	124
18 0	80	48	128
18 6	79	52	131
19 0	77	57	134
19 6	75	62	137
20 0	73	67	140
20 6	71	72	143
21 0	70	76	146
21 6	68	82	150
22 0	66	87	153
22 6	65	91	156
23 0	63	96	159
23 6	61	101	162
24 0	59	106	165
24 6	57	111	168
25 0	56	116	172
25 6	54	121	175
26 0	52	126	178
26 6	51	130	181

Diameter Inside	Number Required Per Ring		
(Ft In)	X-2	X-1	Total
27 0	49	135	t84
27 6	47	140	187
28 0	45	145	190
28 6	44	150	194
29 0	42	155	197
29 6	40	160	200
30 0	38	165	203
30 6	37	169	206
31 0	35	174	209
31 6	33	179	212
32 0	32	184	216
32 6	30	189	219
33 0	28	194	222
33 6	26	199	225
34 0	24	204	228
34 6	23	208	231
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	21	213	234
	19	219	238
	18	223	241
	16	228	244
37 0	14	233	247
37 6	12	238	250
38 0	10	243	253
38 6	9	247	256
39 0 39 6 40 0 40 6 41 0	7 5 4 2	253 258 262 267 272	260 263 266 269 272

### **OVERVIEW**

Electric furnace roofs may be constructed using many different shapes and combinations. The combination of standard size key-arch and key-wedge shapes with standard shapes design, and the two-shape (arch-key-wedge) brick design are the most common in electric furnace roof construction.

Annular rings are laid from the combinations for your specific roof design. Consideration must be given to the best design to provide cost-effective service life. The twoshape, triple taper brick uses two bricks that conform to the roof contour. Bricklaying is simplified using only two shapes, in that inventory levels may be reduced and faster installation is possible. The chart below displays two-shape electric furnace roof brick combinations for 9-inch roof thicknesses. By combining both shapes, all annular rings for a given diameter can be calculated. The center of the range indicates the ideal spherical radius for the given system. Shape identification is done by a notching system at the cold end of the brick shape, as illustrated on p. 29. The two-shape system is also available in 13<sup>1</sup>/<sub>2</sub>-inch sizes for larger electric furnace roofs.

Providing your Harbison-Walker representatives with the dimensions of your electric furnace roof or a current drawing of your roof enables them to produce an accurate ring count and assembly detail.

### ELECTRIC FURNACE ROOF-SHAPES 9 X 4<sup>1</sup>/<sub>2</sub> X 3-Inch Arch-Key-Wedge Shapes

Spherical Radius Range	H-W Shape Designations
6'6" to 7'9"	HW-2721-B HW-2721-S
7'9" to 9'6"	HW-2746-B HW-2746-A
9'6" to 12'6"	HW-2745-B HW-2745-A
12'6" to 16'0"	HW-2592-B HW-2592-A
16'0" to 22'4"	HW-2704-B HW-2704-A



### **OVERVIEW**

Harbison-Walker manufactures Semi-Universal Ladle Brick (SULB) in fireclay, high-alumina and basic refractories in four series of brick to line sidewalls of iron and steel teeming ladles of various diameters and configurations. All series can be produced in widths to construct linings 3 to 9 inches thick. A SULB lining usually includes a tilt back course to lay the rings square against the sloping sides of a ladle and one or more starter sets to start the upward spiral. For guidance in selecting the proper series for any ladle, the following chart identifies

Series	Ladle Diameter (Inch)
SU 20	45 to 70
SU 30	70 to 100
SU 45	100 to 140
SU 60	140 and Up

In all four series, the width of the brick, equivalent to the thickness of the lining, is positioned in the rectangular frame \_\_\_\_\_\_. For example, a 5-inch thick lining in a ladle about 120 inches in diameter would require an SU 5-45 series brick. SULB's are also available in two additional thicknesses \_\_\_\_\_4-inch and 100 mm. A universal starter set that suits all series and wall thicknesses up to 7 inches is available. The 12-piece UL-7-SS12 set is illustrated below. A regular 18-piece starter set for 9-inch thick walls is also available.

The number of SULB shapes required for a lining can be calculated by multiplying the average diameter of the ladle by 3.1416, then dividing by 8.25 (length of brick) to find the number per ring. The height in inches of the ladle wall divided by 3 equals the number of rings. The number of pieces per ring times the number of rings equals the total number of SULB shapes required.



For a ladle with an average diameter of 120 inches (outside diameter of SULB lining) and a height of 96 inches, the calculations follow:

$$\frac{3.1416 \times 120}{8.25} = 46 \text{ pieces per}$$
$$\frac{96}{3} = 32 \text{ rings}$$

46 x 32 = 1472 SULB brick per lining

(All series for a 4-inch thick wall)







Note:

Brick Combinations required for arch construction are detailed in the tables starting on pages 71. These tables are useful for estimating the quantities of brick required for the construction of arches.

### BRICK COUNTS FOR ROTARY KILNS

### **HIGH-ALUMINA BRICK**

### ROTARY KILN BLOCKS Arch-Type (9 x 6 x 3<sup>1</sup>/<sub>2</sub>)

The numbers in the RKB column indicate the inside and outside diameters, respectively, of the ring produced by the shape. For example, RKB 162-A-174 will produce a ring with a 162-inch inside diameter and 174-inch outside diameter.



Ins. Dia.	RKB	Inside	Number
Kiln Shell	Number	Chord (In.)	Per Ring
3'-6"	30-A-42	2 1/2	37
4'-0"	36-A-48	2 5/8	42
4'-6"	42-A-54	2 23/32	47
5'-0"	48-A-600	2 13/16	52
5'-6"	54-A-66	2 7/8	58
6'-0"	60-A-72	2 <sup>29</sup> / <sub>32</sub>	63
6'-6"	66-A-78	2 <sup>31</sup> / <sub>32</sub>	68
7'-0"	72-A-84	3	74
7'-6"	78-A-90	3 <sup>1</sup> / <sub>32</sub>	79
8'-0"	84-A-96	3 1/16	84
8'-6"	90-A-102	3 3/32	89
9'-0"	96-A-108	3 1/8	95
9'-6"	102-A-114	3 1/8	100
10'-0" 10'-6" 11'-0" 11'-3" 11'-6"	108-A-120 114-A-126 120-A-132 123-A-135 126-A-138	3 <sup>5</sup> / <sub>32</sub> 3 <sup>5</sup> / <sub>32</sub> 3 <sup>3</sup> / <sub>16</sub> 3 <sup>3</sup> / <sub>16</sub>	105 111 116 119 121
12'-0"	132-A-144	3 7/32	126
12'-6"	138-A-150	3 7/32	132
13'-0"	144-A-156	3 7/32	137
13'-6"	150-A-162	3 1/4	142
14'-0"	156-A-168	3 <sup>1</sup> /4	148
14'-6"	162-A-174	3 <sup>1</sup> /4	153
15'-0"	168-A-180	3 <sup>9</sup> /32	158
15'-6"	174-A-186	3 <sup>9</sup> /32	164
16'-0"	180-A-192	3 <sup>9</sup> / <sub>32</sub>	169
16'-6"	186-A-198	3 <sup>9</sup> / <sub>32</sub>	174
17'-0"	192-A-204	3 <sup>9</sup> / <sub>32</sub>	179
17'-6"	198-A-210	3 <sup>5</sup> / <sub>16</sub>	185
18'-0"	204-A-216	<b>3</b> <sup>5</sup> /16	190

To facilitate the keying of arch-type rotary kiln blocks, keying bricks of two-thirds thickness, RKA-<sup>2</sup>/<sub>3</sub>, and of three-quarters thickness, RKA-<sup>3</sup>/<sub>4</sub>, are made. Two of each keying brick should be ordered for each ring.

\* All brick quantities per ring have been calculated from theoretical diameter turned by the brick to which a steel plate (1.5 mm thickness) has been attached.
## HIGH-ALUMINA BRICK

### ROTARY KILN BLOCKS Nine-Inch Size (9 x 9 x 4)

The numbers in the RKB column indicate the inside and outside diameters, respectively, of the ring produced by the shape. For example, 48-66 RKB will produce a ring with a 48-inch inside diameter and 66-inch outside diameter for a 9-inch lining.



Ins. Dia.	RKB	Inside	Number
Kiln Shell	Number	Chord (In.)	Per Ring
5'-6"	48-66	6 <sup>17</sup> / <sub>32</sub>	23
6'-0"	54-72	6 <sup>3</sup> / <sub>4</sub>	26
6'-6"	60-78	6 <sup>17</sup> / <sub>16</sub>	28
7'-0"	66-84	7 <sup>1</sup> / <sub>16</sub>	30
7'-6"	72-90	7 <sup>3</sup> / <sub>16</sub>	32
8'-0"	78-96	7 <sup>5</sup> / <sub>16</sub>	34
8'-6"	84-102	7 <sup>13</sup> / <sub>32</sub>	36
9'-0"	90-108	7 <sup>1</sup> / <sub>2</sub>	38
9'-6"	96-114	7 <sup>19</sup> / <sub>32</sub>	40
10'-0"	102-120	7 <sup>21</sup> / <sub>32</sub>	42
10'-6"	108-126	7 <sup>23</sup> / <sub>32</sub>	44
11'-0"	114-132	7 <sup>25</sup> / <sub>32</sub>	46
11'-3"	117-135	7 <sup>13</sup> / <sub>16</sub>	48
11'-6"	120-138	7 <sup>13</sup> / <sub>16</sub>	49
12'-0"	126-144	7 <sup>7</sup> / <sub>8</sub>	51
12'-6"	132-150	7 <sup>29</sup> / <sub>32</sub>	53
13'-0"	138-156	7 <sup>31</sup> / <sub>32</sub>	55
13'-6"	144-162	8	57
14'-0"	150-168	8 <sup>1</sup> / <sub>32</sub>	59
14'-6"	156-174	8 <sup>1</sup> / <sub>16</sub>	61
15'-0"	162-180	8 <sup>3</sup> / <sub>32</sub>	63
15'-6"	168-186	8 <sup>1</sup> / <sub>8</sub>	65
16'-0"	174-192	8 <sup>5</sup> / <sub>32</sub>	67
16'-6"	180-198	8 <sup>3</sup> /16	70
17'-0"	186-204	8 <sup>7</sup> / <sub>32</sub>	72
17'-6"	192-210	8 <sup>7</sup> / <sub>32</sub>	74
18'-0"	198-216	8 <sup>1</sup> / <sub>4</sub>	76
18'-6"	204-222	8 <sup>9</sup> / <sub>32</sub>	78
19'-0"	210-228	8 <sup>9</sup> / <sub>32</sub>	80
19'-6"	216-234	8 <sup>5</sup> / <sub>16</sub>	82
20'-0"	222-240	8 <sup>5</sup> / <sub>16</sub>	84
20'-6"	228-246	8 <sup>11</sup> / <sub>32</sub>	86
21'-0"	234-252	8 <sup>11</sup> / <sub>32</sub>	88
21'-6"	240-258	8 <sup>3</sup> / <sub>8</sub>	90

## BRICK COUNTS FOR ROTARY KILNS

#### **HIGH-ALUMINA BRICK**

### ROTARY KILN BLOCKS Six-Inch Size (9 x 6 x 4)

The numbers under the RKB column indicate the inside and outside diameters, respectively, of the ring produced by each shape. For example, 144-156 RKB will produce a ring with a 144-inch inside diameter and 156-inch outside diameter for a 6-inch lining.



Ins. Dia. Kiln Shell	RKB Number	Inside Chord (In.)	Number Per Ring
3'-6"	30-42	6 <sup>7</sup> /16	15
4'-0"	36-48	<b>6</b> <sup>3</sup> / <sub>4</sub>	17
4'-6"	42-54	7	19
5'-0"	48-60	<b>7</b> <sup>3</sup> /16	21
5'-6"	54-66	<b>7</b> <sup>3</sup> /8	23
6'-0"	60-72	<b>7</b> <sup>1</sup> / <sub>2</sub>	26
6'-6"	66-78	<b>7</b> <sup>5</sup> /8	28
7'-0"	72-84	7 <sup>23</sup> /32	30
7'-6"	78-90	<b>7</b> <sup>13</sup> /16	32
8'-0"	84-96	<b>7</b> <sup>7</sup> /8	34
8'-6"	90-102	<b>7</b> <sup>15</sup> /16	36
9'-0"	96-108	8	38
9'-6"	102-114	<b>8</b> <sup>1</sup> /16	40
10'-0"	108-120	<b>8</b> <sup>3</sup> /32	42
10'-6"	114-126	<b>8</b> <sup>5</sup> / <sub>32</sub>	44
11'-0"	120-132	<b>8</b> <sup>3</sup> /16	46
11'-3"	123-135	<b>8</b> <sup>3</sup> /16	48
11'-6"	126-138	8 7/32	49
12'-0"	132-144	8 <sup>1</sup> /4	51
12'-6"	138-150	<b>8</b> <sup>9</sup> / <sub>32</sub>	53
13'-0"	144-156	<b>8</b> <sup>5</sup> /16	55
13'-6"	150-162	8 <sup>11</sup> / <sub>32</sub>	57
14'-0"	156-168	<b>8</b> <sup>11</sup> / <sub>32</sub>	59
14'-6"	162-174	<b>8</b> <sup>3</sup> / <sub>8</sub>	61
15'-0"	168-180	8 <sup>13</sup> /32	63
15'-6"	174-186	8 <sup>13</sup> / <sub>32</sub>	65
16'-0"	180-192	<b>8</b> <sup>7</sup> /16	67
16'-6"	186-198	8 <sup>15</sup> /32	70
17'-0"	192-204	8 <sup>15</sup> /32	72
17'-6"	198-210	<b>8</b> <sup>1</sup> / <sub>2</sub>	74
18'-0"	204-216	<b>8</b> <sup>1</sup> / <sub>2</sub>	76
18'-6"	210-222	<b>8</b> <sup>1</sup> / <sub>2</sub>	78
19'-0"	216-228	<b>8</b> <sup>17</sup> / <sub>32</sub>	80
19'-6"	222-234	8 <sup>17</sup> / <sub>32</sub>	82
20'-0"	228-240	<b>8</b> <sup>9</sup> /16	84
20'-6"	234-246	<b>8</b> <sup>9</sup> /16	86
21'-0"	240-252	<b>8</b> <sup>9</sup> /16	88

### KA AND KW BLOCKS FOR ROTARY KILNS

Harbison-Walker developed the KA and KW system to simplify and eliminate problems associated with the linings of rotary kilns. KA and KW blocks are 9 x 6 x 4-inch kiln liners made in the arch or wedge shape for high-alumina brick. Each shape is furnished in four sizes, two of which will line any kiln (see chart below). In addition, two thirds and three quarter splits are designed to work with all KA and KW linings to eliminate the need for cutting keys.

Using the proper combination of KA and KW blocks also can reduce shimming, thereby producing a tighter lining with less chance of dropout or spiraling. Because these shapes fit kilns of many sizes, operators with kilns of different sizes can reduce their in-plant inventories.

Kiln Diameter Combinations								
	6 to 8 feet	8 to 13 feet	13 to 21 feet					
Linings 6 inches thick	KA-3, KA-2	KA-2, KA-I	KA-I, KA-IX					
Linings 9 inches thick	KW-3, KW-2	KW-2, KW-I	KW-I, KW-IX					



## Number of KA Blocks Required for Kilns

Diame	eters	Number Dequired Per Linear Et									
Inside Lining	Inside Shell	Number Required Per King									
Ft In	Ft In	KA-3	KA-2	KA-1	KA-1X	Total	KA-3	KA-2	KA-1	KA-1X	Total
5 0 5 3 5 6 5 9 6 0 6 3 6 6 6 9	6 0 6 3 6 6 7 0 7 3 7 6 7 9	50 44 38 32 25 19 13 6	7 15 24 32 41 50 58 67			57 59 62 64 66 69 71 73	67 59 51 43 34 26 18 8	10 20 32 43 55 67 78 90			77 79 83 86 89 93 96 98
7 0 7 3 7 6 7 9 8 0 8 3 8 6 8 9 9 0 9 3 9 3 9 6 9 9	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		76 72 68 64 60 56 52 48 44 40 36 33	6 13 19 25 32 38 44 51 57 63 69		76 78 81 83 85 88 90 92 95 95 97 99 102		102 96 91 86 80 75 70 64 59 54 48 44	8 18 26 34 43 51 59 68 76 84 92		102 104 109 112 114 118 121 123 127 130 132 136
$\begin{array}{cccc} 10 & 0 \\ 10 & 3 \\ 10 & 6 \\ 10 & 9 \\ 11 & 0 \\ 11 & 3 \\ 11 & 6 \\ 11 & 9 \\ 12 & 0 \\ 12 & 3 \\ 12 & 6 \\ 12 & 9 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		28 24 21 17 13 9 5 1 	76 82 88 94 100 107 113 119 118 114 111 107		104 106 109 111 113 116 118 120 123 125 128 130		38 32 28 23 18 12 7 1 	102 110 118 126 134 143 151 159 157 152 148 143		140 142 146 149 152 155 158 160 164 167 171 174
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$			104 100 97 93 90 86 82 79 76 72 69 65	28 35 40 46 52 58 64 70 75 82 87 93	132 135 137 139 142 144 146 149 151 154 156 158			139 133 130 124 120 115 110 106 102 96 92 87	37 47 53 62 70 77 85 93 100 110 116 124	176 180 183 186 190 192 195 199 202 206 208 211
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$			62 58 54 51 47 44 40 37 33 30 26 23 19 15 12 8 5 2	99 105 111 123 128 135 140 146 152 158 164 170 176 182 188 193 199	161 163 165 168 170 172 175 177 179 182 184 187 189 191 194 196 198 201			83 78 72 68 63 59 54 49 44 40 35 31 25 20 16 11 7 3	132 140 148 156 164 171 180 187 195 203 211 219 227 235 243 251 257 265	215 218 220 224 227 230 234 236 239 243 246 250 252 255 259 262 262 264 268

NOTE: When using KA - 1x shape, order two pieces each ring KW -  $\frac{2}{3}x$  and KW -  $\frac{3}{4}x$  to facilitate keying.

## COMBINATION LININGS FOR ROTARY KILNS

## Number of KW Blocks Required for Kilns

Diamo	Inside	Number Required Per Ring				Number Required Per Linear Ft					
Ft In	Ft In	KW-3	KW-2	KW-1	KW-1X	Total	KW-3 KW-2 KW-1 KW-1X Tot			Total	
4 6 4 9 5 0 5 3 5 6 5 9	6 0 6 3 6 6 6 9 7 0 7 3	50 44 38 32 25 19	7 15 24 32 41 50			57 59 62 64 66 69	100 88 76 64 50 38	14 30 48 64 82 100			114 118 124 128 132 138
$\begin{array}{ccccc} 6 & 0 \\ 6 & 3 \\ 6 & 6 \\ 6 & 9 \\ 7 & 0 \\ 7 & 0 \\ 7 & 3 \\ 7 & 6 \\ 7 & 9 \\ 8 & 0 \\ 8 & 3 \\ 8 & 6 \\ 8 & 9 \end{array}$	7       6         7       9         8       0         8       3         8       6         8       9         9       0         9       3         9       6         9       9         10       0         10       3	13 6 — — — — — — — — — — —	58 67 72 68 64 60 56 52 48 44 40			71 73 76 78 81 83 85 88 90 92 95 97	26 12 — — — — — — — — — — — — — —	116 134 152 144 136 128 120 112 104 96 88 80			142 146 152 156 162 166 170 176 180 184 190 194
$\begin{array}{cccc} 9 & 0 \\ 9 & 3 \\ 9 & 6 \\ 9 & 9 \\ 10 & 0 \\ 10 & 3 \\ 10 & 6 \\ 10 & 9 \\ 11 & 0 \\ 11 & 3 \\ 11 & 6 \\ 11 & 9 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		36 33 28 24 21 17 13 9 5 1 	63 69 76 82 88 94 100 107 113 119 117 112	    6 13	99 102 104 106 109 111 113 116 118 120 123 125		72 66 56 48 42 34 26 18 10 2 	126 138 152 164 176 188 200 214 226 238 234 224		198 204 208 212 218 222 226 232 236 240 246 250
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$			108 103 98 94 89 84 79 75 70 65 60 56	20 27 34 41 48 55 63 69 76 84 91 98	128 130 132 135 137 139 142 144 146 149 151 154			216 206 196 188 178 168 158 150 140 130 120 112	40 54 68 82 96 110 126 138 152 168 182 196	256 260 264 270 274 278 284 288 292 298 302 308
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccc} 16 & 6 \\ 16 & 9 \\ 17 & 0 \\ 17 & 3 \\ 17 & 6 \\ 17 & 9 \\ 18 & 0 \\ 18 & 3 \\ 18 & 6 \\ 18 & 9 \\ 19 & 0 \\ 19 & 3 \end{array}$			51 46 42 37 32 28 23 18 14 9 4	105 112 119 126 133 140 147 154 161 168 175 182	156 158 161 163 165 168 170 172 175 177 179 182			102 92 84 64 56 46 36 28 18 8 8	210 224 238 252 266 280 294 308 322 336 350 364	312 316 322 326 330 336 340 344 350 354 358 364

NOTE: When using KA - 1x shape, order two pieces each ring KW - 2/3 x and KW - 3/4 x to facilitate keying.

## CR COMBINATION LININGS

CR (Combination Ring) rotary kiln brick are designed to line kilns from 8 to 24 feet in diameter for a 9-inch lining thickness. The appropriate combinations of the two kiln liners are calculated for the best fit for the given diameter.



CR Series Dimensions (Inches)							
SHAPE A B L H							
CR-89	3 <sup>1</sup> / <sub>2</sub>	2 <sup>13</sup> / <sub>16</sub>	6	9			
CR-249	3 <sup>1</sup> / <sub>2</sub>	3 <sup>9</sup> / <sub>32</sub>	6	9			

### Combination Linings - CR Series

Kiln Diameter			
Feet	Meters	CR-89	CR-249
9'-10"	3.00	72	33
10'- 0"	3.04	71	35
10'- 2"	3.10	71	37
10'- 6"	3.20	69	43
10'-10"	3.30	67	48
11'- 0"	3.36	67	50
11'- 2"	3.40	66	53
11'- 6"	3.50	64	58
11'-10"	3.60	63	63
12'- 0"	3.66	61	66
12'- 2"	3.70	61	66
12'- 6"	3.80	59	74
12'-10"	3.90	57	79
13'- 0"	3.96	57	81
13'- 1"	4.00	56	83
13'- 5"	4.10	54	89
13'- 6"	4.12	54	90
13'- 9"	4.20	53	94
14'- 0"	4.26	51	99
14'- 1"	4.30	51	99
14'- 3"	4.34	50	102
14'- 5"	4.40	50	103
14'- 6"	4.42	49	105
14'- 9"	4.50	48	109
15'- 0"	4.58	47	112
15'- 1"	4.60	46	114
15'- 5"	4.70	45	119
15'- 6"	4.72	44	121
15'- 9"	4.80	43	124
16'- 0"	4.88	42	128
16'- 1"	4.90	41	130
16'- 5"	5.00	40	134
16'- 6"	5.02	39	136
16'- 9"	5.10	38	140
17'- 0"	5.18	37	143
17'- 1"	5.20	36	145
17'- 5"	5.30	35	150
17'- 6"	5.34	34	152
17'- 9"	5.40	33	155
18'- 0"	5.48	32	159
18'- 1"	5.50	32	160
18'- 4"	5.60	30	165
18'- 6"	5.64	29	167
18'- 8"	5.70	29	169
19'- 0"	5.80	27	175

To facilitate the keying of wedge-type rotary kiln blocks, keying bricks of two-thirds thickness, RKW-2/3, and of three-quarters thickness, RKW-3/4, are made. Two of each keying brick should be ordered for each ring.

## ISO and VDZ Combination Linings

Standard practice in many North American minerals processing plants is to use one brick of a size manufactured to fit a specific rotary kiln diameter. On the other hand, international practice is to use combination linings. Within practical limits, any rotary kiln can be lined with an appropriate combination of two kiln liners, one of which fits a kiln of larger diameter and the other a kiln of smaller diameter. As good engineering practice, Harbison-Walker suggests brick blending ratios between 3:1 and 1:3 for the two-shapes. This helps to minimize the small amount of stepping which can occur, allowing for a better fit.

The principal advantages of combination linings are:

- In plants which have several kiln sizes, the number of kiln liner shapes can be reduced, since two shapes in appropriate combintions will fit many kilns.
- Liner to liner contact is maintained, while following minor deformations in kiln shells. This results in a tight lining and minimizes the need for correcting shims.



## **International System**



INTERNATIONAL SYSTEM									
		ISO	VDZ						
BACK CHORD	(A)	103	VARIABLE						
INSIDE CHORD	(B)	VARIABLE	VARIABLE						
MIDDLE CHORD	(C)	VARIABLE	71.5						
LENGTH	(L)	198	198						
HEIGHT	(H)	160 180	160 180						
		200	200						
		220	220						
		250	250						
BASIC LINING			Х						
NON-BASIC LINING		Х							

# Schematic diagram showing critical dimensions of ISO and VDZ shapes



dimension is constant at 103mm (4.05")



VDZ brick mean chord (C) dimension is constant at 71.5mm (2.81")



ISO SHAPES										
SHAPE No.		DIMENS	IONS		VOL.	TAPER				
	A	В	Н	L	dm³					
216	103	86	160		2.99	17				
716	103	98.3	100		3.19	4.7				
218	103	84	180		3.33	19				
718	103	97.7				3.58	5.3			
320	103	89	200	198	3.80	21				
820	103	97.8		100	3.98	5.2				
222	103	80			3.99	23				
322	103	88	220		4.16	15				
622	103	95.5	220		4.33	11.5				
822	103	97.3			4.36	5.7				



VDZ SHAPES											
SHAPE No.		DIME	VSIONS		VOL.	TAPER					
	А	В	Н	L	dm³						
B-216	78	65	160		2.27	13					
B-416	75	68	160		2.27	7					
B-218	78	65	180	180		2.55	13				
B-418	75	68			108	2.55	7				
B-220	78	65	200	190	2.83	13					
B-620	74	69	200		2.83	5					
B-222	78	65			3.11	13					
B-322	76.5	66.5	220		3.11	10					
B-622	74	69			3.11	5					

RECOMMENDED LINING THICKNESS								
ROTARY KILN DIAMETER	*RECOMMENDED BRICK THICK							
<3.6M (12'-0") I.D.	160 mm							
Up to 4M (13'-6") I.D.	180 mm							
Up to 4.5M (16'-6") I.D.	200 mm							
Up to 5.8M (19'-0") I.D.	220 mm							
Over 5.8M (19'-0") I.D. 250mm								
*Recommendations are based on kiln diameter only,								

not taking operating data into consideration.

## **RING COMBINATIONS**

## **BRICK COMBINATIONS REQUIRED FOR RINGS**

The tables on the following pages are useful in estimating the quantities of brick required for the construction of circular linings, roofs and arches. These tables give the combinations of brick sizes required for rings of given diameters.

In calculating the tables, no allowance was made for mortar or expansion joints or for size deviations of the brick. Fractional parts equal to or greater than one tenth of a brick were counted as an entire brick. For these reasons, the brick combinations shown may lay up to diameters which differ slightly from the theoretical diameters. The number of brick required for a ring, as given in the tables, may be slightly in excess of the number actually required.

In laying a ring course of brick, it is often necessary to cut one or two pieces, and in some instances several pieces, to complete the ring.

For brick combinations required for rings not shown in the following tables, or to calculate the ring combinations for brick of two different sizes, refer to the formulas found on page 19 which covers ring calculations.



## 4<sup>1</sup>/<sub>2</sub> Inch Lining - 2<sup>1</sup>/<sub>2</sub> Inch Arch Brick 9 x 4<sup>1</sup>/<sub>2</sub> x 2<sup>1</sup>/<sub>2</sub> or 13<sup>1</sup>/<sub>2</sub> x 4<sup>1</sup>/<sub>2</sub> x 2<sup>1</sup>/<sub>2</sub> Inch

Diam.	Inside	N	umber Re	quired per	Ring	
Brick	work	No.3	No.2	No.1	Ctroight	Total
Ft0	in. 6	Arch 10	Arch	Arch	Straight	10121
0	7	18	3	_	_	21
0	8	17	5	—	_	22
0	9	15	8	—	—	23
0	10	14	10	—	—	24
<u> </u>	11	13	13			26
1	1	10	18		_	28
1	2	9	20	_	—	29
1	3	8	23	—	—	31
1	4	7	25	—	—	32
1	5	5	28	—	—	33
1	7	4	33		_	36
1	8	2	35	_	_	37
1	9	_	38	_	_	38
1	10	—	36	3	—	39
	11	—	36	5	—	41
2	0	—	34	8 10	—	42
2	2		31	13	_	43
2	3	_	31	15	—	46
2	4	—	29	18	—	47
2	5	—	28	20	—	48
2	6	—	26	23	—	49
2	/ 8		26 24	25 28	_	51
2	9	_	23	30	_	53
2	10	_	21	33	—	54
2	11	_	20	36	_	56
3	0	—	19	38	—	57
3	1	_	18 16	40 43	_	58 50
3	2		15	43	_	59 61
3	4	_	14	48	_	62
3	5	—	13	50	—	63
3	6	—	11	53	—	64
3	7	—	10	56	—	66 67
3	8		9	58 60	_	67 68
3	10	_	7	63	_	70
3	11	—	5	66	_	71
4	0		4	68		72
4	1	-	3	70	—	73 75
4	2		2	73 76	_	/5 76
4	4			76	1	77
4	6		_	76	4	80
4	8	—	—	76	6	82
4	10			76	9	85
5	0		_	76 76	11 14	87 90
5	2 4			76	14	92
5	6	_		76	19	95
5	8	—	—	76	21	97
5	10	—	—	76	24	100

## $4^{1}/_{2}$ Inch Lining - $2^{1}/_{2}$ Inch Arch Brick 9 x $4^{1}/_{2}$ x $2^{1}/_{2}$ or $13^{1}/_{2}$ x $4^{1}/_{2}$ x $2^{1}/_{2}$ Inch

Diam. I	nside	Number Required per Ring				
Brick	work	No.3	No.2	No.1		
Ft.	ln.	Arch	Arch	Arch	Straight	Total
6	0	_	_	76	26	102
6	2	_	_	76	29	105
6	4	_	_	76	31	107
6	6	_	_	76	34	110
6	8	_	_	76	36	112
6	10	_	_	76	39	115
7	0	_	_	76	41	117
7	2	_	_	76	44	120
7	4	_		76	46	120
7	6	_	_	76	40	125
7	8	_		76	51	127
7	10	_		76	5/	130
8	0			76	56	132
0	2			76	50	125
0	~			76	61	100
0	+ 6			76	61	140
0	0	_	_	70	66	140
0	10	_	_	70	60	142
0	0			76	71	145
9	2			76	7/	147
0	4			76	74	150
0	6			76	70	155
9	8			76	81	155
9	10	_	_	70	01	160
10	0		_	76	04 97	162
10	2			76	80	165
10	4			76	03	168
10	6			76	92	170
10	8	_		76	97	173
10	10	_	_	76	99	175
11	0	_	_	76	102	178
11	2	_	_	76	102	180
11	4	_	_	76	107	183
11	6	_	_	76	109	185
11	8	_	_	76	112	188
11	10	_	_	76	114	190
12	0	_	_	76	117	193
12	2	_	_	76	119	195
12	4	_	_	76	122	198
12	6	_	_	76	124	200
12	8	_	_	76	127	203
12	10	_	_	76	129	205
13	0	_	_	76	132	208
13	2	_	_	76	134	210
13	4	_	_	76	137	213
13	6	_	_	76	139	215
13	8	_	—	76	142	218
13	10	_		76	144	220
14	0	_	_	76	147	223
14	2	—	—	76	149	225
14	4	—	—	76	152	228
14	6	—	—	76	154	230
14	8	—	—	76	157	233
14	10			76	159	235
15	0	—	_	76	162	238

## 9 Inch Lining - 2<sup>1</sup>/<sub>2</sub> Inch Wedge Brick

## 9 Inch Lining - 21/2 Inch Wedge Brick 9 x 4<sup>1</sup>/<sub>2</sub> x 2<sup>1</sup>/<sub>2</sub>, 9 x 6<sup>3</sup>/<sub>4</sub> x 2<sup>1</sup>/<sub>2</sub> or 9 x 9 x 2<sup>1</sup>/<sub>2</sub> Inch 9 x 4<sup>1</sup>/<sub>2</sub> x 2<sup>1</sup>/<sub>2</sub>, 9 x 6<sup>3</sup>/<sub>4</sub> x 2<sup>1</sup>/<sub>2</sub> or 9 x 9 x 2<sup>1</sup>/<sub>2</sub> Inch

Diam.	Inside	Number Required per Ring				
Brick	work	No.2	No.1	No.1-X		
Ft.	ln.	Wedge	Wedge	Wedge	Straight	Total
2	3	57	_	_	_	57
2	4	55	3	_	_	58
2	5	52	7	_	_	59
2	6	51	10	_	_	61
2	7	48	14	_	_	62
2	8	46	17	_	_	63
2	a	40	20	_	_	64
2	10	12	20	_	_	66
2	11	42	24			67
- 2		20	20			69
2	1	26	24			70
2	2	24	27	_	_	70
2	2	20	40	_	_	71
3	3	00	40	_	_	72
3	4	29	44	_	_	73
3	5	20	47	_	_	75
3	6	25	51	_	_	76
3	/	23	54	_	_	77
3	8	21	5/	_	_	78
3	9	19	61	—	—	80
3	10	17	64	—	—	81
3	11	15	67	_	_	82
4	0	13	70	—	—	83
4	1	11	74	—	-	85
4	2	9	77	—	_	86
4	3	6	81	—	_	87
4	4	4	84	—	—	88
4	5	2	88	—	—	90
4	6	—	91	—	—	91
4	7	_	90	2	_	92
4	8	_	89	4	_	93
4	9	—	88	7	—	95
4	10	—	87	9	—	96
4	11	—	86	11	—	97
5	0	_	85	13	—	98
5	1	—	85	15	—	100
5	2	_	84	17	—	101
5	3	_	83	19	—	102
5	4	_	82	21	_	103
5	5	_	82	23	—	105
5	6	_	81	25	_	106
5	7	_	80	27	_	107
5	8	_	79	29	_	108
5	9	_	78	32	_	110
5	10	_	77	34	_	111
5	11	_	76	36	_	112
6	0	_	75	38	_	113
6	1	_	75	40	_	115
6	2	_	74	42	_	116
6	3	_	73	44	_	117
6	4	_	72	47	_	119
6	5	_	72	48	_	120
6	6	_	71	50	_	121
6	7	_	70	52	_	122
6	8	_	69	55	_	124
6	9	_	68	57	_	125
6	10		67	59	_	126
ő	11		66	61	_	127
v	••	I				

Diam.	Inside	N	Number Required per Ring			
Brick	work	No.2	No.1	No.1-X	<u> </u>	<b>.</b>
<u> </u>	in.	vveage	vveage	weage	Straight	100
7	1	_	65	63 65	_	129
7	2		64	67		130
7	3	_	63	69	_	132
7	4	_	62	72	_	134
7	5	_	61	74	_	135
7	6	—	60	76	—	136
7	7	—	59	78	—	137
7	8	—	59	80	—	139
7	9	—	58	82	—	140
7	10	—	57	84	—	141
7	11	—	56	86	—	142
8	0	—	56	88	—	144
8	1	_	55	90	—	145
8	2	_	54	92	_	140
o S	3 ∕	_	53 52	94 07	_	14/
0 8	4 5		52	97		149
8	5		50	101		150
8	7			103		152
8	8	_	40	105	_	154
8	9	_	48	107	_	155
8	10	_	47	109	_	156
8	11	_	46	111	_	157
9	0	_	46	113	_	159
9	1	_	45	115	—	160
9	2	_	44	117	_	161
9	3	_	43	120	—	163
9	4	—	42	122	—	164
9	5	—	41	124	—	165
9	6	—	40	126	—	166
9	7	—	40	128	—	168
9	8	—	39	130	—	169
9	9		38	132	—	170
9	10	—	37	134	—	171
9	11		36	137		1/3
10	U 1	_	35 25	139	_	175
10	1 2		20	140		176
10	2		33	142		178
10	4	_	32	147	_	179
10	5	_	31	149	_	180
10	6	_	30	151	_	181
10	7	_	30	153	_	183
10	8	_	29	155	_	184
10	9	_	28	157	_	185
10	10	—	27	159		186
10	11	—	26	162	—	188
11	0	_	25	164	—	189
11	1	—	24	166	—	190
11	2	—	23	168	—	191
11	3	—	23	170	—	193
11	4	—	22	172	—	194
11	5		21	174		195

## 9 Inch Lining - 2<sup>1</sup>/<sub>2</sub> Inch Wedge Brick 9 x 4<sup>1</sup>/<sub>2</sub> x 2<sup>1</sup>/<sub>2</sub>, 9 x 6<sup>3</sup>/<sub>4</sub> x 2<sup>1</sup>/<sub>2</sub> or 9 x 9 x 2<sup>1</sup>/<sub>2</sub> Inch

Diam.	Inside	N	Number Required per Ring			
Brick	work	No.2	No.1	No.1-X		
Ft.	ln.	Wedge	Wedge	Wedge	Straight	Total
11	6	_	20	176	_	196
11	7	_	20	178	_	198
11	8	—	19	180	—	199
11	9	—	18	182	—	200
11	10	—	17	184	—	201
11	11	—	16	187	—	203
12	0	—	15	189	—	204
12	1	-	14	191	—	205
12	2	-	13	193	—	206
12	3	-	13	195	—	208
12	4	—	12	197	—	209
12	5	-	11	199	—	210
12	6	-	10	202	—	212
12	7	-	10	203	—	213
12	8	-	9	205	—	214
12	9	—	8	207	—	215
12	10	—	7	210	—	217
12	11		6	212	—	218
13	0	—	5	214	—	219
13	1	—	4	216	—	220
13	2	-	4	218	—	222
13	3	—	3	220	—	223
13	4	—	2	222	—	224
13	5	-	1	224	—	225
13	6	-	—	227	—	227
13	7	-	—	227	1	228
13	8	-	—	227	2	229
13	9	-	—	227	3	230
13	10	-	—	227	5	232
13	11	—	_	227	6	233
14	0	-	—	227	7	234
14	6	-	—	227	15	242
15	0	-	—	227	22	249
15	6	-	—	227	30	257
16	0	-	—	227	37	264
16	6		_	227	45	2/2
1/	0	-	—	227	52	2/9
1/	6		—	227	60	287
10	0	_	—	227	6/ 75	294
10	р О	_	—	227	/5	302
19	U C	_	—	227	00	310
19	ю	-	—	227	90	317

## 9 Inch Lining - 2<sup>1</sup>/<sub>2</sub> Inch Wedge Brick 9 x 4<sup>1</sup>/<sub>2</sub> x 2<sup>3</sup>/<sub>4</sub>, 9 x 6<sup>3</sup>/<sub>4</sub> x 2<sup>1</sup>/<sub>2</sub> or 9 x 9 x 2<sup>1</sup>/<sub>2</sub> Inch

Diam.	Inside	N	umber Red	quired per	Ring	
Brick	work	No 2				
Enor	In.	Wedge	Wedge	Wedge	Straight	Total
20	0			227	08	325
20	6			227	105	332
20	0			227	112	240
21	6	_	_	227	120	247
21	0	_	_	227	120	347
22	0	_	_	227	120	300
	0	_	_	227	135	302
23	0	_	_	227	143	370
23	6	—	—	227	150	377
24	0	—	—	227	158	385
24	6	_	—	227	165	392
25	0	_	—	227	173	400
25	6	—	—	227	181	408
26	0	—	—	227	188	415
26	6	—	—	227	196	423
27	0	—	—	227	203	430
27	6	—	—	227	211	438
28	0	—	—	227	218	445
28	6	_	—	227	226	453
29	0	_	—	227	233	460
29	6	—	—	227	241	468
30	0	_	-	227	248	475
30	6	—	—	227	256	483
31	0	_	—	227	263	490
31	6	—	—	227	271	498
32	0	_	—	227	279	506
32	6	_	_	227	286	513
33	0	_	—	227	294	521
33	6	_	—	227	301	528
34	0	_	—	227	309	536
34	6	_	_	227	316	543
35	0	_	_	227	324	551
35	6	_	_	227	331	558
36	õ	_	_	227	339	566
36	õ	_	_	227	346	573
37	õ	_	_	227	354	581
37	6	_	_	227	362	589
38	õ	_	_	227	369	596
38	6			227	377	604
39	0			227	384	611
30	6			207	302	610
40	0			227	399	626
40	6			207	407	634
/1	0			207	407 417	6/1
	6			221	414	6/0
41	0		_	221	422	656
42	0 E			227	429	664
42	0		_	227	437	671
43	0		—	227	444	0/1
43	6		—	227	452	6/9
	0		—	227	460	08/
44	6	-	—	227	467	694
45	0	-	—	227	475	702

## **RING COMBINATIONS**

## 41/2 Inch Lining — 3 Inch Arch Brick 9 x 41/2 x 3 or 131/2 x 41/2 x 3 Inch

Diam. Inside	Number Required Per Ring					
Brickwork Ft In	No. 4 Arch	No. 3 Arch	No. 2 Arch	No. 1 Arch	Straight	Total
$\begin{array}{cccc} 0 & 4^{1}/_{2} \\ 0 & 5 \\ 0 & 6 \\ 0 & 7 \\ 0 & 8 \\ 0 & 9 \\ 0 & 10 \\ 0 & 11 \end{array}$	15 14 13 12 11 10 8 7	1 3 5 7 9 12 14				15 15 16 17 18 19 20 21
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	6 5 4 3 1 	16 18 20 22 24 27 29 28 26 25 24 23				22 23 24 26 27 28 29 30 31 32 33 34
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		22 21 20 19 18 17 16 15 14 13 12 10	13 15 17 21 23 25 27 29 31 33 36			35 36 37 38 39 40 41 42 43 44 45 46
3         0           3         1           3         2           3         3           3         4           3         5           3         6           3         7           3         8           3         9           3         10           3         11		10 9 8 7 6 5 3 2 1 	38 40 42 44 46 48 51 53 55 57 56 55			48 49 50 51 52 53 54 55 56 57 58 59
4 0 4 1 4 2 4 3 4 4 4 5			54 52 51 50 49 48	6 9 11 13 15 17		60 61 62 63 64 65

## 41/2 Inch Lining — 3 Inch Arch Brick 9 x 41/2 x 3 or 131/2 x 41/2 x 3 Inch — Continued

Diam. Inside	Number Required Per Ring					
Brickwork Ft In	No. 4 Arch	No. 3 Arch	No. 2 Arch	No. 1 Arch	Straight	Total
4 6 4 7 4 8 4 9 4 10 4 11			47 46 45 44 43 42	19 21 23 26 28 30	 	66 67 68 70 71 72
5       0         5       1         5       2         5       3         5       4         5       5         5       6         5       7         5       8         5       9         5       10         5       11			41 40 39 38 37 36 35 34 33 32 31 29	32 34 36 38 40 42 44 46 48 50 52 55		73 74 75 76 77 78 79 80 81 82 83 84
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			28 27 26 25 24 23 22 21 20 19 18 17	57 59 61 63 65 67 70 72 74 76 78 80		85 86 87 88 89 90 92 93 94 95 96 97
7         0           7         1           7         2           7         3           7         4           7         5           7         6           7         7           8         7           7         10           7         11			16 15 14 13 12 11 10 9 7 6 5 4	82 84 86 90 92 94 96 99 101 103 105		98 99 100 101 102 103 104 105 106 107 108 109
8 0 8 1 8 2 8 3 8 6			3 2 1 	107 109 111 113 113	   4	110 111 112 113 117
9         0           10         0           11         0           12         0           13         0           14         0           15         0	- - - - -			113 113 113 113 113 113 113 113	10 22 35 48 60 73 85	123 135 148 161 173 186 198

## 41/2 Inch Lining — 3 Inch Circle Brick 9 x 41/2 x 3 Inch

Diam. Inside	Number Required Per Ring					-
Brickwork Ft In	24-33-3 Circle	36-45-3 Circle	48-57-3 Circle	60-69-3 Circle	72-81-3 Circle	Total
2 0 2 1 2 2 2 3 2 4 2 5 2 6 2 7 2 8 2 9 2 10 2 11	12 11 10 9 8 7 6 5 4 3 2 1	1 3 4 5 7 8 9 11 12 13 15				12 12 13 13 14 14 14 15 15 15 16
3         0           3         1           3         2           3         3           3         4           3         5           3         6           3         7           3         8           3         9           3         10           3         11		16 14 13 12 11 9 8 7 5 4 3 2	2 4 5 7 9 10 12 14 15 17 18			16 16 17 17 18 18 18 18 19 19 19 20 20
$\begin{array}{ccccccc} 4 & 0 \\ 4 & 1 \\ 4 & 2 \\ 4 & 3 \\ 4 & 4 \\ 4 & 5 \\ 4 & 6 \\ 4 & 7 \\ 4 & 8 \\ 4 & 9 \\ 4 & 10 \\ 4 & 11 \end{array}$			20 19 17 15 14 12 10 9 7 5 4 2	2 4 6 8 10 12 14 16 18 20 22		20 21 21 22 22 22 23 23 23 23 23 24 24
$\begin{array}{ccccc} 5 & 0 \\ 5 & 1 \\ 5 & 2 \\ 5 & 3 \\ 5 & 4 \\ 5 & 5 \\ 5 & 6 \\ 5 & 7 \\ 5 & 8 \\ 5 & 9 \\ 5 & 10 \\ 5 & 11 \end{array}$		- - - - - - - - - - - - - - - - - - -		24 22 20 18 16 14 12 10 8 6 4 2		24 25 25 26 26 26 27 27 27 27 28 28 28

## 41/2 Inch Lining — 3 Inch Circle Brick 9 x 41/2 x 3 Inch — Continued

Diam	Inside	Number Required Per Ring					
Brick Ft	work In	72-81-3 Circle	84-93-3 Circle	96-105-3 Circle	108-117-3 Circle	120-129-3 Circle	Total
6 6 6 6 6 6 6 6 6 6	0 1 2 3 4 5 6 7 8 9	29 26 24 22 19 16 14 12 9 7					29 29 29 30 30 30 31 31 31 31 32 22
6	10	3	30	_	_	_	32 33
7 7 7 7 7 7 7 7 7 7 7 7	0 1 2 3 4 5 6 7 8 9 10 11		33 30 27 25 22 19 16 14 11 8 5 3	3 7 9 12 16 19 21 25 28 31 34			33 34 34 35 35 35 35 36 36 36 36 37
8 8 8 8 8 8 8 8 8 8 8 8 8 8	0 1 2 3 4 5 6 7 8 9 10 11			37 34 31 28 24 22 18 15 12 9 7 3			37 37 38 38 38 39 39 39 40 40 40 41 41
9 9 9 9 9 9 9 9 9 9 9	0 1 2 3 4 5 6 7 8 9 10 11				41 38 34 31 28 24 20 17 14 10 7 4		41 42 42 43 43 43 43 43 44 44 44 45 45
10	0	_	_	_	_	45	45

## 6 Inch Lining — 3 Inch Arch Brick $12 \times 6 \times 3$ or $13^{1/2} \times 6 \times 3$ Inch

Brickwork         No. 3         No. 2         No. 1         Arch         No. 1         Arch         Total           2         0         38            38           2         1         37         2           39           2         2         36         4           40           2         3         35         6           41           2         4         34         8           42           2         5         32         11           43           2         6         31         13           44           2         7         30         15           46           2         9         29         19           48           2         10         28         21          51           3         1         24         28          55           3         5         20         36          55	Diam. Inside	Number Required Per Ring				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Brickwork Ft In	No. 3 Arch	No. 2 Arch	No. 1 Arch	Straight	Total
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 0	38	_	_	_	38
2       2       36       4       -       -       40         2       3       35       6       -       -       41         2       4       34       8       -       -       42         2       5       32       11       -       -       43         2       6       31       13       -       -       44         2       7       30       15       -       -       44         2       7       30       15       -       -       46         2       9       29       19       -       -       46         2       9       29       19       -       -       48         2       10       28       21       -       -       50         3       1       24       28       -       -       52         3       3       22       32       32       -       -       51         3       1       24       28       -       -       55       3       5       20       36       -       -       56         3       3       12	2 1	37	2	_	_	39
2       3       35       6       -       -       41         2       4       34       8       -       -       42         2       5       32       11       -       -       43         2       6       31       13       -       -       44         2       7       30       15       -       -       45         2       8       29       17       -       -       46         2       9       29       19       -       -       48         2       10       28       21       -       -       49         2       11       27       23       -       -       50         3       0       26       25       -       -       51         3       1       24       28       -       -       55         3       2       23       30       -       -       55         3       5       20       36       -       -       55         3       6       19       38       -       -       58         3       8       17 <td>2 2</td> <td>36</td> <td>-</td> <td>_</td> <td>_</td> <td>40</td>	2 2	36	-	_	_	40
2       4       34       8         42         2       5       32       11         43         2       6       31       13         44         2       7       30       15         45         2       8       29       17         46         2       9       29       19         48         2       10       28       21         49         2       10       28       21         50         3       0       26       25         51         3       1       24       28         55         3       2       23       30         54         3       3       32       22       32         55         3       5       20       36         56         3       7       18       40         57	2 2	35	6	_	_	/1
2       3       0       -       -       42         2       5       32       11       -       -       43         2       6       31       13       -       -       44         2       7       30       15       -       -       45         2       8       29       17       -       -       46         2       9       29       19       -       -       48         2       10       28       21       -       -       48         2       10       28       21       -       -       50         3       0       26       25       -       -       51         3       1       24       28       -       -       52         3       3       322       33       0       -       54         3       4       21       34       -       -       55         3       5       20       36       -       -       56         3       6       19       38       -       -       58         3       9       16       44 </td <td>2 5</td> <td>34</td> <td>8</td> <td></td> <td></td> <td>42</td>	2 5	34	8			42
2       3       32       11         43         2       6       31       13        44         2       7       30       15         44         2       7       30       15         44         2       9       29       17         48         2       10       28       21         49         2       11       27       23         50         3       0       26       25         51         3       1       24       28        -50         3       3       22       32        -       54         3       4       21       34        -       56         3       5       20       36        -       57         3       7       18       40        -       58         3       8       17       42        -       66         3       9       16 <t< td=""><td>2 4</td><td>27</td><td>11</td><td>_</td><td>_</td><td>42</td></t<>	2 4	27	11	_	_	42
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 5	32	12	_		43
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 0	31	15	_		44
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 1	30	15	_	_	45
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 8	29	17	_	_	40
2       10       28       21         49         2       11       27       23         50         3       0       26       25         51         3       1       24       28         53         3       2       23       30         54         3       4       21       34         55         3       5       20       36         56         3       6       19       38         58         3       8       17       42         59         3       9       16       44         60         3       10       15       46         61         3       11       14       48         62         4       0       13       50         64         4       2       11       54         67         4	2 9	29	19	_	_	48
2       11       27       23       —       —       50         3       0       26       25       —       —       51         3       1       24       28       —       —       52         3       2       23       30       —       —       54         3       4       21       34       —       —       55         3       5       20       36       —       —       56         3       6       19       38       —       —       55         3       6       19       38       —       —       56         3       6       19       38       —       —       55         3       7       18       40       —       —       58         3       8       17       42       —       —       60         3       10       15       46       —       —       62         4       0       13       50       —       —       64         4       1       12       52       —       —       65         4       3       9 <td>2 10</td> <td>28</td> <td>21</td> <td>_</td> <td>_</td> <td>49</td>	2 10	28	21	_	_	49
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 11	27	23	_	_	50
3       1       24       28         52         3       2       23       30         53         3       3       22       32         54         3       4       21       34         56         3       5       20       36         56         3       6       19       38         57         3       7       18       40         58         3       8       17       42         60         3       10       15       46         61         3       11       14       48         62         4       0       13       50         64         4       1       12       52         64         4       2       11       54         65         4       3       9       57         66         4	3 0	26	25	_	_	51
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 1	24	28	—	—	52
3       3       22       32         54         3       4       21       34         55         3       5       20       36         56         3       6       19       38         58         3       6       19       38         58         3       8       17       42         59         3       8       17       42         60         3       10       15       46         61         3       11       14       48         62         4       0       13       50         63         4       1       12       52         64         4       3       9       57         66         4       3       9       57         67         4       4       8       59         70         4	3 2	23	30	-	-	53
3       4       21       34         55         3       5       20       36         56         3       6       19       38         57         3       7       18       40         58         3       8       17       42         59         3       9       16       44         60         3       10       15       46         61         3       11       14       48         62         4       0       13       50         63         4       1       12       52         64         4       2       11       54         65         4       3       9       57         66         4       4       8       59         67         4       5       67         70       4         4	3 3	22	32	-	-	54
3       5       20       36         56         3       6       19       38         57         3       7       18       40         58         3       8       17       42         59         3       9       16       44         60         3       10       15       46         61         3       11       14       48         62         4       0       13       50         63         4       1       12       52         64         4       2       11       54         65         4       3       9       57         66         4       4       8       59         67         4       5       7       61         71         4       6       7       63        72       7         4 <t< td=""><td>3 4</td><td>21</td><td>34</td><td>-  </td><td>-  </td><td>55</td></t<>	3 4	21	34	-	-	55
3       6       19       38         57         3       7       18       40         58         3       8       17       42         59         3       9       16       44         60         3       10       15       46         61         3       11       14       48         62         4       0       13       50         63         4       1       12       52         64         4       2       11       54         66         4       3       9       57         66         4       4       8       59         66         4       4       8       59         67         4       5       7       61         71         4       6       7       63        72       7         4 <td< td=""><td>3 5</td><td>20</td><td>36</td><td>-  </td><td>-  </td><td>56</td></td<>	3 5	20	36	-	-	56
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 6	19	38	_	_	57
3       8       17       42         59         3       9       16       44         60         3       10       15       46         61         3       11       14       48         62         4       0       13       50         63         4       1       12       52         64         4       2       11       54         65         4       3       9       57         66         4       4       8       59         67         4       5       7       61         68         4       6       7       63        71       72         4       9       4       69        73       73         4       10       2       72        74       74         4       11       1       74        75       2        77	3 7	18	40	_	_	58
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 8	17	42	_	_	59
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 9	16	44	_	_	60
3       11       14       48       -       -       62         4       0       13       50       -       -       63         4       1       12       52       -       -       64         4       2       11       54       -       -       65         4       3       9       57       -       -       66         4       4       8       59       -       -       66         4       4       8       59       -       -       67         4       5       7       61       -       -       67         4       5       67       -       -       70       70         4       7       6       65       -       -       71         4       8       5       67       -       -       72         4       9       4       69       -       -       73         4       10       2       72       -       -       76         5       1       -       75       2       -       77         5       2       -	3 10	15	46	_	_	61
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 11	14	48	_	_	62
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4 0	13	50	_	_	63
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4 1	12	52	_	_	64
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4 2	11	54	_	_	65
4       4       8       59         67         4       5       7       61         68         4       6       7       63         70         4       7       6       65         71         4       8       5       67         72         4       9       4       69         73         4       10       2       72         74         4       11       1       74        75       75         5       0        75       2        76         5       1        75       2        77         5       2        774       4        78         5       3        72       7        79         5       4        71       9        80	4 3	9	57	_	_	66
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4 4	8	59	_	_	67
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4 5	7	61	_	_	68
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4 6	7	63	_	_	70
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4 7	6	65	_	_	71
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1 8	5	67	_	_	72
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4 0	1	69			72
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4 10	2	72			73
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4 11	1	74	_	_	75
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	5 0	_	76			76
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5 1		75	2	_	73
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5 7		7/	2 1		78
5   4   71   9   80	5 2		72	7		70
	5 1		71	0	_	80
	5 4 5 5		70	7		00 81
	5 5		40	12		ο1 Ω2
	5 7	-	60	15	-	02
$\begin{bmatrix} 0 & 1 \\ 5 & 0 \end{bmatrix} = \begin{bmatrix} 00 \\ 47 \end{bmatrix} \begin{bmatrix} 10 \\ 17 \end{bmatrix} = \begin{bmatrix} 83 \\ 04 \end{bmatrix}$	J /	-	00 47	10	_	03
	о 8 Е 0	-	0/	1/		04 ог
	D 9	-	00	19	_	00
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5 10 5 11		64	23		00 87
	6 0		40	25		00
	0 U 6 1	-	40	20	-	00
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		-	61	21	_	07
	0 Z			29	_	90
$\begin{bmatrix} 0 & 3 \\ 4 & 4 \end{bmatrix} = \begin{bmatrix} 00 \\ 50 \\ 24 \end{bmatrix} = \begin{bmatrix} 92 \\ 00 \\ 00 \end{bmatrix}$	0 J		0U E0	32	_	92
	o 4	-	59	34		93
$\begin{vmatrix} 0 & 5 & - & 58 & 36 & - & 94 \\ ( & ( & 1 & 57 & 58 & 36 & - & 94 \\ ( & 1 & 57 & 58 & 56 & - & 57 & 56 \\ ( & 1 & 1 & 58 & 56 & - & 57 & 56 & 56 \\ ( & 1 & 1 & 1 & 58 & - & 58 & - & 56 \\ ( & 1 & 1 & 1 & 58 & - & 58 & - & 56 \\ ( & 1 & 1 & 1 & 58 & - & 58 & - & 56 \\ ( & 1 & 1 & 1 & 58 & - & 58 & - & 56 \\ ( & 1 & 1 & 1 & 1 & - & 58 & - & 56 \\ ( & 1 & 1 & 1 & 1 & - & 58 & - & 56 \\ ( & 1 & 1 & 1 & 1 & - & 58 & - & 56 \\ ( & 1 & 1 & 1 & - & 58 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 58 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 58 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & 1 & - & 56 \\ ( & 1 & 1 & 1 & - & 56 & - & 56 \\ ( & 1 & 1 & 1 & -$	6 5		58	36	-	94
	6 6 ( 7	-	5/	38	-	95 07
o / 56 40 96	o /		56	40		90

## 6 Inch Lining — 3 Inch Arch Brick 12 x 6 x 3 or 13<sup>1</sup>/<sub>2</sub> x 6 x 3 Inch — Continued

Diam.	. Inside	Number Required Per Ring				
Brick Ft	work In	No. 3 Arch	No. 2 Arch	No. 1 Arch	Straight	Total
6 6 6	8 9 10 11	  	55 54 53 52	42 44 46 48		97 98 99 100
7 7 7 7 7 7 7 7 7 7 7 7	0 1 2 3 4 5 6 7 8 9 10 11		51 49 48 47 46 45 44 43 42 41 40 39	50 53 55 57 59 61 63 65 67 69 71 73		101 102 103 104 105 106 107 108 109 110 111 112
8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	0 1 2 3 4 5 6 7 8 9 10 11		38 37 36 35 34 33 32 31 30 29 27 26	75 78 80 82 84 86 88 90 92 92 94 97 99		113 115 116 117 118 119 120 121 122 123 124 125
9 9 9 9 9 9 9 9 9 9 9	0 1 2 3 4 5 6 7 8 9 10 11		25 24 23 22 21 20 19 18 17 16 15 14	101 103 105 107 109 111 113 115 117 119 122 124		126 127 128 129 130 131 132 133 134 135 137 138
10 10 10 10 10 10 10 10 10 10 10 10	0 1 2 3 4 5 6 7 8 9 10 11		13 12 11 10 9 8 7 5 4 3 2 1	126 128 130 132 134 136 138 141 143 145 147 149		139 140 141 142 143 144 145 146 147 148 149 150
11 12 13 14	0 0 0 0			151 151 151 151	— 13 25 38	151 164 176 189

## 6 Inch Lining — Rotary Kiln or Cupola Blocks 9 x 6 x 4 Inch

Diam.	. Inside	Number Required Per Ring						
Brick Ft	work In			Total				
4 4 4 4 4 4	6 7 8 9 10 11	<b>54-66</b> 23 20 15 11 8 4	60-72 4 9 13 17 21	23 24 24 24 25 25				
5 5 5 5 5 5 5	0 1 2 3 4 5	60-72 26 21 17 13 9 4	66-78 	26 26 27 27 27 27				
5 5 5 5 5 5	6 7 8 9 10 11	66-78 28 23 18 14 9 5	<b>72-84</b> 5 10 15 20 24	28 28 28 29 29 29 29				
6 6 6 6 6	0 1 2 3 4 5	<b>72-84</b> 30 25 20 15 10 5	<b>78-90</b> 	30 30 30 31 31 31				
6 6 6 6 6	6 7 8 9 10 11	<b>78-90</b> 32 26 21 16 11 6	84-96 — 6 12 17 22 28	32 32 33 33 33 33 34				
7 7 7 7 7 7 7	0 1 2 3 4 5	84-96 34 28 23 17 11 6	<b>90-102</b> 	34 34 35 35 35 36				
7 7 7 7 7 7 7	6 7 8 9 10 11	<b>90-102</b> 36 30 24 18 12 6	<b>96-108</b> 	36 36 37 37 37 38				
8 8 8 8 8 8	0 1 2 3 4 5	96-108 38 31 25 19 13 7	<b>102-114</b> 7 14 20 26 33	38 38 39 39 39 40				

#### Number Required Per Ring Diam. Inside Brickwork Total Ft In 102-114 108-120 108-120 114-126 114-126 120-132 \_ 120-132 123-135 \_ 123-135 126-138

### 6 Inch Lining — Rotary Kiln or Cupola Blocks 9 x 6 x 4 Inch — Continued

NOTE: In orders, the complete names of the blocks desired should be given, as for example "102-114 RKB" or "102-114 Cupola."

126-138

132-144

132-144

138-150

NOTE: In orders, the complete names of the blocks desired should be given, as for example "54-66 RKB" or "60-72 Cupola."

6	Inch Lining —	<b>Rotary Kiln or Cupola Blocks</b>
9	x 6 x 4 Inch —	Continued

Diam. Inside Number Required Per Ring				
Brick	work			<b>.</b>
Ft	In			Total
		138-150	144-156	
11	6	53	_	53
11	7	44	9	53
11	8	35	18	53
11	9	26	28	54
11	10	18	36	54
11	11	9 46		55
		144-156	150-162	
12	0	55	_	55
12	1	45	10	55
12	2	37	19	56
12	3	27	29	56
12	4	18	38	56
12	5	9	48	57
		150-162	156-168	
12	6	57	—	57
12	7	47	10	57
12	8	38	20	58
12	9	28	30	58
12	10	19	39	58
12	11	10	49	59
		156-168	162-174	
13	0	59	_	59
13	1	49	10	59
13	2	39	21	60
13	3	29	31	60
13	4	20	40	60
13	5	10	51	61
		162-174	168-180	
13	6	61	—	61
13	7	51	10	61
13	8	41	21	62
13	9	30	32	62
13	10	21	42	63
13	11	10	53	63
		168-180	174-186	
14	0	63	—	63
14	1	53	11	64
14	2	42	22	64
14	3	31	33	64
14	4	21	44	65
14	5	11	54	65

# 6 Inch Lining — Rotary Kiln or Cupola Blocks 9 x 6 x 4 Inch — Continued

Diam	. Inside	Number Required Per Ring				
Bric	kwork					
Ft	In			lotal		
		174-186	180-192			
14	6	65	_	65		
14	7	54	12	66		
14	8	43	23	66		
14	9	32	34	66		
14	10	22	45	67		
14	11	11	56	67		
		180-192	186-198			
15	0	67	_	67		
15	1	56	12	68		
15	2	45	23	68		
15	3	33	35	68		
15	4	23	46	69		
15	5	11	58	69		
		196 100	102 204			
15	6	70	172-204	70		
10	0	70	10	70		
15	/	30	12	70		
15	ð	40	24	70		
15	9	30	30	71		
15	10	23	48	/		
15	11	12	59	/1		
		192-204	198-210			
16	0	72	—	72		
16	1	60	12	72		
16	2	48	24	72		
16	3	36	37	73		
16	4	24	49	73		
16	5	12	61	73		
		198-210	204-216			
16	6	74	_	74		
16	7	61	13	74		
16	8	49	25	74		
16	9	37	38	75		
16	10	25	50	75		
16	11	12	63	75		
		204-216	210-222			
17	0	76		76		

NOTE: In orders, the complete names of the blocks desired should be given, as for example "174-186 RKB" or "174-186 Cupola."

NOTE: In orders, the complete names of the blocks desired should be given, as for example "138-150 RKB" or "138-150 Cupola."

Inside		Insi	de		Numbe	r Required	Per Ring	
Lin Ft	ing In	She Ft	ell In	KW-3	KW-2	KW-1	KW-1X	Total
5 5 5 6 6 6	0 3 6 9 0 3 6 9	6 6 7 7 7 7	0 3 6 9 0 3 6 9	50 44 38 32 25 19 13 6	7 15 24 32 41 50 58 67			57 59 62 64 66 69 71 73
7 7 7 8 8 8 8 8 8 9 9 9 9 9	0 3 6 9 0 3 6 9 0 3 6 9 9	8 8 8 9 9 9 9 9 9 9 10 10 10 10	0 3 6 9 0 3 6 9 0 3 6 9		76 72 68 64 60 56 52 48 44 40 36 33			76 78 81 83 85 88 90 92 95 97 97 99 102
10 10 10 11 11 11 11 12 12 12 12 12	0 3 6 9 0 3 6 9 0 3 6 9	11 11 11 12 12 12 12 12 12 12 13 13 13 13 13	0 3 6 9 0 3 6 9 0 3 6 9		28 24 21 17 13 9 5 1 — —	76 82 88 94 100 107 113 119 118 114 111 107		104 106 109 111 113 116 118 120 123 125 128 130
13 13 13 14 14 14 14 15 15 15 15 15	0 3 6 9 0 3 6 9 0 3 6 9	14 14 14 15 15 15 15 16 16 16 16	0 3 6 9 0 3 6 9 0 3 6 9			104 100 97 93 90 86 82 79 76 72 69 65	28 35 40 46 52 58 64 70 75 82 87 93	132 135 137 142 144 146 149 151 154 156 158
16 16 16 17 17 17 17 18 18	0 3 6 9 0 3 6 9 0 3	17 17 17 18 18 18 18 18 18 19 19	0 3 6 9 0 3 6 9 0 3			62 58 54 51 47 44 40 37 33 30	99 105 111 117 123 128 135 140 146 152	161 163 165 168 170 172 175 177 179 182

## 6 Inch Lining — Rotary Kiln Blocks 9 x 6 x 4 Inch Arch Type — Two Shape System

## 9 Inch Lining — 3 Inch Wedge Brick 9 x 4<sup>1</sup>/<sub>2</sub> x 3, 9 x 6 <sup>3</sup>/<sub>4</sub> x 3 or 9 x 9 x 3 Inch

Diam	Inside		Numbe	er Required Pe	er Ring	
Brick Ft	kwork In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	Straight	Total
3	0	57	_	_	_	57
3	1	56	2	_	_	58
3	2	55	4	_	_	59
3	3	54	6	_	_	60
3	4	52	9	_	_	61
3	5	51	11	_	_	62
3	6	50	13	_	_	63
3	7	49	15	_	_	64
3	8	48	17	_	_	65
3	9	47	19	_	_	66
3	10	46	21	_	_	67
3	11	45	23	_	_	68
4	0	44	26			70
4	1	43	28	_	-	71
4	2	42	30	—	_	72
4	3	41	32	_	_	73
4	4	40	34	_	_	/4
4	5	39	30	_	_	/5
4	0	38	38	_	_	/0 77
4	0	26	40	_	_	77
4	0	30	42			70
4	10	34	46			80
4	11	33	48	_	_	81
5	0	32	50	_	_	82
5	1	31	52	_	_	83
5	2	29	55	_	_	84
5	3	28	57	_	_	85
5	4	27	59	_	_	86
5	5	26	61	—	—	87
5	6	25	63	_	-	88
5	7	24	65	—	_	89
5	8	23	67	_	_	90
5	9	22	/0	_	_	92
5 5	10	21	72	_	_	93 94
6	0	10	76	_	_	05
6	1	18	78			96
6	2	17	80	_		97
6	3	16	82	_	_	98
6	4	15	84	_	_	99
6	5	14	86	_	_	100
6	6	13	88	_	_	101
6	7	12	90	-	-	102
6	8	11	92	-	_	103
6	9	10	94	-	-	104
6	10	9	96	-	-	105
6	11	7	99	-	-	106

NOTE: This table can be used also for 13<sup>1</sup>/2 x 9 x 3 inch arch brick by substituting Nos. 1, 2 and 3 arch brick for the corresponding wedge brick.

NOTE: For each ring, order two (2) pieces each KA- $^{2}\!/_{3}$  and KA- $^{3}\!/_{4}$  to facilitate

keying. For additional information, see discussion of KA and KW Blocks for Rotary Kilns.

## 9 Inch Lining — 3 Inch Wedge Brick 9 x 41/2 x 3, 9 x 63/4 x 3 or 9 x 9 x 3 Inch-Cont'd.

Diam	. Inside		Numbe	er Required Pe	er Ring	
Bricl Ft	kwork In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	Straight	Total
7	0	6	101	_	_	107
7	1	5	103	_	_	108
7	2	4	105	_	_	109
7	3	3	107	_	_	110
7	4	2	109	_	_	111
7	5	1	111	_	_	112
7	6	_	113	_	_	113
7	7	_	112	3	_	115
7	8	_	111	5	_	116
7	9	—	110	7	—	117
7	10	_	109	9	-	118
7	11	_	108	11	—	119
8	0	_	107	13	_	120
8	1	_	106	15	-	121
8	2	_	105	17	-	122
8	3	_	104	19	-	123
8	4	_	103	21	_	124
8	5	_	102	23	_	125
8	0	_	101	25	_	120
8	/	_	100	27	_	127
8	ð	_	99	29	_	128
0	9	_	9/	32	_	129
0	10	_	90	26	_	130
8	11		95	30		131
9	0	-	94	38	-	132
9	1	—	93	40	—	133
9	2	—	92	42	—	134
9	3	—	91	44	-	135
9	4	-	90	47	-	137
9	5	—	89	49	-	138
9	6	—	88	51	-	139
9	7	—	87	53	-	140
9	8	_	86	55	-	141
9	9 10	-	85	5/	-	142
9	10	_	84	59	_	143
9	11	_	83	61	_	144
10	0	-	82	63 65	_	145
10	ו כ	_	01 00	00 67	_	140
10	2	_	3U 70	0/ 40	_	147
10	3 4	_	79	09 71	_	14ŏ 140
10	4 5	_	70 77	73	_	147
10	5		76	75		150
10	7		70	79		151
10	, 8		73	80		153
10	9		73	82		153
10	10		71	8/		154
10	11	_	70	86		156
10						.50

## 9 Inch Lining — 3 Inch Wedge Brick 9 x 41/2 x 3, 9 x 63/4 x 3 or 9 x 9 x 3 Inch-Cont'd.

Diam.	Inside		Numb	er Required Pe	er Ring	
Brick Ft	work In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	Straight	Total
11 11 11 11 11 11 11 11 11 11 11	0 1 2 3 4 5 6 7 8 9 10 11		69 67 66 65 64 63 62 61 60 59 58	88 90 93 95 97 99 101 103 105 107 109 111		157 159 160 161 162 163 164 165 166 167 168 169
12 12 12 12 12 12 12 12 12 12 12 12 12 1	0 1 2 3 4 5 6 7 8 9 10 11		57 56 55 52 51 50 49 48 47 47 45	113 115 117 122 124 126 128 130 132 134 137		170 171 172 173 174 175 176 177 178 179 181 182
13 13 13 13 13 13 13 13 13 13 13 13 13	0 1 2 3 4 5 6 7 8 9 10 11		44 43 42 41 40 39 38 37 36 35 34 33	139 141 143 145 147 151 153 155 157 159 161		183 184 185 186 187 188 189 190 191 192 193 194
14 14 14 14 14 14 14 14 14 14 14 14 14	0 1 2 3 4 5 6 7 8 9 10 11		32 30 29 28 27 26 25 25 25 23 22 21 20	163 166 168 170 172 174 176 178 181 183 185 187		195 196 197 198 199 200 201 203 204 205 206 207
15 15 15 15 15 15	0 1 2 3 4 5		19 18 17 16 15 14	189 191 193 195 197 199	 	208 209 210 211 212 213

15 5 —

NOTE: This table can be used also for  $13^{1/2} x 9 x 3$  inch arch brick by substituting Nos. 1, 2 and 3 arch brick for the corresponding wedge brick.

NOTE: This table can be used also for  $13^{1/2} x 9 x 3$  inch arch brick by substituting Nos. 1, 2 and 3 arch brick for the corresponding wedge brick.

## 9 Inch Lining — 3 Inch Wedge Brick

Diam	Inside		Number Required Per Ring							
Brick Ft	work In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	Straight	Total				
15	6	_	13	201	_	214				
15	7	_	12	203	_	215				
15	8	_	11	205	_	216				
15	9	_	10	207	_	217				
15	10	_	8	210	_	218				
15	11	_	7	212	—	219				
16	0	_	6	214	_	220				
16	1	_	5	216	_	221				
16	2	_	4	218	—	222				
16	3	_	3	220	—	223				
16	4	_	3	222	_	225				
16	5	_	1	225	-	226				
16	6	_	—	227	_	227				
17	0	_	—	227	6	233				
17	6	_	—	227	12	239				
18	0	_	—	227	18	245				
18	6	_	—	227	25	252				
19	0	_	-	227	31	258				
19	6	_	—	227	37	264				
20	0	_	_	227	44	271				
20	6	_	-	227	50	277				
21	0	_	_	227	56	283				
21	6	_	_	227	62	289				
22	0	_	_	227	69	296				
22	6	_	_	227	75	302				
23	0	_	—	227	81	308				
23	6	_	—	227	88	315				
24	0	_	—	227	94	321				
24	6	_	—	227	100	327				
25	0	_	-	227	106	333				
25	6	_	—	227	113	340				
26	0	_	—	227	119	346				
26	6	_	—	227	125	352				
27	0	_	—	227	132	359				
27	6	_	—	227	138	365				
28	0	_	—	227	144	371				
28	6	-	-	227	150	377				
29	0	-	-	227	157	384				
29	6	_	—	227	163	390				
30	0	_	_	227	169	396				
30	6	-	-	227	176	403				
31	0	-	-	227	182	409				
31	6	-	-	227	188	415				
32	0	-	-	227	194	421				
32	6	-	-	227	201	428				
33	0	-	-	227	207	434				
33	6	-	-	227	213	440				
34	0	-	-	227	220	447				
34	6	-	-	227	226	453				
35	0	-	-	227	232	459				
35	6	-	-	227	238	465				
36	0	-	-	227	245	472				
36	6	-	-	227	251	478				

## 9 x 4<sup>1</sup>/<sub>2</sub> x 3, 9 x 6<sup>3</sup>/<sub>4</sub> x 3 or 9 x 9 x 3 Inch–Cont'd.

### 9 Inch Lining — 3 Inch Key Brick 9 x 4<sup>1</sup>/<sub>2</sub> x 3 Inch

Diam.	Inside		Nu	umber Requ	ired Per Rin	g	
Brick Ft	work In	No. 4 Key	No. 3 Key	No. 2 Key	No. 1 Key	Straight	Total
1 1 1	6 8 10	26 23 20	4 8	  	  		26 27 28
2 2 2 2 2 2 2	0 2 4 6 8 10	17 14 12 9 6 3	13 17 21 25 29 34				30 31 33 34 35 37
3 3 3 3 3 3	0 2 4 6 8 10		38 35 32 29 27 24	4 9 13 17 21		       	38 39 41 42 44 45
4 4 4 4 4 4	0 2 4 6 8 10	  	21 18 15 13 10 7	25 30 34 38 42 46		 	46 48 49 51 52 53
5 5 5 5 5 5 5 5	0 2 3 4 6 8 10		4 1 	51 55 57 56 55 53 52	  4 7 10		55 56 57 58 59 60 62
6 6 6 6 6	0 2 4 6 8 10			50 49 48 46 45 43	13 16 18 21 24 27	       	63 65 66 67 69 70
7 7 7 7 7 7	0 2 4 6 8 10	 		42 41 39 38 36 35	30 32 35 38 41 44	     	72 73 74 76 77 79
8 8 8 8 8	0 2 4 6 8 10			34 32 31 29 28 27	46 49 52 55 58 60		80 81 83 84 86 87
9 9 9 9 9	0 2 4 6 8 10			25 24 22 21 20 18	63 66 69 72 74 77	 	88 90 91 93 94 95
10 10 10	0 2 4	 	 	17 15 14	80 83 86	_ _ _	97 98 100

NOTE: This table can be used also for  $13^{1/2} \times 9 \times 3$  inch arch brick by substituting Nos. 1, 2 and 3 arch brick for the corresponding wedge brick.

### 9 Inch Lining — 3 Inch Key Brick 9 x 41/2 x 3 Inch — Continued

Diam. I	nside		Nu	ımber Requ	ired Per Rir	ıg	
Brickv Ft	vork In	No. 4 Key	No. 3 Key	No. 2 Key	No. 1 Key	Straight	Total
10 10 10	6 8 10			13 11 10	88 91 94		101 102 104
11 11 11 11 11 11 11	0 2 4 6 8 10			9 7 6 4 3 2	96 100 102 105 108 110		105 107 108 109 111 112
12 12 13 13 14 14	0 6 0 6 0 6				113 113 113 113 113 113 113	5 9 13 17 21	113 118 122 126 130 134
15 15 16 16 17 17	0 6 0 6 0 6				113 113 113 113 113 113 113	26 30 34 38 42 47	139 143 147 151 155 160
18 18 19 19 20 20	0 6 0 6 0 6				113 113 113 113 113 113 113	51 55 59 63 68 72	164 168 172 176 181 185
21 21 22 22 23 23 23	0 6 0 6 0 6				113 113 113 113 113 113 113	76 80 84 88 93 97	189 193 197 201 206 210
24 24 25 25 26 26	0 6 0 6 0 6	 		 	113 113 113 113 113 113 113	101 105 109 114 118 122	214 218 222 227 231 235
27 27 28 28 29 29	0 6 0 6 0 6	  	  		113 113 113 113 113 113 113	126 130 135 139 143 147	239 243 248 252 256 260
30 30 31 31 32 32	0 6 0 6 0 6				113 113 113 113 113 113 113	151 155 160 164 168 172	264 268 273 277 281 285
33 33 34 35	0 6 0 0		 		113 113 113 113 113	176 181 185 193	289 294 298 306

## 9 Inch Lining — 3 Inch Key Brick 9 x 6 x 3 Inch

Diam. Inside	Number Required Per Ring							
Brickwork Ft In	No. 3 Key	No. 2 Key	No. 1 Key	Straight	Total			
1 6 1 8 1 10	19 18 18	 2 3	  		19 20 21			
2 0 2 2 2 4 2 6 2 8 2 10	17 16 15 15 14 14	5 7 9 11 13 14	  	 	22 23 24 26 27 28			
3 0 3 2 3 4 3 6 3 8 3 10	13 12 12 11 10 9	16 18 19 21 23 25	       		29 30 31 32 33 34			
4 0 4 2 4 4 4 6 4 8 4 10	9 8 7 7 6 5	26 28 30 31 33 35	  	- - - -	35 36 37 38 39 40			
5 0 5 2 5 4 5 6 5 8 5 10	5 4 3 2 2 1	36 38 40 42 43 45	  	     	41 42 43 44 45 46			
6 0 6 2 6 4 6 6 6 8 6 10	  	48 47 46 45 44 43	 2 4 6 8 10	       	48 49 50 51 52 53			
7 0 7 2 7 4 7 6 7 8 7 8 7 10		41 40 39 38 37 36	13 15 17 19 21 23		54 55 56 57 58 59			
8 0 8 2 8 4 8 6 8 8 8 10	  	34 33 32 31 30 28	26 28 30 32 34 37	 	60 61 62 63 64 65			
9 0 9 2 9 4 9 6 9 8 9 10	  	27 26 25 24 23 22	39 41 43 46 48 50	  	66 67 68 70 71 72			

\*NOTE: For brickwork of inside diameters less than 6 feet, involving the use of 9 x 6 inch No. 3 Keys which have a very sharp taper, a better bricklaying fit can be obtained by the use of the 9 x 4<sup>1</sup>/<sub>2</sub> inch Key-brick combinations.

## 9 Inch Lining — 3 Inch Key Brick 9 x 6 x 3 Inch — Continued

Diam.	Inside		Numb	er Required Pe	er Ring	
Brick Ft	work In	No.3 Key	No. 2 Key	No. 1 Key	Straight	Total
10 10 10 10 10 10	0 2 4 6 8 10	  	21 19 18 17 16 15	52 55 57 59 61 63	  	73 74 75 76 77 78
11 11 11 11 11 11	0 2 4 6 8 10	 	13 12 11 10 9 8	66 68 70 72 74 76		79 80 81 82 83 84
12 12 12 12 12 12 12 12	0 2 4 6 8 10		6 5 4 3 2	79 81 83 85 87 90		85 86 87 88 89 90
13 13 14 14 15 15	0 6 0 6 0 6	   		91 91 91 91 91 91		91 95 98 101 104 107
16 16 17 17 18 18	0 6 0 6 0 6			91 91 91 91 91 91	19 22 26 29 32 35	110 113 117 120 123 126
19 20 21 22 23 24	0 0 0 0 0			91 91 91 91 91 91 91	38 44 51 57 63 70	129 135 142 148 154 161
25 26 27 28 29 30	0 0 0 0 0	  		91 91 91 91 91 91	76 82 88 95 101 107	167 173 179 186 192 198
31 32 33 34 35 36	0 0 0 0 0		  	91 91 91 91 91 91	114 120 126 132 139 145	205 211 217 223 230 236
37 38 39 40 41	0 0 0 0 0	  	 	91 91 91 91 91 91	151 158 164 170 176	242 249 255 261 267

### 9 Inch Lining — Rotary Kiln Blocks 9 x 9 x 4 Inch

Diam	. Inside	Number Required Per Ring				
Brick Ft	kwork In			Total		
_		60-78	66-84			
5	0	28	_	28		
5	1	23	5	28		
5	2	18	10	28		
5	3	14	15	29		
5	4	9	20	29		
5	5	5	24	29		
		66-84	72-90			
5	6	30	—	30		
5	7	25	5	30		
5	8	20	10	30		
5	9	15	16	31		
5	10	10	21	31		
5	11	5	26	31		
		72-90	78-96			
6	0	32	_	32		
6	1	26	6	32		
6	2	21	12	33		
6	3	16	17	33		
6	4	11	22	33		
6	5	6	28	34		
		78-96	84-102			
6	6	34	_	34		
6	7	28	6	34		
6	8	23	12	35		
6	9	17	18	35		
6	10	11	24	35		
6	11	6	30	36		
		82-102	90-108			
7	0	36	_	36		
7	1	30	6	36		
7	2	24	13	37		
7	3	18	19	37		
7	4	12	25	37		
7	5	6	32	38		
		90-108	96-114			
7	6	38	_	38		
7	7	31	7	38		
7	8	25	14	39		
7	9	19	20	39		
7	10	13	26	39		
7	11	7	33	40		

NOTE: In orders, the complete names of the blocks should be given, as for example "60-78 RKB."

## 9 Inch Lining — Rotary Kiln Blocks 9 x 9 x 4 Inch — Continued

Diam	. Inside	Number Required Per Ring					
Bric	kwork			Total			
- FL	111						
		96-114	102-120				
8	0	40	—	40			
8	1	34	7	41			
8	2	27	14	41			
8	3	20	21	41			
8	4	14	28	42			
8	5	7	35	42			
		102-120	108-126				
8	6	42	_	42			
8	7	35	8	43			
8	8	28	15	43			
8	9	21	22	43			
8	10	14	30	44			
8	11	7	37	44			
		108-126	114-132				
9	0	44	—	44			
9	1	37	8	45			
9	2	29	16	45			
9	3	22	23	45			
9	4	15	31	46			
9	5	7	39	46			
		114-132	117-135				
9	6	46	_	46			
9	7	31	16	47			
9	8	15	32	47			
		117-135	120-138				
9	9	48		48			
9	10	32	16	48			
9	11	16	32	48			
Ĺ,				10			
		120-138	123-141				
10	0	49	—	49			
10	1	32	17	49			
10	2	16	13	49			
1				1			

NOTE: In orders, the complete names of the blocks should be given, as for example "84-102 RKB."

## 9 Inch Lining — Rotary Kiln Blocks 9 x 9 x 4 Inch — Continued

Diam.	. Inside	Number Required Per Ring				
Brick	work			Total		
Ft	In			Total		
		123-141	126-144			
10	3	50	—	50		
10	4	33	17	50		
10	5	16	34	50		
		126-144	132-150			
10	6	51	_	51		
10	7	42	9	51		
10	8	34	17	51		
10	9	25	27	52		
10	10	17	35	52		
10	11	8	44	52		
		132-150	138-156			
11	0	53	-	53		
11	1	44	9	53		
11	2	35	18	53		
11	3	26	28	54		
11	4	18	36	54		
11	5	9	46	55		
		138-156	144-162			
11	6	55	_	55		
11	7	45	10	55		
11	8	37	19	56		
11	9	27	29	56		
11	10	18	38	56		
11	11	9	48	57		
		144-162	150-168			
12	0	57	—	57		
12	1	47	10	57		
12	2	38	20	58		
12	3	28	30	58		
12	4	19	39	58		
12	5	10	49	59		
		150-168	156-174			
12	6	59	-	59		
12	7	49	10	59		
12	8	39	21	60		
12	9	29	31	60		
12	10	20	40	60		
12	11	10	51	61		
		156-174	162-180			
13	0	61		61		
13	1	51	10	61		
13	2	41	21	62		
13	3	30	32	62		
13	4	21	42	63		
13	5	10	53	63		

NOTE: In orders, the complete names of the blocks should be given, as for example "123-141 RKB."

## 9 Inch Lining — Rotary Kiln Blocks 9 x 9 x 4 Inch — Continued

Diam.	Inside	Number Required Per Ring				
Brick	work			Total		
Ft	In			Total		
		162-180	168-186			
13	6	63	_	63		
13	7	53	11	64		
13	8	42	22	64		
13	9	31	33	64		
13	10	21	44	65		
13	11	11	54	65		
		1/0 10/	174 100			
14	0	100-100	1/4-192			
14	0	00		C0		
14	1	54	12	66		
14	2	43	23	66		
14	3	32	34	66		
14	4	22	45	67		
14	5	11	56	67		
		174-192	180-198			
14	6	67	_	67		
14	7	56	12	68		
14	8	45	23	68		
14	0	33	35	68		
14	7	33	30	00		
14	10	23	40	69		
14	11	11	58	69		
		180-198	186-204			
15	0	70	_	70		
15	1	58	12	70		
15	2	46	24	70		
15	3	35	36	71		
15	4	23	48	71		
15	5	12	59	71		
		186-204	192-210			
15	6	72	_	72		
15	7	60	12	72		
10	0	40	24	72		
10	0	40	24	12		
15	9 10	30	3/	13		
15	10	24	49	73		
15	11	12	61	/3		
		192-210	198-216			
16	0	74	—	74		
16	1	61	13	74		
16	2	49	25	74		
16	3	37	38	75		
16	4	25	50	75		
16	5	12	63	75		
		198-216	204-222			
16	6	76		76		
10	7	42	12	70		
10	,	U3 E0	13	10		
10	0	00	20	/0		
16	9	38	39	11		
16	10	25	52	/7		
16	11	13	65	78		

## 9 Inch Lining — Rotary Kiln Blocks 9 x 9 x 4 Inch — Continued

Diam	. Inside	Number Required Per Ring				
Brick Ft	work In			Total		
		204-222	210-228			
17	0	78	—	78		
17	1	65	13	78		
17	2	52	27	79		
17	3	39	40	79		
17	4	26	53	79		
17	5	13	67	80		
		210-228	216-234			
17	6	80	_	80		
17	7	66	14	80		
17	8	53	28	81		
17	9	40	41	81		
17	10	27	54	81		
17	11	14	68	82		
		216-234	222-240			
18	0	82	_	82		
18	1	68	14	82		
18	2	55	28	83		
18	3	41	42	83		
18	4	27	56	83		
18	5	14	70	84		
		222-240	228-246			
18	6	84	_	84		
18	7	70	15	85		
18	8	56	29	85		
18	9	42	43	85		
18	10	28	58	86		
18	11	14	72	86		
		228-246	234-252			
19	0	86	—	86		
19	1	72	15	87		
19	2	57	30	87		
19	3	43	44	87		
19	4	29	59	88		
19	5	14	74	88		
		234-252	240-258			
19	6	88		88		
10	7	74	15	80		
10	, 8	59	30	80		
10	9	11	45	80		
10	, 10	30	-5	07 QA		
19	11	15	75	90		
		240-258	—			
20	0	90	-	90		
-						

NOTE: In orders, the complete names of the blocks should be given, as for example "204-222 RKB."

NOTE: In orders, the complete names of the blocks should be given, as for example "162-180 RKB."

## 9 Inch Lining — Rotary Kiln Blocks 9 x 6 x 4 Inch Wedge Type —Two Shape System

Ins	side	Ins	side		Numbe	er Required	Per Ring	
Lir Ft	ning In	Sł Ft	nell In	KW-3	KW-2	KW-1	KW-1X	Total
4	6	6	0	50	7	_	_	57
4	9	6	3	44	15	_	_	59
5	0	6	6	38	24	-	_	62
5	3	6	9	32	32	-	_	64
5	6	7	0	25	41	-	_	66
5	9	/	3	19	50	-	_	69
6	0	7	6	13	58	-	_	71
6	3	7	9	6	67	-	_	73
6	6	8	0	-	/6	_	-	/6
6	9	8	3	-	12	12	_	/8
7	0 3	8	0		64	10		83
7	6	9	0		60	25		85
7	9	9	3	_	56	32	_	88
8	0	9	6	-	52	38	_	90
8	3	9	9	_	48	44	_	92
8	6	10	0	_	44	51	_	95
8	9	10	3	-	40	57	_	97
9	0	10	6	_	36	63	_	99
9	3	10	9	-	33	69	_	102
9	6	11	0	-	28	76	-	104
9	9	11	3	-	24	82	_	106
10	0	11	6	-	21	88	_	109
10	3	11	9	-	1/	94	-	111
10	0	12	3	-	13	100	_	113
10	9	12	5	-	5	107	_	110
11	3	12	9		1	119		120
11	6	13	0	_		117	6	123
11	9	13	3	-	_	112	13	125
12	0	13	6	_	_	108	20	128
12	3	13	9	_	_	103	27	130
12	6	14	0	_	_	98	34	132
12	9	14	3	_	_	94	41	135
13	0	14	6	-	-	89	48	137
13	3	14	9	-	-	84	55	139
13	6	15	0	-	-	79	63	142
13	9	15	3	-	-	/5	69	144
14	3	15	0	-		70	2/0	140
14	5	16	7			60	91	147
14	9	16	3	_	_	56	98	154
15	0	16	6	_	_	51	105	156
15	3	16	9	_	_	46	112	158
15	6	17	0	_	_	42	119	161
15	9	17	3	_	_	37	126	163
16	0	17	6	_	_	32	133	165
16	3	17	9	-	-	28	140	168
16	6	18	0	-	-	23	147	170
16	9	18	3	-	-	18	154	172
17	0	18	6	-	-	14	161	175
17	3	18	9	-	-	9	168	177
17	0	19	0	-		4	1/5	1/9
	7	19	ა	-	-		102	102

NOTE: For each ring, order two (2) pieces each KW-2/3 and KW-3/4 to facilitate keying. For additional information, see discussion of KA and KW blocks for Rotary Kilns.

## 12 Inch Lining — 3 Inch Wedge Brick 12 x 4<sup>1</sup>/<sub>2</sub> x 3, 12 x 6 x 3 or 12 x 9 x 3 Inch

Brickwork         No. 3         No. 2         No. 1         No. 1         No. 1X         Wedge         No. 1X         Wedge         Total           4         0         76         -         -         -         -         -         79           4         0         76         -         -         -         -         -         79           4         0         66         19         -         -         -         -         85           5         0         63         25         -         -         -         -         95           5         0         54         44         -         -         -         -         95           6         0         51         50         -         -         -         -         101           6         0         51         50         -         -         -         101	Diam	Inside		Nu	ımber Requ	ired Per Rin	ıg	
4       0       76            78         4       6       66       19           85         5       0       63       25          89         5       3       60       32          99         5       6       57       38          99         6       0       51       50          101         6       6       44       63          101         6       6       44       63          101         7       0       38       75          110         7       3       35       82          123         8       0       25       101          129         8       3       22       107          132         9       0       13<	Brick	work	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Straight	Total
4       3       72       7       -       -       -       -       79       82         5       0       66       19       -       -       -       -       -       88         5       0       63       25       -       -       -       -       -       88         5       6       57       38       -       -       -       -       -       99         6       0       51       50       -       -       -       -       101         6       3       47       57       38       75       -       -       -       -       101         7       3       35       82       -       -       -       -       113         7       6       32       88       75       -       -       -       -       120         8       0       25       101       -       -       -       -       120       122         8       9       16       119       -       -       -       133       132       -       -       -       133        9       0       13	4	0	76	_	_	_	_	76
4       6       669       13           82         5       0       63       25           99         5       9       54       44           99         6       0       51       50           101         6       3       47       57           101         6       3       47       57          101         6       3       47       57          101         6       9       41       69          110         7       3       35       82          120         7       6       32       88          121         8       0       25       101          129         8       9       13       126          148	4	3	72	7	_	_	_	79
4       9       66       19          85         5       0       63       25           92         5       6       57       38           95         6       0       51       50           101         6       3       44       63          113         6       9       44       69          110         6       9       44       69          123         7       0       38       75          123         8       0       25       101          126         8       3       25       107         132       126         129         8       0       151          133       135       135       135       145        151         9       0	4	6	69	13	_	_	_	82
5         0         63         25         -         -         -         -         -         -         92         95           5         9         54         44         -         -         -         -         92         95           6         0         51         50         -         -         -         -         101           6         3         47         57         -         -         -         -         101           6         9         41         69         -         -         -         -         113           7         0         38         75         -         -         -         -         113           7         6         32         88         -         -         -         123           8         0         22         107         -         -         -         123           8         0         22         107         -         -         -         132           9         0         13         126         -         -         -         132           9         3         145         -         -	4	9	66	19	—	_	_	85
5       3       60       32           92       95         5       9       54       44           92       95         6       0       51       50           101         6       6       9       41       69          113         7       0       38       75           113         7       0       38       75           120         7       9       29       94          121       122         8       0       25       101          122       123         8       9       16       132       126          132       135         9       0       13       126          142       145         9       3       105       132          151	5	0	63	25	_	_	_	88
5       6       57       38           95       98         6       0       51       50           101         6       3       47       57           101         6       9       41       69           113         7       0       38       75           113         7       0       38       22       107          120         7       9       29       94          121         8       0       25       101          122         8       9       16       119          132         9       0       13       126          142         9       3       100       122         145         9       3       145         151	5	3	60	32	_	_	_	92
5       9       54       44       -       -       -       99         6       0       51       50       -       -       -       -       101         6       3       47       57       -       -       -       -       104         6       6       44       63       -       -       -       -       107         6       9       41       69       -       -       -       -       113         7       0       38       75       -       -       -       -       113         7       0       32       88       22       -       -       -       120         7       9       29       94       -       -       -       120       120         8       0       25       101       -       -       -       129       132         8       0       13       126       -       -       -       139       142         9       6       7       138       -       -       144       13       -       -       142         9       9       3 <td< td=""><td>5</td><td>6</td><td>57</td><td>38</td><td>_</td><td>_</td><td>_</td><td>95</td></td<>	5	6	57	38	_	_	_	95
6         0         51         50             101           6         3         47         57             104           6         6         44         63             110           7         0         38         75            113           7         3         35         82            123           8         0         25         101            124           8         9         16         119            123           9         0         13         126            132           9         0         13         126            142           9         6         7         138           142           9         6         7         138           151           10	5	9	54	44	_	_	_	98
6 $3$ $47$ $57$ $    104$ $6$ $9$ $41$ $69$ $    107$ $6$ $9$ $41$ $69$ $    110$ $7$ $0$ $38$ $75$ $    111$ $7$ $9$ $29$ $94$ $   120$ $7$ $9$ $29$ $94$ $   122$ $8$ $0$ $25$ $101$ $   122$ $8$ $9$ $16$ $119$ $   132$ $9$ $0$ $13$ $126$ $    142$ $9$ $6$ $7$ $138$ $   142$ $9$ $3$ $145$ $   1414$ $10$	6	0	51	50				101
6       6       44       63          107         6       9       41       69          110         7       0       38       75          113         7       3       35       82          117         7       6       32       88          120         7       9       29       94          124         8       0       25       101          125         8       9       16       119          132         8       9       16       119          134         9       3       105          151         10       0        151         154         10       0        133        164         10       0        135       32         157	6	3	47	57	_	_	_	104
6       9       41       69       -       -       -       10         7       0       38       75       -       -       -       -       111         7       0       32       88       -       -       -       -       117         7       6       32       88       -       -       -       -       123         8       0       25       101       -       -       -       -       129         8       6       19       113       -       -       -       -       129         8       6       19       113       -       -       -       139         9       0       13       126       -       -       -       139         9       3       10       132       -       -       -       142         9       6       7       138       -       -       -       144         10       3       -       144       13       -       -       151         10       3       -       148       6       -       -       161         11	6	6	44	63	_	_	_	107
7       0       38       75       -       -       -       -       113         7       3       35       82       -       -       -       -       117         7       6       32       88       -       -       -       -       117         7       9       29       94       -       -       -       -       123         8       0       25       101       -       -       -       -       126         8       3       22       107       -       -       -       -       129         8       6       19       113       -       -       -       132         9       0       13       126       -       -       -       133         9       0       13       126       -       -       -       142         9       6       7       138       -       -       -       144         10       0       -       151       -       -       -       151         10       3       -       142       19       -       161         111	6	9	41	69	_	_	_	110
7       3       35       82          117         7       6       32       88          120         8       0       25       101          124         8       3       22       107          129         8       6       19       113          132         8       9       16       119          139         9       0       13       126          142         9       6       7       138         144         10       0        151         144         10       0        151         161         11       0        139       25         164         11       0        122       57        167       167         11       0        126       50	7	0	38	75	_	_	_	113
7       6       32       88          120         7       9       29       94         123         8       0       25       101         124         8       3       22       107         129         8       6       19       113         132         8       9       16       119         139         9       3       10       132          142         9       6       7       138          144         9       9       3       145         151         10       0        151         151         10       3        148       6        151         10       3        151         164         11       3        139       25         167         111       9        122<	7	3	35	82	_	_	_	117
7       9       29       94         123         8       0       25       101         126         8       3       22       107         129         8       6       19       113         129         8       9       16       119         135         9       0       13       126          139         9       3       10       132         142       142         9       6       7       138         141       142         9       6       7       138         142       151         10       0        151         151       151         10       6        144       13        157       157         10       9        129       44         164         11       3        122       57       -        170	7	6	32	88	_	_	_	120
8         0         25         101         -         -         -         -         126           8         3         22         107         -         -         -         129           8         6         19         113         -         -         -         132           9         0         13         126         -         -         -         142           9         6         7         138         -         -         -         142           9         6         7         138         -         -         -         142           9         9         3         145         -         -         -         142           10         0         -         151         -         -         -         151           10         3         -         144         13         -         157         164           11         0         -         139         25         -         -         167           11         6         -         122         38         -         -         170           11         9         -         126 <td>7</td> <td>9</td> <td>29</td> <td>94</td> <td>_</td> <td>_</td> <td>_</td> <td>123</td>	7	9	29	94	_	_	_	123
8       3       22       107          129         8       6       19       113          132         9       0       13       126          139         9       3       10       132          142         9       6       7       138          145         9       9       3       145          145         10       0        151          151         10       6        144       13        154         10       6        144       13        161         11       0        139       25         164         11       3        132       38        170       170         11       6        122       57        -       176         12       3        120       63	8	0	25	101				126
8       6       19       113          132         9       0       13       126          139         9       3       10       132          142         9       6       7       138          145         9       9       3       145          145         10       0        151          151         10       3        148       6         151         10       6        144       13        151         10       9        132       38        164         11       3        132       38        170         11       6        122       57        176         12       3        120       63         189         12       9        107       88	8	3	22	107	_	_	_	129
8       9       16       119          135         9       0       13       126          142         9       6       7       138          142         9       6       7       138          142         9       6       7       138          142         10       0        151          151         10       6        144       13         151         10       6        144       13         161         11       0        139       25         164         11       3        129       44        170       173         12       0        126       50         176         12       3        120       63         189         13       0	8	6	19	113	_	_	_	132
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	9	16	119	_	-	_	135
9       3       10       132          142         9       6       7       138          145         9       9       3       145          145         10       0        151          151         10       3        148       6         151         10       6        144       13        157         10       6        142       19        161         11       0        139       25         164         11       3        135       32         167         11       6        129       44         170         11       9        126       50         176         12       3        120       63        179       183         12       9        107       88       <	9	0	13	126	_	_	_	139
9       6       7       138           145         10       0        151          151         10       3        148       6         151         10       6        144       13         157         10       9        142       19         161         11       0        139       25         164         11       3        132       38         167         11       6        120       50         166         12       0        126       50         176         12       0        120       63         183         12       9        113       76         192         13       0        113       76         192         13       9	9	3	10	132	_	_	_	142
9       9       3       145          148         10       0        151          151         10       3        148       6         154         10       6        144       13         157         10       9        142       19         161         11       0        139       25         164         11       3        132       38         167         11       6        122       57         176         12       0        126       50         176         12       3        120       63         183         12       9        113       76         192         13       0        113       76         192         13       9	9	6	7	138	_	_	_	145
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	9	9	3	145	—	_	_	148
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	0	_	151	_	_	_	151
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	3	_	148	6	_	_	154
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	6	-	144	13	_	_	157
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	9	-	142	19	_	—	161
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	0	_	139	25	_	_	164
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	3	_	135	32	_	_	167
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	6	_	132	38	-	_	170
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	11	9	-	129	44	_	_	173
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	12	0	_	126	50	_	_	176
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	12	3	-	122	57	-	-	179
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	12	6	-	120	63	_	_	183
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	12	9	_	117	69	_	_	186
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	13	0	_	113	76	_	_	189
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	13	3	-	110	82	-	-	192
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	13	6	-	107	88	-	-	195
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	13	9		104	94			198
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	14	0	_	101	100	_	_	201
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	14	3	-	98	107	-	-	205
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	14	6	-	95	113	-	-	208
15         0          88         126           214           15         3          85         132           217           15         6          82         138           220           15         9          79         144           223	14	9	-	91	120			211
15         3         -         85         132         -         217           15         6         -         82         138         -         -         220           15         9         -         79         144         -         -         223	15	0	_	88	126	_	_	214
15         6          82         138           220           15         9          79         144           223	15	3	-	85	132	-	-	217
15 9 — 79 144 — — 223	15	6	-	82	138	-	-	220
	15	9	-	79	144	-	-	223

## 12 Inch Lining — 3 Inch Wedge Brick 12 x 41/2 x 3, 12 x 6 x 3 or 12 x 9 x 3 Inch–Cont'd.

Diam.	Inside	Number Required Per Ring					
Brick Ft	work In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Straight	Total
16	0	_	76	151	_	_	227
16	3	-	73	157	_	_	230
16	6	-	69	164	_	_	233
16	9	-	66	170	_	—	236
17	0	_	63	176	_	_	239
17	3	-	60	182	—	-	242
17	6	-	57	188	—	-	245
17	9	—	54	195	—	—	249
18	0	_	51	201	_	_	252
18	3	-	47	208	_	-	255
18	6	-	44	214	—	-	258
18	9	-	41	220	—	—	261
19	0	_	38	226	_	_	264
19	3	-	35	232	—	-	267
19	6	-	32	239	—	-	271
19	9	-	29	245	_	-	274
20	0	_	25	252	_	_	277
20	3	-	22	258	—	_	280
20	6	-	19	264	—	_	283
20	9	_	16	270	_	—	286
21	0	_	13	276	_	_	289
21	3	-	10	283	_	_	293
21	6	-	7	289	—	—	296
21	9	—	3	296	-	—	299
22	0	_	_	302	_	_	302
22	3	-	-	299	6	-	305
22	6	-	-	295	13	—	308
22	9	-	_	292	19	—	311
23	0	_	_	289	26	_	315
23	3	-	-	286	32	-	318
23	6	-	-	283	38	-	321
23	9	_	_	280	44	—	324
24	0	_	_	277	50	_	327
24	3	-	-	273	57	-	330
24	6	-	_	270	63	_	333
24	9	_	_	267	70	—	337
25	0	_	_	264	76	_	340
25	3	-	-	261	82	-	343
25	6	-	-	258	88	-	346
25	9	_		255	94		349
26	0	_	_	251	101	_	352
26	3	-	-	248	107	-	355
26	6	-	-	245	114	-	359
26	9			242	120		362
27	0	_	_	239	126	_	365
27	3	-	-	236	132	-	368
27	6	-	-	233	138	-	371
27	9	-	-	229	145	-	374
		l	1	1	1	ļ	I

## 12 Inch Lining — 3 Inch Wedge Brick 12 x 41/2 x 3, 12 x 6 x 3 or 12 x 9 x 3 Inch–Cont'd.

Diam. I	Inside	Number Required Per Ring					
Brickv Ft	vork In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Straight	Total
28	0	_	_	226	151	_	377
28	3	_	_	223	158	_	381
28	6	_	_	220	164	_	384
28	9	_	_	217	170	_	387
29	0	—	—	214	176	—	390
29	5	_	_	211	102	_	393
29	0	_	_	207	105	_	200
29	7			204	195		377
30	0	—	_	202	201	_	403
30	3	—	-	198	208	—	406
30	6	—	-	195	214	—	409
30	9	_	_	192	220	_	412
31	0	_	_	189	226	_	415
31	3	_	-	185	233	-	418
31	6	-	-	182	239	-	421
31	9	-	-	180	245	-	425
32	0	_		176	252	_	428
32	3	_	_	173	258	_	431
32	6	_	_	170	264	_	434
32	9	—	—	167	270	—	437
33	0	_	_	163	277	_	440
33	3	_	_	160	283	_	443
33	6	_	_	158	289	_	447
33	9	_	-	154	296	_	450
34	0	_	_	151	302	_	453
34	3	_	_	148	308	_	456
34	6	_	_	145	314	_	459
34	9	—	-	141	321	—	462
35	0	_	_	138	327	_	465
35	3	_	_	135	333	_	468
35	6	_	_	132	340	_	472
35	9	_	_	129	346	_	475
36	0	_	_	126	352	_	478
36	3	_	_	123	358	_	481
36	6	_	_	119	365	_	484
36	9	—	—	116	371	—	487
37	0	_	_	113	377	_	490
37	3	_	_	110	384	_	494
37	6	_	_	107	390	_	497
37	9	_	_	104	396	_	500
38	0	_	_	101	402	_	503
38	3	_	_	97	409	_	506
38	6	_	_	94	415	_	509
38	9	_	-	91	421	_	512
39	0	_	_	88	428	_	516
39	3	_	_	85	434	_	519
39	6	_	_	82	440	_	522
39	9	_	-	79	446	_	525
		1	1	1	1	1	

## 12 Inch Lining — 3 Inch Wedge Brick 12 x 41/2 x 3, 12 x 6 x 3 or 12 x 9 x 3 Inch–Cont'd.

Diam.	Inside	ide Number Required Per Ring					
Brickv Ft	vork In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Straight	Total
40	0	_	_	76	452	_	528
40	3	_	_	72	459	_	531
40	6	_	_	69	465	_	534
40	9	_	_	66	472	_	538
41	0			42	470		E / 1
41	2	_	_	60	4/0	_	541
41	5			57	404		544
41	9	_	_	54	490	_	550
				50	500		550
42	0		_	50	503	—	553
42	3 4	_	_	47	509	_	550
42	0	_	_	44	510	_	500
42	9	_	_	41	522	_	563
43	0	_	_	38	528	—	566
43	3	_	-	35	534	_	569
43	6	—	—	32	540	—	572
43	9	—	—	28	547	—	575
44	0	_	_	25	553	_	578
44	3	_	_	22	560	_	582
44	6	_	_	19	566	_	585
44	9	_	_	16	572	_	588
45	0	_	_	13	578	_	591
45	3	—	-	10	584	—	594
45	6	_	_	6	591	_	597
45	9	_	_	3	597	_	600
46	0	_	_	_	604	_	604
46	3	_	_	_	604	3	607
46	6	_	_	_	604	6	610
46	9	—	-	_	604	9	613
47	0	_	_	_	604	12	616
47	3	_	_	_	604	15	619
47	6	_	_	_	604	18	622
47	9	_	_	_	604	22	626
10	0				604	25	620
18	3				604	20	627
10	6				604	31	635
48	9	_	_	_	604	34	638
	0					27	
49	U	_	-	-	604	3/	641
49	0	_	_	_	004	44	048
50	6	_	_	_	604	50	6004
50	O	_			004	00	000
51	0	-	_	-	604	62	666
51	6	-	-	-	604	69	673
52	0	-	-	-	604	75	679
52	6	_			604	81	685
53	0	_	_	_	604	88	692
53	6	_	_	_	604	94	698
54	0	_	_	_	604	100	704
54	6	-	_	_	604	106	710

## 12 Inch Lining — 3 Inch Key Brick 12 x 6 x 3 Inch

Diam.	Inside		Number Requ	iired Per Ring	
Bricky Ft	work In	No.2 Key	No. 1 Key	Straight	Total
10 10 10 10 10 10	0 2 4 6 8 10	76 75 74 72 71 70	2 4 7 9 11		76 77 78 79 80 81
11	0	69	13		82
11	2	68	15		83
11	4	67	17		84
11	6	66	19		85
11	8	65	21		86
11	10	64	23		87
12 12 12 12 12 12 12	0 2 4 6 8 10	63 62 61 60 59 58	25 27 29 32 34 36		88 89 90 92 93 94
13	0	57	38		95
13	2	56	40		96
13	4	55	42		97
13	6	54	44		98
13	8	53	46		99
13	10	52	48		100
14	0	51	50		101
14	2	49	53		102
14	4	48	55		103
14	6	47	57		104
14	8	46	59		105
14	10	45	61		106
15	0	44	63		107
15	2	43	65		108
15	4	42	67		109
15	6	41	69		110
15	8	40	71		111
15	10	39	73		111
16	0	38	75		113
16	2	37	78		115
16	4	36	80		116
16	6	35	82		117
16	8	34	84		118
16	10	33	86		119
17 17 17 17 17 17	0 2 4 6 8 10	32 31 30 29 27 26	88 90 92 94 97 99	       	120 121 122 123 124 125
18	0	25	101		126
18	2	24	103		127
18	4	23	105		128
18	6	22	107		129
18	8	21	109		130
18	10	20	111		131

## 12 Inch Lining — 3 Inch Key Brick 12 x 6 x 3 Inch — Continued

Brickwork         No. 2         No. 1         Straight         Total           19         0         19         113          132           19         0         19         113          133           19         4         17         117          133           19         6         16         119          135           19         8         15         122          137           19         10         14         124          139           20         0         13         126          139           20         11         130          140         142           20         0         7         138          144           20         0         7         138          144            21         0         7         138          144           21         0         7         138          144           21         0          151          151           22         0	Diam.	Inside	Number Required Per Ring				
19         0         19         113         -         132           19         2         18         115         -         133           19         4         17         117         -         134           19         6         16         119         -         135           19         8         15         122         -         137           19         10         14         124         -         139           20         2         12         128         -         140           20         6         10         132         -         142           20         8         9         134         -         144           20         0         7         138         -         145           21         0         7         138         -         144           21         0         7         138         -         145           21         1         1         143         -         144           21         0         -         151         1         151           22         0         -         151         1<	Brick Ft	work In	No. 2 Key	No. 1 Key	Straight	Total	
19       2       18       115        133         19       4       17       117        134         19       8       15       122        137         19       10       14       124        139         20       2       12       128        139         20       2       12       128        140         20       4       11       130        141         20       6       10       132        142         20       8       9       134        144         21       0       7       138        145         21       2       5       141        146         21       0       7       138        144         21       0       7       138        145         21       10       1       149        151         22       0        151       1       152         22       10       1       149        151	19	0	19	113	_	132	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	19	2	18	115	_	133	
19         6         16         119         -         135           19         8         15         122         -         137           19         10         14         124         -         138           20         0         13         126         -         139           20         2         12         128         -         140           20         4         11         130         -         141           20         6         10         132         -         142           20         8         9         134         -         143           20         10         8         136         -         144           21         0         7         138         -         145           21         10         1         149         -         146           21         8         2         147         -         148           21         8         2         147         -         151           22         0         -         151         1         152           22         0         -         151         1	19	4	17	117	_	134	
19       8       15       122        137         19       10       14       124        137         19       10       14       124        137         20       0       13       126        139         20       2       12       128        140         20       4       11       130        141         20       6       10       132        142         20       8       9       134        142         20       10       8       136        144         21       2       5       141        145         21       2       5       141        146         21       4       4       143        148         21       6       3       145        151         22       0        151       1       152         22       0        151       1       151         22       0        151       1       164	19	6	16	119	_	135	
19         10         14         124          138           20         0         13         126          139           20         2         12         128          140           20         4         11         130          141           20         6         10         132          142           20         8         9         134          143           20         0         7         138          144           21         0         7         138          144           21         0         7         138          144           21         0         7         138          144           21         0         7         138          144           21         0         -         151          148           21         10         1         149          150           22         0          151         1         151           23         0          151	19	8	15	122	_	137	
1.1 $1.1$ $1.1$ $1.1$ $1.0$ $1.00$ $20$ $2$ $12$ $128$ $$ $140$ $20$ $2$ $12$ $128$ $$ $141$ $20$ $6$ $10$ $132$ $$ $142$ $20$ $6$ $10$ $132$ $$ $142$ $20$ $0$ $8$ $9$ $134$ $$ $144$ $20$ $10$ $8$ $136$ $$ $144$ $21$ $2$ $5$ $141$ $$ $146$ $21$ $2$ $5$ $141$ $$ $146$ $21$ $4$ $4$ $143$ $$ $148$ $21$ $6$ $$ $151$ $$ $151$ $22$ $0$ $$ $151$ $1$ $152$ $22$ $0$ $$ $151$ $1$ $161$ $24$ $0$ $$ $151$ $13$ $164$ $24$ $0$	19	10	14	124	_	138	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		10					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	0	13	126	_	139	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	2	12	128	_	140	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	4	11	130	_	141	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	6	10	132	_	142	
20         10         8         136          144           21         0         7         138          145           21         2         5         141          145           21         4         4         143          147           21         6         3         145          148           21         8         2         147          149           21         10         1         149          151           22         0          151         1         152           22         2          151         1         152           22         4          151         1         154           23         0          151         1         164           24         0          151         13         164           24         0          151         13         164           24         0          151         13         164           25         6          151	20	8	9	134	_	143	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	10	8	136	—	144	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	0	7	138		145	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	2	5	141	_	146	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	4	4	143	_	147	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	6	3	145	_	148	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	8	2	147	_	149	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	10	1	149	_	150	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	22	0		151		151	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	22	2	_	151	1	152	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	4	_	151	2	153	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	6	_	151	3	154	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	23	0	_	151	6	157	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	23	6	_	151	10	161	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	24	0		151	13	164	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	24	6	_	151	16	167	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	25	0	_	151	19	170	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	25	6	_	151	22	173	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	26	0	_	151	25	176	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	26	6	_	151	28	179	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	27	0	_	151	32	183	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	27	6	_	151	35	186	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	28	0	—	151	38	189	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	28	6	—	151	41	192	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	29	0	—	151	44	195	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	29	6	_	151	47	198	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	30	0	_	151	50	201	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	30	6	_	151	54	205	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	31	0	_	151	57	208	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	31	6	-	151	60	211	
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	32	0	_	151	63	214	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	32	6	_	151	66	217	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	33	0	_	151	69	220	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	33	6	_	151	72	223	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	34	0	_	151	76	227	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	34	6	_	151	79	230	
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	35	0	_	151	82	233	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	35	6		151	85	236	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	36	0		151	88	239	
$ \begin{vmatrix} 37 & 0 & & 151 & 94 & 245 \\ 37 & 6 & & 151 & 98 & 249 \\ 38 & 0 & & 151 & 101 & 252 \\ 38 & 6 & & 151 & 104 & 255 \\ \end{vmatrix} $	36	6	-	151	91	242	
$ \begin{vmatrix} 3/ & 6 & & 151 & 98 & 249 \\ 38 & 0 & & 151 & 101 & 252 \\ 38 & 6 & & 151 & 104 & 255 \\ \end{vmatrix} $	37	0	-	151	94	245	
$\begin{vmatrix} 38 & 0 \\ 38 & 6 \\ - \\ 151 \\ 104 \\ 252 \\ 151 \\ 104 \\ 255 \\ - \\ 255 \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\$	37	6	-	151	98	249	
	38	0	-	151	101	252	
	38	0		151	104	255	

## 13<sup>1</sup>/<sub>2</sub> Inch Lining — 3 Inch Wedge Brick 13<sup>1</sup>/<sub>2</sub> x 4<sup>1</sup>/<sub>2</sub> x 3, 13<sup>1</sup>/<sub>2</sub> x 6 x 3 or 13<sup>1</sup>/<sub>2</sub> x 9 x 3 lnch

Diam	Inside		Nu	umber Requ	ired Per Rin	g	
Brick	work	No. 3	No. 2	No. 1	No. 1-X		Tatal
Ft	In	Wedge	Wedge	Wedge	Wedge	Straight	Total
4	6	85	_	_	_	_	85
4	9	82	6	_	_	_	88
5	0	79	13	_	_	_	92
5	3	76	19	—	_	_	95
5	6	73	25	—	—	—	98
5	9	69	32	_	_	_	101
6	0	66	38	—	—	—	104
6	3	63	44	-	_	-	107
6	6	60	50	_	—	—	110
6	9	57	56	_	_	_	113
7	0	54	63	—	—	—	117
7	3	51	69	-	_	_	120
7	6	47	76	_	_	_	123
/	9	44	82	_	_	_	126
8	0	41	88	_	_	_	129
8	3	38	94	-	_	-	132
8	6	35	100	—	—	—	135
8	9	32	107	_	_	_	139
9	0	29	113	_	_	—	142
9	3	25	120	—	—	—	145
9	6	22	126	_	—	—	148
9	9	19	132	_	_	_	151
10	0	16	138	_	_	_	154
10	3	13	144	_	_	_	157
10	6	10	151	—	_	_	161
10	9	7	157	_	_	-	164
11	0	3	164	_	_	_	167
11	3	_	170	_	_	_	170
11	6	—	167	6	—	—	173
11	9	—	163	13	—	—	176
12	0	_	160	19	_	_	179
12	3	—	157	26	_	_	183
12	6	—	154	32	—	—	186
12	9	—	151	38	_	_	189
13	0	-	148	44	_	_	192
13	3	-	145	50	-	—	195
13	6	-	141	57	—	—	198
13	9	_	138	63	_	_	201
14	0	-	135	70	_	_	205
14	3	-	132	76	-	—	208
14 14	6 9		129	82			211 214
14	7		120	00			214
15	0	-	123	94	-	-	217
15	3	-	119	101	-	-	220
15	6	-	116	10/	-	-	223
15	9	_	113	114	-	_	227

## 131/2 Inch Lining — 3 Inch Wedge Brick 131/2 x 41/2 x 3, 131/2 x 6 x 3 or 131/2 x 9 x 3 Inch – Continued

Diam. Ins	side	Number Required Per Ring					
Brickwor Ft	rk In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Straight	Total
16 16 16 16	0 3 6 9	 	110 107 104 101	120 126 132 138	  	 	230 233 236 239
17 17 17 17	0 3 6 9	_ _ _ _	97 94 92 88	145 151 157 164		_ _ _ _	242 245 249 252
18 18 18 18	0 3 6 9	  	85 82 79 75	170 176 182 189	  	  	255 258 261 264
19 19 19 19	0 3 6 9		72 70 66 63	195 201 208 214	 	 	267 271 274 277
20 20 20 20	0 3 6 9		60 57 53 50	220 226 233 239			280 283 286 289
21 21 21 21 21	0 3 6 9		48 44 41 38	245 252 258 264	   	 	293 296 299 302
22 22 22 22 22	0 3 6 9	_ _ _	35 31 28 26	270 277 283 289			305 308 311 315
23 23 23 23 23	0 3 6 9	_ _ _	22 19 16 13	296 302 308 314			318 321 324 327
24 24 24 24	0 3 6 9	  	9 6 4	321 327 333 340			330 333 337 340
25 25 25 25	0 3 6 9	 	   	336 333 330 327	7 13 19 25	  	343 346 349 352
26 26 26 26	0 3 6 9	  	  	324 321 318 314	31 38 44 51	  	355 359 362 365
27 27 27 27 27	0 3 6 9	 		311 308 305 302	57 63 69 75		368 371 374 377

### 13<sup>1</sup>/<sub>2</sub> Inch Lining — 3 Inch Wedge Brick 13<sup>1</sup>/<sub>2</sub> x 4<sup>1</sup>/<sub>2</sub> x 3, 13<sup>1</sup>/<sub>2</sub> x 6 x 3 or 13<sup>1</sup>/<sub>2</sub> x 9 x 3 Inch – Continued

Diam.	Inside		Nu	Number Required Per Ring				
Bricky Ft	work In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Straight	Total	
28	0	_	_	299	82	_	381	
28	3	—	_	296	88	—	384	
28	6	—	_	292	95	—	387	
28	9	—	_	289	101	—	390	
29	0	_	_	286	107	_	393	
29	3	_	_	283	113	_	396	
29	6	_	_	280	119	_	399	
29	9	_	_	277	126	_	403	
30	0	_	_	274	132		406	
30	3	_	_	270	139	_	409	
30	6	_	_	267	145	_	412	
30	9	—	_	264	151	—	415	
31	0	_	_	261	157	_	418	
31	3	_	_	258	163	—	421	
31	6	-	_	255	170	_	425	
31	9	—	_	252	176	—	428	
32	0	_	_	248	183	_	431	
32	3	_	_	245	189	_	434	
32	6	_	_	242	195	_	437	
32	9	—	_	239	201		440	
33	0	_	_	236	207	_	443	
33	3	_	_	233	214	_	447	
33	6	_	_	230	220	_	450	
33	9	_	_	227	226	_	453	
34	0	_	_	223	233	_	456	
34	3	_	-	220	239	_	459	
34	6	_	-	217	245	—	462	
34	9	—	_	214	251	_	465	
35	0	_	_	210	258	_	468	
35	3	_	_	208	264	_	472	
35	6	-	-	205	270	—	475	
35	9	—	—	201	277	_	478	
36	0	_	_	198	283	_	481	
36	3	-	-	195	289	—	484	
36	6	—	-	192	295	—	487	
36	9	_	_	188	302	_	490	
37	0	_	-	186	308	_	494	
37	3	—	-	183	314	—	497	
37	6	-	-	179	321	—	500	
37	9			176	327	_	503	
38	0	_	_	173	333	_	506	
38	3	-	-	170	339	—	509	
38	6	-	-	166	346	—	512	
38	9			164	352	_	516	
39	0	_	_	161	358	_	519	
39	3	—	-	157	365	—	522	
39	6	-	-	154	371	—	525	
39	9			151	3/7		528	

### 131/2 Inch Lining — 3 Inch Wedge Brick 131/2 x 41/2 x 3, 131/2 x 6 x 3 or 131/2 x 9 x 3 Inch – Continued

Diam. Ins	side	Number Required Per Ring					
Brickwor Ft	rk In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Straight	Total
40 40 40 40	0 3 6 9	 	 	148 144 142 139	383 390 396 402	 	531 534 538 541
41 41 41 41	0 3 6 9		_ _ _ _	135 132 129 126	409 415 421 427	_ _ _ _	544 547 550 553
42 42 42 42 42	0 3 6 9	 	 	122 120 117 113	434 440 446 453	 	556 560 563 566
43 43 43 43	0 3 6 9	 	 	110 107 104 101	459 465 471 477	 	569 572 575 578
44 44 44 44	0 3 6 9	 	 	98 95 91 88	484 490 497 503		582 585 588 591
45 45 45 45	0 3 6 9			85 82 79 76	509 515 521 528	   	594 597 600 604
46 46 46 46	0 3 6 9			73 69 66 63	534 541 547 553		607 610 613 616
47 47 47 47	0 3 6 9	 	 	60 57 54 51	559 565 572 578	 	619 622 626 629
48 48 48 48	0 3 6 9	 		47 44 41 38	585 591 597 603	 	632 635 638 641
49 49 49 49	0 3 6 9	  		35 32 29 25	609 616 622 629	  	644 648 651 654
50 50 50 50	0 3 6 9			22 19 16 13	635 641 647 653		657 660 663 666
51 51 51 51 51	0 3 6 9		  	10 7 3	660 666 673 679		670 673 676 679

## 13<sup>1</sup>/<sub>2</sub> Inch Lining — 3 Inch Key Brick $13^{1}/_{2}$ x 6 x 3 Inch

Diam	. Inside	Number Required Per Ring				
Brick Ft	kwork In	No. 3 Key	No. 2 Key	No. 1 Key	Straight	Total
2 2 2 2 2	3 4 6 8 10	29 28 26 25 24	 1 4 6 8	 	 	29 29 30 31 32
3 3 3 3 3 3	0 2 4 6 8 10	23 21 20 19 18 17	10 13 15 18 20 22	       	 	33 34 35 37 38 39
4 4 4 4 4 4	0 2 4 6 8 10	16 14 13 12 11 9	24 27 29 31 33 36	       		40 41 42 43 44 45
5 5 5 5 5 5	0 2 4 6 8 10	8 7 6 4 3 2	38 40 42 45 47 49	  		46 47 48 49 50 51
6 6 6 6 6	0 2 4 6 8 10	  	52 51 49 48 46 44	2 5 7 10 13	 	52 53 54 55 56 57
7 7 7 7 7 7	0 2 4 6 8 10	  	43 41 40 38 36 35	16 19 21 24 27 29	 	59 60 61 62 63 64
8 8 8 8 8	0 2 4 6 8 10		33 31 30 28 26 24	32 35 37 40 43 46	 	65 66 67 68 69 70
9 9 9 9 9	0 2 4 6 8 10		23 21 19 18 16 14	48 51 54 56 59 62		71 72 73 74 75 76
10 10 10 10 10 10	0 2 4 6 8 10		13 11 9 8 6 5	64 67 70 73 76 78		77 78 79 81 82 83

\*NOTE: For brickwork of inside diameters less than 6 feet, involving the use of 13<sup>1</sup>/<sub>2</sub> x 6 inch No. 3 Keys which have a very sharp taper, appreciable cutting may be necessary in some cases to secure the best bricklaying fit.

## 131/2 Inch Lining — 3 Inch Key Brick 131/2 x 6 x 3 Inch — Continued

Diam. Inside	e	Number Requ	Number Required Per Ring				
Brickwork Ft In	No. 3 Key	No. 3 No. 2 No. Key Key Ke	. 1 Straight	Total			
11 0 11 2 11 3 11 6		3         8            1         8             8             8	1 — 4 — 5 — 5 2	84 85 85 87			
12 0 12 6 13 0 13 6 14 0 14 6		8         8         8         8         8         8	5         5           5         8           5         11           5         14           5         18           5         21	90 93 96 99 103 106			
15 0 15 6 16 0 16 6 17 0 17 6			5     24       5     27       5     30       5     33       5     36       5     39	109 112 115 118 121 124			
18         0           18         6           19         0           19         6           20         0           20         6			5         43           5         46           5         49           5         52           5         55           5         58	128 131 134 137 140 143			
21 0 21 6 22 0 22 6 23 0 23 6		8             8             8             8             8             8             8             8	5         61           5         65           5         68           5         71           5         74           5         77	146 150 153 156 159 162			
24 0 24 6 25 0 25 6 26 0 26 6		8             8             8             8             8             8             8             8	5         80           5         83           5         87           5         90           5         93           5         96	165 168 172 175 178 181			
27 0 27 6 28 0 28 6 29 0 29 6		—         —         8           —         —         8           —         —         8           —         —         8           —         —         8           —         —         8           —         —         8           —         —         8           —         —         8           —         —         8	5         99           5         102           5         105           5         109           5         112           5         115	184 187 190 194 197 200			
30 0 30 6 31 0 31 6 32 0		8 8 8 8 8 8	5     118       5     121       5     124       5     127       5     131	203 206 209 212 216			
33 0 34 0 35 0 36 0	 		5 137 5 143 5 149 5 156	222 228 234 241			
37       0         38       0         39       0         40       0			5 162 5 168 5 175 5 181	247 253 260 266			

### 15 Inch Lining — 3 Inch Wedge Brick 15 x 6 x 3 or 15 x 9 x 3 Inch

Diam.	Inside		Number Required Per Ring				
Brick Ft	work In	No. 3 Wedge	No.2 Wedge	No.1 Wedge	Total		
5 5 5 5 5	0 1 3 6 9	95 94 91 88 85	 7 13 19		95 96 98 101 104		
6 6 6	0 3 6 9	82 79 75 73	25 31 38 44	 	107 110 113 117		
7 7 7 7	0 3 6 9	69 66 63 60	51 57 63 69		120 123 126 129		
8 8 8	0 3 6 9	57 53 51 47	75 82 88 95	  	132 135 139 142		
9 9 9 9	0 3 6 9	44 41 38 35	101 107 113 119	  	145 148 151 154		
10 10 10 10	0 3 6 9	31 29 25 22	126 132 139 145		157 161 164 167		
11 11 11 11	0 3 6 9	19 16 13 9	151 157 163 170	 	170 173 176 179		
12 12 12 12	0 3 6 9	7 3 	176 183 189 186	 6	183 186 189 192		
13 13 13 13	0 3 6 9	 	182 179 176 173	13 19 25 32	195 198 201 205		
14 14 14 14	0 3 6 9		170 167 164 160	38 44 50 57	208 211 214 217		
15 15 15 15	0 3 6 9	_ _ _ _	157 154 151 148	63 69 76 82	220 223 227 230		
16 16 16 16	0 3 6 9	_ _ _ _	145 142 138 135	88 94 101 107	233 236 239 242		

### 15 Inch Lining — 3 Inch Wedge Brick 15 x 6 x 3 or 15 x 9 x 3 Inch — Continued

Diam. Inside			Number Required Per Ring				
Brick Ft	work In	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Total		
17	0	132	113	—	245		
17	3	129	120	_	249		
17	6	126	126	_	252		
17	9	123	132	—	255		
18	0	120	138		258		
18	3	116	145	_	261		
18	6	113	151	_	264		
18	9	110	157	—	267		
19	0	107	164		271		
19	3	104	170	_	274		
19	6	101	176	_	277		
19	9	98	182	—	280		
20	0	94	189	_	283		
20	3	91	195	_	286		
20	6	88	201	_	289		
20	9	85	208		293		
21	0	82	214	_	296		
21	3	79	220	_	299		
21	6	76	226	_	302		
21	9	72	233	_	305		
22	0	69	239	_	308		
22	3	66	245	_	311		
22	6	63	252	_	315		
22	9	60	258	—	318		
23	0	57	264	_	321		
23	3	54	270	—	324		
23	6	50	277	—	327		
23	9	47	283	_	330		
24	0	44	289	_	333		
24	3	41	296	—	337		
24	6	38	302	—	340		
24	9	35	308	_	343		
25	0	32	314	_	346		
25	3	28	321	-	349		
25	6	25	327	—	352		
25	9	22	333	_	355		
26	0	19	340	_	359		
26	3	16	346	-	362		
26	6	13	352	-	365		
26	9	10	358	_	368		
27	0	6	365	_	371		
27	3	3	3/1	-	3/4		
27 27	6 9		377 374	7	377 381		
/			0,1	,			
28	0	-	371	13	384		
28	3	-	368	19	387		
28	6	-	365	25	390		
28	9	_	361	32	393		

## 15 Inch Lining — 3 Inch Wedge Brick 15 x 6 x 3 or 15 x 9 x 3 Inch — Continued

Diam.	Inside	Numb	er Required Per Ring	
Brick	work	No. 1	No. 1-X	
Ft	In	Wedge	Wedge	Total
29	0	358	38	396
29	3	355	44	399
29	6	352	51	403
29	9	349	57	406
			(0	
30	0	346	63 69	409 /12
30	6	330	76	/15
30	9	336	82	418
21	0	222	00	401
31	0	333	88 05	421
21	3	330	95	420
21	0	327	101	420
31	9	324	107	431
32	0	321	113	434
32	3	317	120	437
32	6	314	126	440
32	9	311	132	443
33	0	308	139	447
33	3	305	145	450
33	6	302	151	453
33	9	299	157	456
34	0	295	164	459
34	3	292	170	462
34	6	289	176	465
34	9	286	182	468
35	0	283	180	472
35	2	203	105	472
35	6	200	201	475
35	9	273	208	478
27	0	270	214	40.4
30	0	270	214	484
30	3	207	220	487
30	0	204	220	490
30	9	201	233	494
37	0	258	239	497
37	3	255	245	500
37	6	252	251	503
37	9	248	258	506
38	0	245	264	509
38	3	242	270	512
38	6	239	277	516
38	9	236	283	519
39	0	233	289	522
39	3	230	295	525
39	6	226	302	528
39	9	223	308	531
40	0	220	314	534
40	3	217	321	538
40	6	214	327	541
40	9	211	333	544
41	0	200	220	E 4 7
41 1	0	208	339	04/ 550
41 /1	<u>ь</u>	204	340	550
/1	0	100	352	556
41	7	170	300	550

## 15 Inch Lining — 3 Inch Wedge Brick 15 x 6 x 3 or 15 x 9 x 3 Inch — Continued

Diam. Inside		Number Requ	uired Per Ring	_
Brickwork Ft In	No. 1 Wedge	No. 1-X Wedge	Straight	Total
42 0 42 3 42 6 42 9	195 192 189 186	365 371 377 383	 	560 563 566 569
43 0 43 3 43 6 43 9	182 179 176 173	390 396 402 409	 	572 575 578 582
44 0 44 3 44 6 44 9	170 167 164 160	415 421 427 434	 	585 588 591 594
45 0 45 3 45 6 45 9	157 154 151 148	440 446 453 459	 	597 600 604 607
46 0 46 3 46 6 46 9	145 142 138 135	465 471 478 484	 	610 613 616 619
47 0 47 3 47 6 47 9	132 129 126 123	490 497 503 509		622 626 629 632
48 0 48 3 48 6 48 9	120 116 113 110	515 522 528 534	  	635 638 641 644
49 0 49 3 49 6 49 9	107 104 101 98	541 547 553 559	  	648 651 654 657
50         0           50         3           50         6           50         9	94 91 88 85	566 572 578 585	 	660 663 666 670
51 0 51 6 52 0 52 6	82 76 69 63	591 603 616 629	 	673 679 685 692
53         0           53         6           54         0           54         6	57 50 44 38	641 654 666 679	  	698 704 710 717
55       0         55       6         56       0         56       6	32 25 19 13	691 704 717 729	 	723 729 736 742
57 0 57 6 58 0 58 6	6 	742 754 754 754		748 754 761 767

## 18 Inch Lining — 3 Inch Wedge Brick 18 x 6 x 3 or 18 x 9 x 3 Inch

Diam.	Inside	Number Required Per Ring				
Brick Ft	work In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	Total	
6 6 6 6 6	0 1 2 3 6 9	113 112 111 110 107 104	3 5 7 13 19		113 115 116 117 120 123	
7 7 7 7	0 3 6 9	101 97 94 91	25 32 38 44		126 129 132 135	
8 8 8	0 3 6 9	88 85 82 79	51 57 63 69	 	139 142 145 148	
9 9 9 9	0 3 6 9	76 72 69 66	75 82 88 95	  	151 154 157 161	
10 10 10 10	0 3 6 9	63 60 57 54	101 107 113 119	 	164 167 170 173	
11 11 11 11	0 3 6 9	50 47 44 41	126 132 139 145	     	176 179 183 186	
12 12 12 12	0 3 6 9	38 35 32 28	151 157 163 170	 	189 192 195 198	
13 13 13 13	0 3 6 9	25 22 19 16	176 183 189 195	  	201 205 208 211	
14 14 14 14	0 3 6 9	13 10 6 3	201 207 214 220	 	214 217 220 223	
15 15 15 15	0 3 6 9		227 223 220 217	7 13 19	227 230 233 236	
16 16 16 16	0 3 6 9		214 211 207 205	25 31 38 44	239 242 245 249	
17 17 17 17	0 3 6 9		201 198 195 192	51 57 63 69	252 255 258 261	

## 18 Inch Lining — 3 Inch Wedge Brick 18 x 6 x 3 or 18 x 9 x 3 Inch — Continued

Brickwork RNo. 2 WedgeNo. 1 WedgeNo. 1.X WedgeTotal180 18189 18375 82 95- - 271 271264 271 271190 175175 175101 175 175 175- 283 283 283289 296200 167163 151 154126 139 145- 289 299289 296200 167163 132 145126 19 - 296- 289 299289 296210 154151 167 145- 199 167302 299210 154157 145- 163 139 163302 299220 154151 163 163- 299306 201 216220 139 141157 170 170- 299305 316220 139 129176 199 199- 210315 318 311220 139 141157 170- 20 189 20315 213240 117 220126 201 207 209- 333 333333 333 33324 24 25 25 25 25 25 25 25101 101 101 251 26- 237 273 306 365 289- 365 333 365 336337 337 336 333 333- 340 33324 25 25 25 25101 101 251 26- 270 270 365365 365 365 365 365 366 362 289- 365 3333 339- 365 3339<	Diam. Inside			Number Requ	uired Per Ring	
18 18 180 185 183189 185 183 183 17975 82 19 19 170 173 173 173 173 173 173 173 173 173 173 173 173 173 173 174 173 175 170 173 173 173 174 175 179 175 179 175 179 176 170 173 177 173 176 170 173 176 170 173 176 170 173 176 170 173 183 193 1170110 201 1110 1113 1117 1117210 1110 1113 11111 11111 11111 11111 11111 11111 11111 11111 11111 11111 11111 111111 11111 11111 11111 11111 111	Brick Ft	work In	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Total
18318582 $267$ 18917995 $271$ 190176101 $277$ 193173107 $283$ 199167119 $289$ 200163126 $289$ 206157139 $299$ 210151151 $302$ 210151157 $305$ 216145163 $305$ 216145163 $302$ 220139176 $315$ 220139176 $337$ 240113207 $330$ 230126201 $3333$ 240113227 $340$ 230117220 $340$ 240113227 $340$ 240113227 $340$ 240101251 $355$ 250101251 $365$ 250101258 $368$ 26088277 $365$ 250101251 $368$ 26088289 $368$ 26073308 $3$	18	0	189	75	_	264
186183882711901761012771931731072801991671192831991671192892031611322892061571393022101511513022101511513052161451633152201391763152201391763302261221893272301262013302361192143332301262013302361192143332401132273402391172203522501012513522508528335525695264365263852833652599125136626385283366266822893712707530	18	3	185	82	_	267
18917995274190176101-277193173107-280196170113-283199167119-283200163126-289203161132-293206157139-296210151151-302216145163-315216132189-315229129195-324220139176-331226132207-333230126201-327233123207-333239117220-334239117220-344240113227-340250101251-35525991244-35525991253636526385283-36525973308-38127075302-37726088277-3652599125-371 </td <td>18</td> <td>6</td> <td>183</td> <td>88</td> <td>_</td> <td>271</td>	18	6	183	88	_	271
190176101277196170113280199167119283199167119289203161132299203157139296209151151302210151151305216145163315220139176315226132189321220126201333226132189333230126201333239117220340236119214333239104233340240113227346249104245355256952643552599127136526385283365259912713622608827736525695264362260882773652697929	18	9	179	95	_	274
193173107-20196170113-283199167119-286200163126-299203161132-296209154145-299210151151-302216145163-305219141170-305219141170-315220139176-318226132189-321230126201-333236119214-333239104245-340240113227-340240101233-336250101251-35525695264-35525991271-36526682289-36526979295-38727075302-38728657339-38127966321-38728657339-38427966321-399	10	0	176	101		277
196170113283199167119289203161132289203161132299209154145299210151151302216145163305216145163315216145163315220139176327220139176330229129195324220113227330230126201333240113227346230110233343239107239346240113227340246107239346249104245352250991258365263852833652668228936526682289384270753023842707530238427075	19	3	170	107		277
199167119-226200163126-289206157139-293206157139-299210151151-302216145163-305219141170-315220139176-315220139176-3315226132189-321220126201-3333239117220-3333239117220-333240113227-340243110233-344246107239-35525695264-35525695264-36226088277-36525991255-36426682289-37127075302-3772775302-38127966321-3652669315-38427953346-37127075302-37728 <td>10</td> <td>6</td> <td>170</td> <td>113</td> <td></td> <td>200</td>	10	6	170	113		200
200163 161 157126 132 199 293 296 299210151 157151 148 157302 305 305210151 148157 149 305308 	19	9	167	119	_	286
20 $3$ $161$ $132$ $ 223$ $20$ $6$ $157$ $139$ $ 299$ $21$ $0$ $151$ $115$ $ 302$ $21$ $3$ $148$ $157$ $ 305$ $21$ $6$ $145$ $163$ $ 308$ $21$ $9$ $141$ $170$ $ 311$ $22$ $0$ $139$ $176$ $ 315$ $21$ $9$ $141$ $170$ $ 311$ $22$ $0$ $139$ $176$ $ 321$ $22$ $0$ $132$ $189$ $ 3318$ $22$ $6$ $132$ $189$ $ 321$ $22$ $0$ $126$ $201$ $ 327$ $23$ $0$ $126$ $201$ $ 3337$ $24$ $0$ $113$ $227$ $ 3340$ $24$ $0$ $113$ $227$ $ 344$ $24$ $0$ $101$ $251$ $ 352$ $25$ $0$ $101$ $251$ $ 362$ $25$ $0$ $101$ $251$ $ 336$ $25$ $0$ $77$ $258$ $ 336$ $26$ $9$ $77$ $332$ $ 337$ $26$ $0$ $88$ $277$ $ 336$ $25$ $9$ $97$ $258$ $ 336$ $26$ $6$ $82$ $289$ $ 337$ $26$ <td>20</td> <td>0</td> <td>163</td> <td>126</td> <td></td> <td>289</td>	20	0	163	126		289
20 $6$ $157$ $139$ $ 226$ $20$ $9$ $154$ $145$ $ 299$ $21$ $0$ $151$ $151$ $ 302$ $21$ $3$ $148$ $157$ $ 305$ $21$ $6$ $145$ $163$ $ 308$ $21$ $9$ $141$ $170$ $ 315$ $22$ $0$ $139$ $176$ $ 315$ $22$ $3$ $135$ $183$ $ 318$ $22$ $6$ $132$ $189$ $ 321$ $22$ $9$ $129$ $195$ $ 333$ $23$ $0$ $126$ $201$ $ 337$ $23$ $0$ $126$ $201$ $ 3330$ $23$ $6$ $119$ $214$ $ 3333$ $23$ $9$ $117$ $220$ $ 3340$ $24$ $0$ $113$ $227$ $ 340$ $24$ $0$ $113$ $227$ $ 340$ $24$ $9$ $104$ $245$ $ 352$ $25$ $0$ $97$ $258$ $ 352$ $25$ $6$ $95$ $264$ $ 337$ $26$ $9$ $77$ $73$ $302$ $ 377$ $27$ $0$ $75$ $302$ $ 337$ $26$ $9$ $66$ $321$ $ 387$ $27$ $66$ $63$ $327$ $ 387$ <t< td=""><td>20</td><td>3</td><td>161</td><td>132</td><td>_</td><td>207</td></t<>	20	3	161	132	_	207
209154145 $ 299$ 210151151 $ 302$ 213148157 $ 305$ 216145163 $ 308$ 219141170 $ 311$ 220139176 $ 315$ 223135183 $ 318$ 226132189 $ 321$ 230126201 $ 333$ 236119214 $ 333$ 236117220 $ 334$ 240113227 $ 340$ 243110233 $ 344$ 249104245 $ 355$ 25695264 $ 359$ 25991271 $ 362$ 26088277 $ 365$ 26385283 $ 365$ 26385283 $ 371$ 27075 $302$ $ 381$ 27075 $302$ $ 381$ 26977 $373$ $386$ $-$ 27075 $302$ $ 399$ 28063 $327$ $ 390$ 28953 $346$ $ 399$ 29051 <td>20</td> <td>6</td> <td>157</td> <td>139</td> <td>_</td> <td>296</td>	20	6	157	139	_	296
120 $161$ $115$ $115$ $115$ $121$ $21$ $0$ $151$ $151$ $151$ $ 302$ $21$ $3$ $148$ $157$ $ 305$ $21$ $6$ $145$ $163$ $ 315$ $21$ $9$ $141$ $170$ $ 315$ $22$ $3$ $135$ $183$ $ 311$ $22$ $6$ $132$ $189$ $ 321$ $22$ $9$ $129$ $195$ $ 324$ $23$ $0$ $126$ $201$ $ 3337$ $23$ $6$ $119$ $214$ $ 3337$ $24$ $0$ $113$ $227$ $ 340$ $24$ $0$ $113$ $227$ $ 344$ $24$ $0$ $113$ $227$ $ 344$ $24$ $0$ $113$ $227$ $ 344$ $24$ $0$ $113$ $227$ $ 340$ $24$ $0$ $113$ $227$ $ 340$ $24$ $0$ $101$ $251$ $ 352$ $25$ $0$ $101$ $251$ $ 355$ $25$ $6$ $95$ $264$ $ 359$ $25$ $9$ $91$ $271$ $ 362$ $26$ $0$ $88$ $277$ $ 346$ $26$ $9$ $75$ $302$ $ 371$ $26$ $9$ $75$ $302$ $ 381$ </td <td>20</td> <td>9</td> <td>154</td> <td>145</td> <td>_</td> <td>299</td>	20	9	154	145	_	299
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	,	154	145		277
21 $3$ $148$ $157$ $ 305$ $21$ $6$ $145$ $163$ $ 308$ $21$ $9$ $141$ $170$ $ 311$ $22$ $0$ $139$ $176$ $ 315$ $22$ $3$ $135$ $183$ $ 318$ $22$ $6$ $132$ $189$ $ 321$ $22$ $9$ $129$ $195$ $ 324$ $23$ $0$ $126$ $201$ $ 337$ $23$ $6$ $119$ $214$ $ 333$ $23$ $6$ $119$ $214$ $ 3337$ $24$ $0$ $113$ $227$ $ 340$ $24$ $3$ $110$ $233$ $ 344$ $24$ $3$ $110$ $233$ $ 344$ $24$ $9$ $104$ $245$ $ 349$ $25$ $0$ $101$ $251$ $ 352$ $25$ $6$ $95$ $264$ $ 355$ $25$ $6$ $95$ $264$ $ 365$ $26$ $3$ $85$ $283$ $ 348$ $26$ $6$ $82$ $289$ $ 371$ $27$ $0$ $75$ $302$ $ 387$ $26$ $9$ $79$ $295$ $ 387$ $27$ $6$ $69$ $315$ $ 389$ $27$ $6$ $69$ $315$ $ 389$ $27$ <td< td=""><td>21</td><td>0</td><td>151</td><td>151</td><td>  -</td><td>302</td></td<>	21	0	151	151	-	302
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	3	148	157	-	305
219141170 $$ $311$ $22$ 0139176 $ 315$ $22$ 3135183 $ 318$ $22$ 6132189 $ 321$ $22$ 9129195 $ 324$ $23$ 0126201 $ 327$ $23$ 3123207 $ 330$ $23$ 6119214 $ 333$ $23$ 9117220 $ 340$ $24$ 0113227 $ 340$ $24$ 3110233 $ 344$ $24$ 9104245 $ 352$ $25$ 0101251 $ 352$ $25$ 0101251 $ 362$ $25$ 991271 $ 365$ $26$ 88277 $ 365$ $26$ 979295 $ 371$ $26$ 979295 $ 377$ $27$ 075 $302$ $ 377$ $27$ 075 $302$ $ 381$ $27$ 075 $302$ $ 381$ $27$ 063 $327$ $ 390$ $28$ 063 $327$ $ 390$ $28$ 063 $327$ $ 390$ $28$ 953 $346$ $ 390$ <td>21</td> <td>6</td> <td>145</td> <td>163</td> <td>_</td> <td>308</td>	21	6	145	163	_	308
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	9	141	170	—	311
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	22	0	139	176	_	315
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	3	135	183	_	318
229 $129$ $195$ $$ $324$ $23$ 0 $126$ $201$ $ 337$ $23$ 6 $119$ $214$ $ 333$ $23$ 9 $117$ $220$ $ 340$ $24$ 0 $113$ $227$ $ 340$ $24$ 0 $113$ $227$ $ 340$ $24$ 0 $113$ $227$ $ 340$ $24$ 0 $104$ $245$ $ 352$ $25$ 0 $101$ $251$ $ 352$ $25$ 0 $101$ $251$ $ 352$ $25$ 0 $97$ $258$ $ 355$ $25$ 6 $95$ $264$ $ 365$ $26$ 3 $85$ $283$ $ 368$ $26$ 6 $82$ $289$ $ 377$ $27$ 0 $75$ $302$ $ 377$ $27$ 0 $75$ $302$ $ 381$ $27$ 0 $66$ $321$ $ 387$ $28$ 0 $63$ $327$ $ 390$ $28$ 3 $60$ $333$ $ 399$ $28$ 9 $53$ $346$ $ 399$ $29$ 0 $51$ $352$ $ 403$ $29$ 9 $41$ $371$ $ 403$	22	6	132	189	_	321
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	9	129	195	_	324
23 $3$ $123$ $207$ $ 330$ $23$ $6$ $119$ $214$ $ 333$ $23$ $9$ $117$ $220$ $ 333$ $24$ $0$ $113$ $227$ $ 340$ $24$ $3$ $110$ $233$ $ 343$ $24$ $6$ $107$ $239$ $ 346$ $24$ $9$ $104$ $245$ $ 349$ $25$ $0$ $101$ $251$ $ 352$ $25$ $3$ $97$ $258$ $ 355$ $25$ $6$ $95$ $264$ $ 359$ $25$ $9$ $91$ $271$ $ 365$ $26$ $88$ $277$ $ 365$ $26$ $6$ $82$ $289$ $ 371$ $26$ $9$ $79$ $295$ $ 377$ $27$ $0$ $75$ $302$ $ 381$ $27$ $0$ $75$ $302$ $ 381$ $27$ $6$ $69$ $315$ $ 387$ $28$ $0$ $63$ $327$ $ 390$ $28$ $3$ $60$ $333$ $ 399$ $28$ $9$ $53$ $346$ $ 399$ $29$ $0$ $51$ $352$ $ 403$ $27$ $9$ $41$ $371$ $ 412$	23	0	126	201	_	327
23 $6$ $119$ $214$ $ 333$ $23$ $9$ $117$ $220$ $ 337$ $24$ $0$ $113$ $227$ $ 340$ $24$ $3$ $110$ $233$ $ 343$ $24$ $6$ $107$ $239$ $ 346$ $24$ $9$ $104$ $245$ $ 349$ $25$ $0$ $101$ $251$ $ 352$ $25$ $3$ $97$ $258$ $ 355$ $25$ $6$ $95$ $264$ $ 359$ $25$ $9$ $911$ $271$ $ 362$ $26$ $0$ $88$ $277$ $ 365$ $26$ $3$ $85$ $283$ $ 368$ $26$ $6$ $82$ $289$ $ 371$ $26$ $9$ $79$ $295$ $ 377$ $27$ $0$ $75$ $302$ $ 381$ $27$ $0$ $75$ $302$ $ 381$ $27$ $6$ $69$ $321$ $ 387$ $28$ $0$ $63$ $327$ $ 390$ $28$ $3$ $60$ $333$ $ 399$ $28$ $6$ $57$ $339$ $ 399$ $28$ $9$ $53$ $346$ $ 399$ $29$ $0$ $51$ $352$ $ 403$ $29$ $9$ $41$ $371$ $ 412$	23	3	123	201	_	330
23 $9$ $117$ $220$ $ 337$ $24$ $0$ $113$ $227$ $ 340$ $24$ $3$ $110$ $233$ $ 343$ $24$ $6$ $107$ $239$ $ 346$ $24$ $9$ $104$ $245$ $ 349$ $24$ $9$ $104$ $245$ $ 349$ $24$ $9$ $104$ $245$ $ 352$ $25$ $0$ $101$ $251$ $ 352$ $25$ $6$ $95$ $264$ $ 359$ $25$ $9$ $91$ $271$ $ 362$ $26$ $0$ $88$ $277$ $ 368$ $26$ $6$ $82$ $289$ $ 371$ $26$ $9$ $79$ $295$ $ 377$ $27$ $0$ $75$ $302$ $ 377$ $27$ $0$ $75$ $302$ $ 381$ $27$ $9$ $66$ $321$ $ 380$ $27$ $9$ $66$ $321$ $ 390$ $28$ $0$ $63$ $327$ $ 390$ $28$ $6$ $57$ $339$ $ 399$ $28$ $6$ $57$ $339$ $ 399$ $29$ $0$ $51$ $352$ $ 403$ $29$ $6$ $44$ $365$ $ 409$ $29$ $9$ $411$ $371$ $ 412$	23	6	110	207	_	333
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	23	9	117	220	_	337
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	24	0	113	227	_	340
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	24	3	110	233	_	343
249 $104$ $245$ $ 349$ $25$ 0101 $251$ $ 352$ $25$ 397 $258$ $ 355$ $25$ 695 $264$ $ 359$ $25$ 991 $271$ $ 362$ $26$ 0 $88$ $277$ $ 365$ $26$ 3 $85$ $283$ $ 368$ $26$ 6 $82$ $289$ $ 371$ $26$ 979 $295$ $ 374$ $26$ 979 $295$ $ 381$ $27$ 075 $302$ $ 381$ $27$ 075 $302$ $ 381$ $27$ 9 $66$ $321$ $ 384$ $27$ 9 $66$ $321$ $ 390$ $28$ 3 $60$ $333$ $ 399$ $28$ 9 $53$ $346$ $ 399$ $28$ 9 $53$ $346$ $ 399$ $29$ 0 $51$ $352$ $ 403$ $29$ 6 $44$ $365$ $ 409$ $29$ 9 $411$ $371$ $ 412$	24	6	107	239	_	346
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	24	9	104	245	_	349
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	25	0	101	251	_	352
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	25	3	97	258	_	355
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	25	6	95	264	_	359
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	25	9	91	271	_	362
26 $3$ $85$ $283$ $ 368$ $26$ $6$ $82$ $289$ $ 371$ $26$ $9$ $79$ $295$ $ 374$ $26$ $9$ $79$ $295$ $ 374$ $27$ $0$ $75$ $302$ $ 377$ $27$ $3$ $73$ $308$ $ 381$ $27$ $6$ $69$ $315$ $ 384$ $27$ $9$ $66$ $321$ $ 387$ $28$ $0$ $63$ $327$ $ 390$ $28$ $3$ $60$ $333$ $ 393$ $28$ $6$ $57$ $339$ $ 396$ $28$ $9$ $53$ $346$ $ 399$ $29$ $0$ $51$ $352$ $ 403$ $29$ $6$ $44$ $365$ $ 409$ $29$ $9$ $411$ $371$ $ 412$	26	0	00	277		365
23 $3$ $63$ $223$ $ 300$ $26$ $6$ $82$ $289$ $ 371$ $26$ $9$ $79$ $295$ $ 374$ $27$ $0$ $75$ $302$ $ 377$ $27$ $3$ $73$ $308$ $ 381$ $27$ $6$ $69$ $315$ $ 384$ $27$ $9$ $66$ $321$ $ 387$ $28$ $0$ $63$ $327$ $ 390$ $28$ $3$ $60$ $333$ $ 393$ $28$ $6$ $57$ $339$ $ 396$ $28$ $9$ $53$ $346$ $ 399$ $29$ $0$ $51$ $352$ $ 403$ $29$ $6$ $44$ $365$ $ 409$ $29$ $9$ $411$ $371$ $ 412$	20	3	00 85	282		362
23 $6$ $62$ $209$ $$ $371$ $26$ $9$ $79$ $295$ $$ $374$ $27$ $0$ $75$ $302$ $$ $377$ $27$ $3$ $73$ $308$ $$ $381$ $27$ $6$ $69$ $315$ $$ $387$ $27$ $9$ $66$ $321$ $$ $387$ $28$ $0$ $63$ $327$ $$ $390$ $28$ $3$ $60$ $333$ $$ $393$ $28$ $6$ $57$ $339$ $$ $396$ $28$ $9$ $53$ $346$ $$ $399$ $29$ $0$ $51$ $352$ $$ $403$ $29$ $3$ $47$ $359$ $$ $406$ $29$ $6$ $44$ $365$ $$ $409$ $29$ $9$ $411$ $371$ $$ $412$	20	5	00 01	203	_	300
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	9	79	209	_	374
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	27	0	75	30.5		277
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	27	3	75	302	_	201
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	27	5	40	315	_	201
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	27	0	64	221	_	207
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	7	00	JZ I		JU /
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	28	0	63	327	-	390
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	28	3	60	333	-	393
28         9         53         346          399           29         0         51         352          403           29         3         47         359          406           29         6         44         365          409           29         9         41         371          412	28	6	57	339	-	396
29         0         51         352          403           29         3         47         359          406           29         6         44         365          409           29         9         41         371          412	28	9	53	346		399
29         3         47         359          406           29         6         44         365          409           29         9         41         371          412	29	0	51	352	_	403
29         6         44         365          409           29         9         41         371          412	29	3	47	359	_	406
29 9 41 371 — 412	29	6	44	365	-	409
	29	9	41	371	-	412

## 18 Inch Lining — 3 Inch Wedge Brick 18 x 6 x 3 or 18 x 9 x 3 Inch — Continued

Diam. Inside Brickwork		Number Required Per Ring				
		No. 2	No. 1	No. 1-X	Total	
Ft	In	Wedge	Wedge	Wedge	TUIAI	
30	0	38	377	_	415	
30	3	35	383	—	418	
30	6	31	390	—	421	
30	9	29	396	—	425	
31	0	26	402	_	428	
31	3	22	409	—	431	
31	6	19	415	—	434	
31	9	16	421	_	437	
32	0	13	427	_	440	
32	3	9	434	—	443	
32	6	7	440	_	447	
32	9	4	446	—	450	
33	0	_	453	_	453	
33	3	_	449	7	456	
33	6	—	446	13	459	
33	9	_	443	19	462	
34	0	_	440	25	465	
34	3	_	437	31	468	
34	6	—	434	38	472	
34	9	—	431	44	475	
35	0	_	427	51	478	
35	3	_	424	57	481	
35	6	_	421	63	484	
35	9	—	418	69	487	
36	0	_	415	75	490	
36	3	_	412	82	494	
36	6	—	409	88	497	
36	9	_	406	94	500	
37	0	_	402	101	503	
37	3	_	399	107	506	
37	6	—	396	113	509	
37	9	_	393	119	512	
38	0	_	390	126	516	
38	3	_	387	132	519	
38	6	—	384	138	522	
38	9	_	380	145	525	
39	0	_	377	151	528	
39	3	-	374	157	531	
39	6	-	371	163	534	
39	9	_	368	170	538	
40	0	_	365	176	541	
40	3	_	362	182	544	
40	6	-	358	189	547	
40	9		355	195	550	
41	0		352	201	553	
41	3	_	349	207	556	
41	6	-	346	214	560	
41	9		343	220	563	
42	0		340	226	566	
42	3	_	336	233	569	
42	6	_	333	239	572	
42	9	-	330	245	575	

## 18 Inch Lining — 3 Inch Wedge Brick 18 x 6 x 3 or 18 x 9 x 3 Inch — Continued

Diam. Inside		Number Required Per Ring					
Brickwor Ft	k In	No. 1 Wedge	No. 1-X Wedge	Straight	Total		
43 43 43 43	0 3 6 9	327 324 321 318	251 258 264 270		578 582 585 588		
44 44 44 44	0 3 6 9	314 311 308 305	277 283 289 295	 	591 594 597 600		
45 45 45 45	0 3 6 9	302 299 296 292	302 308 314 321	 	604 607 610 613		
46 46 47 47	0 6 0 6	289 283 277 270	327 339 352 365	 	616 622 629 635		
48 48 49 49	0 6 0 6	264 258 252 245	377 390 402 415	 	641 648 654 660		
50 50 51 51	0 6 0 6	239 233 226 220	427 440 453 465	 	666 673 679 685		
52 52 53 53	0 6 0 6	214 208 201 195	478 490 503 515		692 698 704 710		
54 54 55 55	0 6 0 6	189 182 176 170	528 541 553 566	 	717 723 729 736		
56 56 57 57	0 6 0 6	164 157 151 145	578 591 603 616	  	742 748 754 761		
58 58 59 59	0 6 0 6	138 132 126 120	629 641 654 666	   	767 773 780 786		
60 61 62 63	0 0 0 0	113 101 88 76	679 704 729 754	 	792 805 817 830		
64 65 66 67	0 0 0 0	63 51 38 25	779 804 829 855		842 855 867 880		
68 69 70 71	0 0 0 0	13 — — —	880 905 905 905	 13 25	893 905 918 930		
#### **BRICK COMBINATIONS REQUIRED FOR ARCHES**

The following tables are useful in estimating the quantities of brick required for the construction of arches. These tables give the combinations of brick sizes required for arches of given spans and rises.

In calculating the tables, no allowance was made for mortar or expansion joints or for size deviations of the brick. Fractional parts equal to or greater than one tenth of a brick were counted as an entire brick. For these reasons, the number of brick required for an arch, as given in the tables, may be slightly in excess of the number actually required.

In laying an arch course of brick, it is often necessary to cut one or two pieces, and in some instances several pieces, to complete the course.

For the brick combinations required for arches not included in the following tables, or to determine the dimensions or other numerical characteristics of arches, refer to the arch formulas found on page UR - 28, which detail arch calculations.



#### 41/2 Inch Arch Thickness — 3 Inch Arch Brick 9 x 41/2 x 3 or 131/2 x 41/2 x 3 Inch 2 Inch Rise Per Foot of Span

			Inside		Number Required Per Course					
S  Ft	pan In	Rise Ft In	R Ft	adius In	No. 3 Arch	No. 2 Arch	No. 1 Arch	Straight	Total	
1 1 1 1 1 1	0 1 2 3 4 5 6	2 2 <sup>5</sup> / <sub>32</sub> 2 <sup>11</sup> / <sub>32</sub> 2 <sup>1</sup> / <sub>2</sub> 2 <sup>21</sup> / <sub>32</sub> 2 <sup>27</sup> / <sub>32</sub>	1 1 1 1 1	10 10 <sup>27</sup> /32 11 <sup>21</sup> /32 0 <sup>1</sup> /2 1 <sup>11</sup> /32 2 <sup>5</sup> /32	6 5 5 4 4	1 2 3 4 4		       	7 7 8 8 8 8	
1 1 1 1 1	7 8 9 10 11	3 <sup>5</sup> / <sub>32</sub> 3 <sup>11</sup> / <sub>32</sub> 3 <sup>1</sup> / <sub>2</sub> 3 <sup>21</sup> / <sub>32</sub> 3 <sup>27</sup> / <sub>32</sub>	1 1 1 1 1	3 <sup>27</sup> / <sub>32</sub> 4 <sup>21</sup> / <sub>32</sub> 5 <sup>1</sup> / <sub>2</sub> 6 <sup>11</sup> / <sub>32</sub> 7 <sup>5</sup> / <sub>32</sub>	3 2 2 2 2 2	6 7 8 8 9	 	 	9 9 10 10 11	
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0 1 2 3 4 5 6 7 8 9 10 11	$\begin{array}{c} 4\\ 4 & 5/32\\ 4 & 11/32\\ 4 & 1/2\\ 4 & 21/32\\ 5 & 5/32\\ 5 & 5/32\\ 5 & 511/32\\ 5 & 1/2\\ 5 & 21/32\\ 5 & 27/32\\ \end{array}$	1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{c} 8\\ 8^{27}/_{32}\\ 9^{21}/_{32}\\ 10^{1}/_{2}\\ 11^{11}/_{32}\\ 0^{5}/_{32}\\ 1\\ 1^{27}/_{32}\\ 2^{21}/_{32}\\ 3^{1}/_{2}\\ 4^{11}/_{32}\\ 5^{5}/_{32} \end{array}$		10 10 11 12 11 11 11 10 10 10 9 9	1 2 3 4 5 6		11 11 12 12 13 13 13 13 14 14 14 15	
3 3 3 3 3 3 3	0 2 4 6 8 10	6 6 <sup>11/</sup> 32 6 <sup>21/</sup> 32 7 7 <sup>11/</sup> 32 7 <sup>21/</sup> 32	2 2 2 3 3	6 7 <sup>21</sup> /32 9 <sup>11</sup> /32 11 0 <sup>21</sup> /32 2 <sup>11</sup> /32		8 7 6 5	7 8 10 11 12 14		15 16 17 17 18 19	
4 4 4 4 4 4 4 4	0 2 4 6 8 10 11	8 8 <sup>11</sup> / <sub>32</sub> 9 9 <sup>11</sup> / <sub>32</sub> 9 <sup>21</sup> / <sub>32</sub> 9 <sup>27</sup> / <sub>32</sub>	3 3 3 3 3 3 4 4	4 5 <sup>21</sup> / <sub>32</sub> 7 <sup>11</sup> / <sub>32</sub> 9 10 <sup>21</sup> / <sub>32</sub> 0 <sup>11</sup> / <sub>32</sub> 1 <sup>5</sup> / <sub>32</sub>		4 3 2 1 1	15 17 18 20 21 22 23	    	19 20 21 22 22 23 23 23	
5 5 6 6	0 6 0 6	10 11 1 0 1 1	4 4 5 5	2 7 0 5	 	 	23 23 23 23 23	1 3 5 7	24 26 28 30	

#### 41/2 Inch Arch Thickness — 3 Inch Arch Brick 9 x 41/2 x 3 or 131/2 x 41/2 x 3 Inch 1.608 Inch (119/32 Inch) Rise Per Foot of Span (60° Central Angle)

			In	side	Number Required Per Course				
S Ft	pan In	Rise Ft In	Ra Ft	adius In	No. 3 Arch	No. 2 Arch	No. 1 Arch	Straight	Total
1 1 1 1	0 1 2 3	1 <sup>19</sup> /32 1 <sup>3</sup> /4 1 <sup>7</sup> /8 2	1 1 1 1	0 1 2 3	4 4 3 3	2 3 4 4			6 7 7 7
1 1 1 1	4 5 6 7	2 <sup>5</sup> / <sub>32</sub> 2 <sup>9</sup> / <sub>32</sub> 2 <sup>13</sup> / <sub>32</sub> 2 <sup>17</sup> / <sub>32</sub>	1 1 1 1	4 5 6 7	3 2 2 2	5 6 6 7		_ _ _	8 8 9
1 1 1 1	8 9 10 11	2 <sup>11</sup> /16 2 <sup>13</sup> /16 2 <sup>15</sup> /16 3 <sup>3</sup> /32	1 1 1 1	8 9 10 11	1 1 1 —	8 8 9 9	  1	 	9 9 10 10
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0 1 2 3 4 5 6 7 8 9	3 7/32 311/32 3 5/8 3 3/4 3 7/8 4 1/32 4 5/32 4 9/32 4 7/16 4 9/14	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0 1 2 3 4 5 6 7 8 9	- - - - - - - - - - - -	9 9 8 8 8 7 7 7 6 6	1 2 3 4 5 5 6 7 7 8		10 11 11 12 12 12 13 13 13 13
2	10	4 7/16 4 <sup>11</sup> /16	2	10	_	5	9	_	14
3 3 3 3 3 3 3 3 3 3 3 3 3 3	0 1 2 3 4 5 6 7 8 9 10 11	$4^{13/16} \\ 4^{31/32} \\ 5^{3/32} \\ 5^{7/32} \\ 5^{11/32} \\ 5^{1/2} \\ 5^{5/8} \\ 5^{3/4} \\ 5^{29/32} \\ 6^{1/32} \\ 6^{5/32} \\ 6^{9/32} \\ 6^{9/32} \\ 5^{10} \\ 6^{10} \\ 5$	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	0 1 2 3 4 5 6 7 8 9 10 11		5 5 4 4 3 3 2 2 2 1 1	10 10 11 12 12 13 14 15 15 16 17 17		15 15 16 16 16 17 17 18 18 18
4 4 4 4	0 1 2 3 6	6 <sup>7</sup> /16 6 <sup>9</sup> /16 6 <sup>11</sup> /16 6 <sup>27</sup> /32 7 <sup>1</sup> /4	4 4 4 4	0 1 2 3 6		1 — — —	18 19 19 19 19 19		19 19 19 20 21
5 5 6 6	0 6 0 6	8 <sup>1</sup> / <sub>32</sub> 8 <sup>27</sup> / <sub>32</sub> 9 <sup>21</sup> / <sub>32</sub> 10 <sup>7</sup> / <sub>16</sub>	5 5 6 6	0 6 0 6	 		19 19 19 19	4 6 8 10	23 25 27 29

#### 41/2 Inch Arch Thickness — 3 Inch Arch Brick 9 x 41/2 x 3 or 131/2 x 41/2 x 3 Inch 11/2 Inch Rise Per Foot of Span

			Ir	nside	Number Required Per Course				
Sp Ft	oan In	Rise Ft In	R Ft	adius In	No. 3 Arch	No. 2 Arch	No. 1 Arch	Straight	Total
1 1 1 1 1 1 1 1 1 1 1	0 1 2 3 4 5 6 7 8 9 10 11	1 1/2 1 5/8 1 3/4 1 7/8 2 2 1/8 2 1/4 2 3/8 2 1/2 2 5/8 2 3/4 2 7/8	1 1 1 1 1 1 1 1 1 1 2	0 3/4 1 <sup>13/16</sup> 2 7/8 3 <sup>15/16</sup> 5 6 1/16 7 1/8 8 3/16 9 1/4 10 <sup>5</sup> /16 11 3/8 0 7/16	3 3 2 2 1 1 1 	3 3 4 5 5 6 7 7 8 9 9 8			6 6 7 7 8 8 8 8 9 9 10 10
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0 1 2 3 4 5 6 7 8 9 10 11	3 3 1/8 3 1/4 3 3/8 3 1/2 3 5/8 3 3/4 3 7/8 4 4 1/8 4 1/8 4 1/4 4 3/8	2 2 2 2 2 2 2 2 2 2 2 2 2 3 3	1 1/2 2 9/16 3 5/8 411/16 5 3/4 6 3/16 7 7/8 815/16 10 11 1/16 0 1/8 1 3/16		8 8 7 7 6 6 6 5 5 5 5 4	2 3 4 5 6 7 8 8 9 10		10 11 11 12 12 12 12 13 13 13 13 14 14
3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	0 1 2 3 4 5 6 7 8 9 10 11	$\begin{array}{c} 4 \ 1/2 \\ 4 \ 5/8 \\ 4 \ 3/4 \\ 4 \ 7/8 \\ 5 \\ 5 \ 1/4 \\ 5 \ 3/8 \\ 5 \ 1/2 \\ 5 \ 5/8 \\ 5 \ 3/4 \\ 5 \ 7/8 \end{array}$	3 3 3 3 3 3 3 3 3 3 4 4	2 1/4 3 5/16 4 3/8 5 7/16 6 1/2 7 9/16 8 5/8 911/16 10 3/4 1113/16 0 7/8 115/16		4 3 3 2 2 2 1 	10 11 12 12 13 14 14 15 16 17 18 18		14 15 15 16 16 16 17 17 17 18 18
4 4 4 4	0 3 6 9	6 6 <sup>3</sup> /8 6 <sup>3</sup> /4 7 <sup>1</sup> /8	4 4 4 5	3 6 <sup>3</sup> /16 9 <sup>3</sup> /8 0 <sup>9</sup> /16	  	  	18 18 18 18	1 2 3 4	19 20 21 22
5 5 5 5	0 3 6 9	7 <sup>1</sup> / <sub>2</sub> 7 <sup>7</sup> / <sub>8</sub> 8 <sup>1</sup> / <sub>4</sub> 8 <sup>5</sup> / <sub>8</sub>	5 5 5 6	3 <sup>3</sup> /4 6 <sup>15</sup> /16 10 <sup>1</sup> /8 1 <sup>5</sup> /16	  		18 18 18 18	5 6 7 8	23 24 25 26
6 6	0 6	9 9 <sup>3</sup> /4	6 6	4 <sup>1</sup> / <sub>2</sub> 10 <sup>7</sup> / <sub>8</sub>	_	_	18 18	9 11	27 29

#### 41/2 Inch Arch Thickness — 3 Inch Arch Brick 9 x 41/2 x 3 or 131/2 x 41/2 x 3 Inch 2.302 Inch (2<sup>5</sup>/16 Inch) Rise Per Foot of Span

_				Inside Radius Ft In		Number Required Per Course					
Sp Ft	an In	Ft	Rise In			No. 3 Arch	No. 2 Arch	No. 1 Arch	Straight	Total	
1	0		2 <sup>5</sup> /16		8 <sup>31</sup> / <sub>32</sub>	7	_	_	_	7	
1	1		2 <sup>1</sup> / <sub>2</sub>		9 <sup>23</sup> /32	6	1	_	_	7	
1	2		2 <sup>11</sup> /16		10 <sup>15</sup> /32	6	2	_	_	8	
1	3		2 7/8		11 <sup>7</sup> /32	6	2	_	_	8	
1	4		3 <sup>1</sup> /16		11 <sup>31</sup> /32	5	3	_	_	8	
1	5		3 <sup>1</sup> /4	1	023/32	5	4	_	_	9	
1	6		315/32	1	1 <sup>15</sup> /32	5	4	_	_	9	
1	7		3 <sup>21</sup> /32	1	2 <sup>3</sup> /16	4	6	_	_	10	
1	8		327/32	1	2 <sup>15</sup> /16	4	6	_	_	10	
1	9		4 <sup>1</sup> / <sub>32</sub>	1	3 <sup>11</sup> /16	3	7	_	_	10	
1	10		4 7/32	1	4 7/16	3	8	_	_	11	
1	11		4 <sup>13</sup> / <sub>32</sub>	1	5 <sup>3</sup> /16	3	8	—	-	11	
2	0		4 <sup>19</sup> /32	1	5 <sup>15</sup> /16	2	9	_	_	11	
2	1		4 <sup>25</sup> /32	1	6 <sup>11</sup> /16	2	10	—	-	12	
2	2		5	1	7 <sup>7</sup> /16	2	10	—	—	12	
2	3		5 <sup>3</sup> /16	1	8 <sup>3</sup> /16	1	11	—	—	12	
2	4		5 <sup>3</sup> /8	1	8 <sup>15</sup> /16	1	12	—	—	13	
2	6		5 <sup>3</sup> /4	1	10 <sup>7</sup> /16	—	14	—	—	14	
2	8		6 <sup>1</sup> /8	1	11 <sup>29</sup> /32	—	13	1	—	14	
2	10		6 <sup>17</sup> /32	2	1 <sup>13</sup> /32	—	12	3	_	15	
3	0		6 <sup>29</sup> /32	2	2 <sup>29</sup> /32	_	11	5	_	16	
3	2		7 <sup>9</sup> /32	2	4 <sup>13</sup> /32	—	10	6	-	16	
3	4		7 <sup>11</sup> /16	2	5 <sup>29</sup> /32	—	10	7	—	17	
3	6		8 <sup>1</sup> /16	2	7 <sup>13</sup> /32	—	9	9	—	18	
3	8		8 <sup>7</sup> /16	2	8 <sup>7</sup> /8	—	8	11	—	19	
3	10		8 <sup>13</sup> /16	2	10 <sup>3</sup> /8	—	7	12	—	19	
4	0		<b>9</b> <sup>7</sup> / <sub>32</sub>	2	11 <sup>7</sup> /8	_	7	13	_	20	
4	2		9 <sup>19</sup> /32	3	1 <sup>3</sup> /8	—	6	15	—	21	
4	4		<b>9</b> <sup>31</sup> / <sub>32</sub>	3	2 <sup>7</sup> /8	—	6	16	-	22	
4	6		10 <sup>3</sup> /8	3	4 <sup>3</sup> /8	—	5	17	-	22	
4	8		10 <sup>3</sup> /4	3	5 <sup>27</sup> /32	—	4	19	-	23	
4	10		11 <sup>1</sup> /8	3	7 <sup>11</sup> /32	—	3	21	—	24	
5	0		11 <sup>1</sup> /2	3	827/32	_	3	22	_	25	
5	2		11 <sup>29</sup> /32	3	10 <sup>11</sup> /32	—	2	23	-	25	
5	4	1	0 9/32	3	11 <sup>27</sup> /32	—	1	25	-	26	
5	6	1	021/32	4	1 <sup>11</sup> /32	-	-	27	-	27	
5	8	1	1 <sup>1</sup> /16	4	2 <sup>13</sup> /16	-		27	-	27	
5	10	1	1 <sup>7</sup> /16	4	4 <sup>5</sup> /16	_	—	27	1	28	
6	0	1	1 <sup>13</sup> /16	4	5 <sup>13</sup> /16	_		27	2	29	
6	6	1	2 <sup>31</sup> /32	4	10 5/16			27	4	31	
Ŭ	-	· ·	- /02								

#### 9 Inch Arch Thickness — 3 Inch Wedge Brick 9 x 41/2 x 3, 9 x 63/4 x 3 or 9 x 9 x 3 Inch 11/2 Inch Rise Per Foot of Span

	Inside Number Required Per Course				rse			
Span Ft li	n	Rise Ft In	Ra Ft	adius In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	Total
1 6 1 7 1 8 1 9 1 10 1 11	5 7 3 9 0 1	2 <sup>1</sup> /4 2 <sup>3</sup> /8 2 <sup>1</sup> /2 2 <sup>5</sup> /8 2 <sup>3</sup> /4 2 <sup>7</sup> /8	1 1 1 1 1 2	7 1/8 8 3/16 9 1/4 10 <sup>5</sup> /16 11 3/8 0 <sup>7</sup> /16	9 8 8 7 7 7	1 2 3 4 4		10 10 10 11 11 11
2 0 2 1 2 2 2 3 2 4 2 5 2 6 2 7 2 8 2 7 2 8 2 9 2 10 2 11	) 1 2 3 3 4 5 5 6 7 7 8 9 9 0 1	3 3 1/8 3 1/4 3 3/8 3 1/2 3 5/8 3 3/4 3 7/8 4 4 1/8 4 1/4 4 3/8	2 2 2 2 2 2 2 2 2 2 2 3 3 3	1 1/2 2 9/16 3 5/8 411/16 5 3/4 613/16 7 7/8 815/16 10 11 1/16 0 1/8 1 3/16	7 6 5 5 4 4 4 3 3	5 6 7 8 8 9 10 10 10 11 12 12	- - - - - - - - - - - -	12 12 13 13 13 14 14 14 15 15 15
3 0 3 1 3 2 3 3 4 3 5 3 6 3 7 3 8 3 7 3 8 3 7 3 8 3 7 3 10 3 11	) 1 2 3 3 4 5 5 6 7 8 9 9 0 1	$\begin{array}{c} 4 \ 1/2 \\ 4 \ 5/8 \\ 4 \ 3/4 \\ 4 \ 7/8 \\ 5 \\ 5 \ 1/4 \\ 5 \ 3/8 \\ 5 \ 1/2 \\ 5 \ 5/8 \\ 5 \ 3/4 \\ 5 \ 7/8 \end{array}$	3 3 3 3 3 3 3 3 3 4 4	2 1/4 3 5/16 4 3/8 5 7/16 6 1/2 7 9/16 8 5/8 911/16 10 3/4 1113/16 0 7/8 1 <sup>15</sup> /16	3 2 1 1 	13 14 15 16 16 17 18 18 18 17 17 16 16		16 16 17 17 17 18 18 18 18 19 19 19 20
4 0 4 1 4 2 4 3 4 4 4 5 4 6 4 7 4 8 4 7 4 8 4 0 4 10 4 11	) 1 2 3 4 5 5 6 7 8 9 0 1	6 6 1/8 6 1/4 6 3/8 6 1/2 6 5/8 6 3/4 6 7/8 7 7 1/8 7 1/4 7 3/8	4 4 4 4 4 4 4 5 5 5	3 4 <sup>1</sup> / <sub>16</sub> 5 <sup>1</sup> / <sub>8</sub> 6 <sup>3</sup> / <sub>16</sub> 7 <sup>1</sup> / <sub>4</sub> 8 <sup>5</sup> / <sub>16</sub> 9 <sup>3</sup> / <sub>8</sub> 10 <sup>7</sup> / <sub>16</sub> 11 <sup>1</sup> / <sub>2</sub> 0 <sup>9</sup> / <sub>16</sub> 1 <sup>5</sup> / <sub>8</sub> 2 <sup>11</sup> / <sub>16</sub>		16 15 15 14 14 14 13 13 13 13 12 12	4 5 6 7 8 8 9 10 10 10 11 12	20 20 21 21 22 22 22 23 23 23 23 24
5 C 5 1 5 2 5 3 5 4 5 5	) 1 2 3 4 5	7 <sup>1</sup> / <sub>2</sub> 7 <sup>5</sup> / <sub>8</sub> 7 <sup>3</sup> / <sub>4</sub> 7 <sup>7</sup> / <sub>8</sub> 8 8 <sup>1</sup> / <sub>8</sub>	5 5 5 5 5 5	3 <sup>3</sup> / <sub>4</sub> 4 <sup>13</sup> / <sub>16</sub> 5 <sup>7</sup> / <sub>8</sub> 6 <sup>15</sup> / <sub>16</sub> 8 9 <sup>1</sup> / <sub>16</sub>	 	12 12 11 11 11 11 10	12 13 14 14 15 16	24 25 25 25 26 26

#### 9 Inch Arch Thickness — 3 Inch Wedge Brick 9 x 41/2 x 3, 9 x 63/4 x 3 or 9 x 9 x 3 Inch–Cont'd. 11/2 Inch Rise Per Foot of Span

	Incide Number Required Per Course			rse					
Sp Ft	oan In	Ft	lise In	Ra Ft	adius In	No. 2 Wedge	No. 1 Wedge	Straight	Total
5	6		8 <sup>1</sup> /4	5	10 <sup>1</sup> /8	10	16	_	26
5	7		8 <sup>3</sup> /8	5	11 <sup>3</sup> /16	9	18	_	27
5	8		8 <sup>1</sup> / <sub>2</sub>	6	0 1/4	9	18	_	27
5	9		8 <sup>5</sup> /8	6	1 <sup>5</sup> /16	8	19	_	27
5	10		8 <sup>3</sup> /4	6	2 <sup>3</sup> /8	8	20	_	28
5	11		8 7/8	6	3 7/16	8	20	_	28
6	0		9	6	4 <sup>1</sup> / <sub>2</sub>	7	21	_	28
6	1		<b>9</b> <sup>1</sup> / <sub>8</sub>	6	5 <sup>9</sup> /16	7	22	_	29
6	2		<b>9</b> <sup>1</sup> / <sub>4</sub>	6	6 <sup>5</sup> /8	7	22	_	29
6	3		9 <sup>3</sup> /8	6	7 <sup>11</sup> /16	6	23	_	29
6	4		<b>9</b> <sup>1</sup> / <sub>2</sub>	6	8 <sup>3</sup> /4	6	24	_	30
6	5		9 <sup>5</sup> /8	6	<b>9</b> <sup>13</sup> / <sub>16</sub>	6	24	_	30
6	6		9 <sup>3</sup> / <sub>4</sub>	6	10 <sup>7</sup> /8	5	25	_	30
6	7		9 <sup>7</sup> /8	6	11 <sup>15</sup> /16	5	26	_	31
6	8		10	7	1	5	26	_	31
6	9		10 <sup>1</sup> /8	7	2 <sup>1</sup> /16	4	27	_	31
6	10		10 <sup>1</sup> /4	7	3 <sup>1</sup> /8	4	28	_	32
6	11		10 <sup>3</sup> /8	7	4 <sup>3</sup> /16	4	28	_	32
7	0		10 <sup>1</sup> /2	7	5 <sup>1</sup> /4	3	29	_	32
7	1		10 <sup>5</sup> /8	7	6 <sup>5</sup> /16	3	30	_	33
7	2		10 <sup>3</sup> /4	7	7 <sup>3</sup> /8	3	30	_	33
7	3		10 <sup>7</sup> /8	7	8 <sup>7</sup> /16	3	31	_	34
7	4		11	7	<b>9</b> <sup>1</sup> / <sub>2</sub>	2	32	_	34
7	5		11 <sup>1</sup> /8	7	10 <sup>9</sup> /16	2	32	_	34
7	6		11 <sup>1</sup> /4	7	11 <sup>5</sup> /8	2	33	_	35
7	7		11 <sup>3</sup> /8	8	011/16	1	34	-	35
7	8		11 <sup>1</sup> /2	8	1 <sup>3</sup> /4	1	34	-	35
7	9		11 <sup>5</sup> /8	8	2 <sup>13</sup> /16	-	36	-	36
7	10		11 <sup>3</sup> /4	8	3 7/8	-	36	-	36
7	11		11 <sup>7</sup> /8	8	4 <sup>15</sup> /16	—	36	_	36
8	0	1	0	8	6	_	36	1	37
8	6	1	0 <sup>3</sup> /4	9	0 <sup>3</sup> /8	-	36	3	39
9	0	1	1 <sup>1</sup> /2	9	6 <sup>3</sup> /4	-	36	5	41
9	6	1	2 <sup>1</sup> /4	10	1 <sup>1</sup> /8	_	36	7	43
10	0	1	3	10	7 <sup>1</sup> /2	-	36	9	45
10	6	1	3 <sup>3</sup> /4	11	1 <sup>7</sup> /8	—	36	11	47
11	0	1	4 <sup>1</sup> / <sub>2</sub>	11	8 <sup>1</sup> / <sub>4</sub>	_	36	13	49
11	6	1	5 <sup>1</sup> /4	12	2 <sup>5</sup> /8	-	36	15	51
12	0	1	6	12	9	-	36	17	53
12	6	1	6 <sup>3</sup> /4	13	3 <sup>3</sup> /8	-	36	19	55
13	0	1	7 <sup>1</sup> / <sub>2</sub>	13	9 <sup>3</sup> /4	-	36	21	57
13	6	1	8 <sup>1</sup> /4	14	4 <sup>1</sup> /8	_	36	24	60
14	0	1	9	14	10 <sup>1</sup> /2	_	36	26	62
14	6	1	9 <sup>3</sup> / <sub>4</sub>	15	4 7/8	-	36	28	64
15	0	1	10 <sup>1</sup> /2	15	11 <sup>1</sup> /4	- 1	36	30	66

NOTE: This table can be used also for  $13^{1/2} x 9 x 3$  inch arch brick by substituting No. 1 and 2 arch brick for the corresponding wedge brick.

NOTE: This table can be used also for  $13^{1/2} x 9 x 3$  inch arch brick by substituting No. 1, 2, and 3 arch brick for the corresponding wedge brick.

9 Inch Arch Thickness - 3 Inch Wedge Brick 9 x  $4\frac{1}{2}$  x 3, 9 x  $6\frac{3}{4}$  x 3 or 9 x9 x 3 Inch 1.608 Inch ( $1^{19}/_{32}$  Inch) Rise Per Foot of Span ( $60^{\circ}$  Central Angle)

		Incide	Number Required Per Course				
Span Ft In	Rise Ft In	Radius Ft In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	Total	
6 1 7 1 8 1 9 1 10 1 11	2 <sup>13</sup> / <sub>32</sub> 2 <sup>17</sup> / <sub>32</sub> 2 <sup>11</sup> / <sub>16</sub> 2 <sup>13</sup> / <sub>16</sub> 2 <sup>15</sup> / <sub>16</sub> 3 <sup>3</sup> / <sub>32</sub>	1 6 1 7 1 8 1 9 1 10 2 11	10 9 9 8 8	1 2 2 3 4	  	10 10 11 11 11 11 12	
2 0 2 1 2 2 2 3 2 4 2 5 2 6 2 7 2 8 2 9 2 10 2 11	3 7/32 3 11/32 3 15/32 3 5/8 3 3/4 3 7/8 3 1/32 3 5/32 4 9/32 4 7/16 4 9/16 4 11/16	2 0 2 1 2 2 2 3 2 4 2 5 2 6 2 7 2 8 2 9 3 10 3 11	8 7 7 6 6 5 5 5 4 4 4 4	4 5 6 7 8 9 9 10 11 11 11	- - - - - - - - - - - - - - - - - - -	12 12 13 13 13 14 14 14 15 15 15 15 16	
3         0           3         1           3         2           3         3           3         4           3         5           3         6           3         7           3         8           3         9           3         10           3         11	$\begin{array}{c} 4 & {}^{13}/16 \\ 4 & {}^{31}/32 \\ 5 & {}^{3}/32 \\ 5 & {}^{7}/32 \\ 5 & {}^{11}/32 \\ 5 & {}^{12}/2 \\ 5 & {}^{5}/8 \\ 5 & {}^{3}/4 \\ 5 & {}^{29}/32 \\ 6 & {}^{1/8} \\ 6 & {}^{5}/32 \\ 6 & {}^{9}/32 \end{array}$	3         0           3         1           3         2           3         3           3         4           3         5           3         6           3         7           3         8           3         9           4         10           3         11	3 3 2 2 2 1 1 1 	13 13 14 15 16 16 17 18 18 18 19 19 18	     12	16 16 17 17 18 18 18 18 19 19 19 20 20	
4 0 4 1 4 2 4 3 4 4 4 5 4 6 4 7 4 8 4 9 4 10 4 11	6 7/16 6 9/16 6 11/16 6 27/32 6 31/32 7 3/32 7 3/32 7 1/4 7 3/8 7 1/2 7 5/8 7 25/32 7 29/32	4 0 4 1 4 2 4 3 4 4 4 5 4 6 4 7 4 8 5 9 5 10 5 11		18 18 17 17 17 16 16 16 16 15 15 15 14	2 3 4 5 6 6 7 8 8 9 10	20 21 21 22 22 22 23 23 23 23 24 24	
5 0 5 1 5 2 5 3 5 4 5 5	8 1/32 8 3/16 8 <sup>5</sup> /16 8 <sup>7</sup> /16 8 <sup>9</sup> /16 8 <sup>23</sup> /32	5 0 5 1 5 2 5 3 5 4 5 5	- - - -	14 14 13 13 12 12	10 11 12 13 14 14	24 25 25 26 26 26	

9 Inch Arch Thickness - 3 Inch Wedge Brick 9 x  $4\frac{1}{2}$  x 3, 9 x  $6\frac{3}{4}$  x 3 or 9 x9 x 3 Inch Cont'd 1.608 Inch ( $1^{19}/_{32}$  Inch) Rise Per Foot of Span ( $60^{\circ}$  Central Angle)

		Insido	Number Required Per Course				
Span Ft Ir	Rise Ft In	Radius Ft In	No. 2 Wedge	No. 1 Wedge	Straight	Total	
6 5 7 5 8 5 9 5 10 5 11	8 27/32 8 31/32 9 1/8 9 1/4 9 3/8 9 1/2	5     6       5     7       6     8       6     9       6     10       6     11	12 11 11 11 10 10	15 16 16 17 18 18	- - - -	27 27 28 28 28 28	
6         0           6         1           6         2           6         3           6         4           6         5           6         6           6         7           6         8           6         9           6         10           6         11	9 21/32 9 25/32 9 29/32 10 1/16 10 3/16 10 5/16 10 7/16 10 19/32 10 23/32 10 27/32 11 11 1/8	6       0         6       1         6       2         6       3         6       4         6       5         6       6         7       8         7       9         7       10         7       11	10 9 9 8 8 8 7 7 7 6 6 6	19 20 21 22 23 24 24 24 25 26 27		29 29 30 30 31 31 31 31 32 32 33	
7         0           7         1           7         2           7         3           7         4           7         5           7         6           7         7           8         7           7         10           7         11	$\begin{array}{c} 11 \ ^{1/4} \\ 11 \ ^{3/8} \\ 11 \ ^{17}/_{32} \\ 11 \ ^{21}/_{32} \\ 11 \ ^{25}/_{32} \\ 11 \ ^{55}/_{32} \\ 1 \ ^{15}/_{16} \\ 1 \ ^{0}/_{16$	7         0           7         1           7         2           7         3           7         4           7         5           7         6           7         7           7         8           7         9           7         10           7         11	6 5 4 4 3 3 3 2 2 2	27 28 29 30 31 32 32 33 34 34 35	- - - - - - - - - - - - - - - -	33 33 34 34 34 35 35 35 35 36 36 36 36 36 37	
8 0 8 1 8 2 8 3 8 6	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	8 0 8 1 8 2 8 3 8 6	1 1 1 	36 36 37 38 38	_ _ _ 1	37 37 38 38 39	
9     0       9     6       10     0       10     6       11     0       11     6	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9 0 9 6 10 0 10 6 11 0 11 6	  	38 38 38 38 38 38 38	3 5 7 10 12 14	41 43 45 48 50 52	
12       0         12       6         13       0         13       6         14       0         14       6	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	12         0           12         6           13         0           13         6           14         0           14         6	- - - - -	38 38 38 38 38 38 38 38	16 18 20 22 24 26	54 56 58 60 62 64	
15 0	2 0 1/8	15 0	_	38	28	66	

NOTE: This table can be used also for  $13\frac{1}{2} \times 9 \times 3$  inch arch brick by substituting No. 1, 2, and 3 arch brick for corresponding wege brick.

NOTE: This table can be used also for 13½ x 9 x 3 inch arch brick by substituting No. 1, 2, and 3 arch brick for corresponding wege brick.

#### 9 Inch Arch Thickness — 3 Inch Wedge Brick 9 x 41/2 x 3, 9 x 63/4 x 3 or 9 x 9 x 3 Inch 2 Inch Rise Per Foot of Span

			Ir	nside	Nu	mber Requir	red Per Cou	rse
Sp Ft	pan In	Rise Ft In	Ra Ft	adius In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	Total
1 1	10 11	3 <sup>21</sup> / <sub>32</sub> 3 <sup>27</sup> / <sub>32</sub>	1 1	6 <sup>11/</sup> 32 7 <sup>5</sup> /32	12 11	1		12 12
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0 1 2 3 4 5 6 7 8 9 10 11	$\begin{array}{c} 4\\ 4 & 5/32\\ 4 & 11/32\\ 4 & 1/2\\ 4 & 21/32\\ 5 & 5$	1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{c} 8\\ 8^{27}/_{32}\\ 9^{21}/_{32}\\ 10 \\ 1/_{2}\\ 11^{11}/_{32}\\ 0 \\ 5/_{32}\\ 1\\ 1^{27}/_{32}\\ 2^{21}/_{32}\\ 3 \\ 1/_{2}\\ 4^{11}/_{32}\\ 5 \\ 5^{5}/_{32} \end{array}$	11 10 10 9 9 8 8 8 8 7 7	2 3 4 5 6 7 8 8 9 10		13 13 14 14 15 15 15 16 16 16 16 17
3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	0 1 2 3 4 5 6 7 8 9 10 11	6 65/32 611/32 61/2 621/32 7 7 5/32 711/32 711/32 71/2 721/32 727/32	2 2 2 2 2 2 2 2 3 3 3 3 3 3 3	$\begin{array}{c} 6\\ 6^{27}/32\\ 7^{21}/32\\ 8 \\ 1/2\\ 9^{11}/32\\ 10 \\ 5/32\\ 11\\ 11^{27}/32\\ 0^{21}/32\\ 1 \\ 1/2\\ 2^{11}/32\\ 3 \\ 5/32 \end{array}$	7 6 5 5 4 4 3 3 3	10 11 12 13 14 14 15 16 16 16 17 18 18		17 17 18 19 19 19 20 20 20 20 21 21
4 4 4 4 4 4 4 4 4 4 4 4	0 1 2 3 4 5 6 7 8 9 10 11	8 8 5/32 8 11/32 8 1/2 8 21/32 9 9 5/32 9 11/32 9 1/2 9 21/32 9 27/32	3 3 3 3 3 3 3 3 3 4 4	$\begin{array}{c} 4\\ 4^{27}/_{32}\\ 5^{21}/_{32}\\ 6^{1}/_{2}\\ 7^{11}/_{32}\\ 8^{5}/_{32}\\ 9\\ 9^{27}/_{32}\\ 10^{21}/_{32}\\ 11^{1}/_{2}\\ 1^{5}/_{32} \end{array}$	2 2 1 1 	19 20 21 22 24 23 23 22 22 22 22 21		21 22 22 23 23 24 24 24 24 25 25 25
5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0 1 2 3 4 5 6 7 8 9 10 11	10 10 <sup>5</sup> / <sub>32</sub> 10 <sup>11</sup> / <sub>32</sub> 10 <sup>21</sup> / <sub>32</sub> 10 <sup>27</sup> / <sub>32</sub> 11 11 <sup>5</sup> / <sub>32</sub> 11 <sup>11</sup> / <sub>32</sub> 11 <sup>1</sup> / <sub>2</sub> 11 <sup>21</sup> / <sub>32</sub> 11 <sup>27</sup> / <sub>32</sub>	4 4 4 4 4 4 4 4 4 4 4 4 4	$\begin{array}{c} 2\\ 2^{27}/32\\ 3^{21}/32\\ 4^{1}/2\\ 5^{11}/32\\ 6^{5}/32\\ 7\\ 7^{27}/32\\ 8^{21}/32\\ 9^{1}/2\\ 10^{11}/32\\ 11^{5}/32 \end{array}$		21 20 20 20 19 19 19 19 19 18 18 18 17	5 5 7 7 8 9 9 10 11 11 11 13	26 26 27 27 27 27 28 28 29 29 29 29 30

#### 9 Inch Arch Thickness — 3 Inch Wedge Brick 9 x 41/2 x 3, 9 x 63/4 x 3 or 9 x 9 x 3 Inch–Cont'd. 2 Inch Rise Per Foot of Span

				Ir	Inside Number Required Per Course			rse	
Sp Ft	an In	Ft	Rise In	R: Ft	adius In	No. 2 Wedge	No. 1 Wedge	Straight	Total
6	0	1	0	5	0	17	13	_	30
6	1	1	0 <sup>5</sup> /32	5	027/32	16	14	_	30
6	2	1	011/32	5	1 <sup>21</sup> /32	16	15	—	31
6	3	1	0 <sup>1</sup> /2	5	2 <sup>1</sup> /2	16	15	_	31
6	4	1	021/32	5	3 <sup>11</sup> /32	15	16	—	31
6	5	1	027/32	5	4 <sup>5</sup> / <sub>32</sub>	15	17	—	32
6	6	1	1	5	5	15	17	-	32
6	7		1 <sup>5</sup> /32	5	5 <sup>27</sup> /32	15	18	_	33
6	8		1 1/32	5	6 <sup>21</sup> /32	14	19	_	33
6	9		1 '/2 121/	5	/ '/2	14	19	_	33
0	10		127/00	5	811/32 0.5/aa	14	20	_	34
0			127/32	Э	9 3/32	13	21	_	34
7	0	1	2	5	10	13	21	—	34
/	1		2 <sup>5</sup> /32	5	102//32	12	23	—	35
/	2		211/32	5	0 1/-	12	23	—	35
7	3		Z 1/2 221/22	6	0 '/2 111/22	11	24	_	30
7	4		2=1/32 227/22	6	2 5/22	11	25	_	30
7	6	1	2 / 32	6	2 732	10	25		36
7	7		3 5/32	6	327/32	10	20		37
7	, 8	1	311/32	6	421/32	10	27	_	37
7	9	1	3 1/2	6	5 <sup>1</sup> /2	10	28	_	38
7	10	1	321/32	6	6 <sup>11</sup> /32	9	29	_	38
7	11	1	3 <sup>27</sup> /32	6	7 5/32	9	29	_	38
8	0	1	4	6	8	9	30		39
8	1	1	4 <sup>5</sup> /32	6	8 <sup>27</sup> /32	8	31	_	39
8	2	1	411/32	6	9 <sup>21</sup> / <sub>32</sub>	8	31	_	39
8	3	1	4 <sup>1</sup> /2	6	10 <sup>1</sup> /2	7	33	_	40
8	4	1	4 <sup>21</sup> / <sub>32</sub>	6	11 <sup>11</sup> /32	7	33	_	40
8	5	1	4 <sup>27</sup> / <sub>32</sub>	7	0 5/32	6	34	_	40
8	6	1	5	7	1	6	35	_	41
8	7	1	5 <sup>5</sup> /32	7	1 <sup>27</sup> /32	6	35	—	41
8	8	1	5 <sup>11</sup> / <sub>32</sub>	7	2 <sup>21</sup> /32	5	36	—	41
8	9	1	5 <sup>1</sup> /2	7	3 <sup>1</sup> /2	5	37	—	42
8	10	1	5 <sup>21</sup> / <sub>32</sub>	7	4 <sup>11</sup> /32	5	37	-	42
8	11	1	5 <sup>27</sup> /32	7	5 <sup>5</sup> /32	5	38	—	43
9	0	1	6	7	6	4	39	_	43
9	2	1	6 <sup>11</sup> / <sub>32</sub>	7	7 <sup>21</sup> / <sub>32</sub>	4	40		44
9	4	1	6 <sup>21</sup> /32	7	<b>9</b> <sup>11</sup> / <sub>32</sub>	3	41	—	44
9	6	1	7	7	11	2	43	—	45
9	8	1	7 <sup>11</sup> /32	8	021/32	1	45	—	46
9	10	1	7 <sup>21</sup> / <sub>32</sub>	8	2 <sup>11</sup> /32	—	46	—	46
10	0	1	8	8	4	_	47	_	47
10	6	1	9	8	9	—	47	2	49
11	0	1	10	9	2	-	47	4	51
12	0	2	0	10	0	—	47	9	56
13	0	2	2	10	10	—	47	13	60
14	0	2	4	11	8	-	47	17	64
15	0	2	6	12	6	_	47	22	69

NOTE: This table can be used also for 13<sup>1</sup>/<sub>2</sub> x 9 x 3 inch arch brick by substituting No. 1 and 2 arch brick for the corresponding wedge brick.

NOTE: This table can be used also for  $13^{1/2} \times 9 \times 3$  inch arch brick by substituting No. 1, 2, and 3 arch brick for the corresponding wedge brick.

#### 9 Inch Arch Thickness — 3 Inch Wedge Brick 9 x 41/2 x 3, 9 x 63/4 x 3 or 9 x 9 x 3 Inch 2.302 Inch (25/16 Inch) Rise Per Foot of Span

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Inside			nside	Number Required Per Course				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	S Ft	Span In	Rise Ft In	R Ft	adius In	No. 3 Wedge	No. 2 Wedge	No. 1 Wedge	Total
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2	0	4 <sup>19</sup> /32	1	5 <sup>15</sup> /16	14	_	_	14
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2	1	4 <sup>25</sup> /32	1	6 <sup>11/</sup> 16	13	1	-	14
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2	2	5	1	7 7/16	13	1	_	14
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2	3	5 <sup>3</sup> /16	1	8 <sup>3</sup> /16	12	3	-	15
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2	4	5 <sup>3</sup> /8	1	8 <sup>15</sup> /16	12	3	_	15
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2	5	5 <sup>9</sup> /16	1	9 <sup>11</sup> / <sub>16</sub>	11	4	-	15
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2	6	5 <sup>3</sup> /4	1	10 7/16	11	5	-	16
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2	7	515/16	1	11 5/32	11	5	_	16
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2	8	6 1/8	1	021/	10	6	_	16
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		9	6 <sup>11</sup> /32	2	0 <sup>21</sup> /32	10		_	17
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		10	6 <sup>17</sup> /32	2	1 13/32	10		_	1/
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		11	023/32	2	Z 9/32	10	8	_	18
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	0	6 <sup>29</sup> /32	2	2 <sup>29</sup> /32	9	9	_	18
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	1	7 <sup>3</sup> /32	2	3 <sup>21</sup> / <sub>32</sub>	9	9	-	18
3       3       7 <sup>15</sup> / <sub>32</sub> 2       5 <sup>5</sup> / <sub>32</sub> 8       11        19         3       4       7 <sup>11</sup> / <sub>16</sub> 2       5 <sup>2</sup> / <sub>32</sub> 7       12        19         3       5       7 <sup>7</sup> / <sub>8</sub> 2       6 <sup>21</sup> / <sub>32</sub> 7       13        20         3       6       8 <sup>1</sup> / <sub>16</sub> 2       7 <sup>13</sup> / <sub>32</sub> 7       13        20         3       7       8 <sup>1</sup> / <sub>4</sub> 2       8 <sup>7</sup> / <sub>8</sub> 6       14        20         3       8       8 <sup>7</sup> / <sub>16</sub> 2       8 <sup>7</sup> / <sub>8</sub> 6       15        21         3       9       8 <sup>5</sup> / <sub>8</sub> 2       9 <sup>5</sup> / <sub>8</sub> 6       16        22         4       0       9 <sup>7</sup> / <sub>32</sub> 2       11 <sup>7</sup> / <sub>8</sub> 4       18        22         4       0       9 <sup>7</sup> / <sub>32</sub> 2       11 <sup>7</sup> / <sub>8</sub> 4       18        22         4       9       9 <sup>1/32</sup> / <sub>32</sub> 3       0 <sup>5</sup> / <sub>8</sub> 3       21        23         4       9       9 <sup>1/32</sup> / <sub>32</sub> 3       2 <sup>7</sup> / <sub>8</sub> 3	3	2	7 9/32	2	4 <sup>13</sup> /32	8	11	_	19
3       4 $7^{11}/16$ 2 $5^{29}/32$ 7       12        19         3       5 $7^{7}/8$ 2 $6^{21}/32$ 7       13        20         3       6 $8^{1}/16$ 2 $7^{13}/32$ 7       13        20         3       7 $8^{1}/16$ 2 $8^{1/8}/16$ 6       14        20         3       8 $8^{7}/16$ 2 $8^{7/8}/8$ 6       15        21         3       9 $8^{5/8}/8$ 2 $9^{5/8}/6$ 6       16        22         4       0 $9^{7/32}/22$ 2 $11^{7/8}/8$ 4       18        22         4       0 $9^{7/32}/22$ 2 $11^{7/8}/8$ 4       19        23         4       1 $9^{13/32}/32$ 3 $5^{7/8}/8$ 3       21        24         4       9^{31/32}/32       3 $2^{7/8}/8$ 3       21        24         4       6       10^{3/8}/3       3 4^{3/8}/3 <td>3</td> <td>3</td> <td>7<sup>15</sup>/32</td> <td>2</td> <td>5 <sup>5</sup>/32</td> <td>8</td> <td>11</td> <td>-</td> <td>19</td>	3	3	7 <sup>15</sup> /32	2	5 <sup>5</sup> /32	8	11	-	19
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	4	7 <sup>11</sup> /16	2	5 <sup>29</sup> /32	7	12	_	19
3       6       8       9       1	3	5	/ //8	2	6 <sup>21</sup> /32	/	13	-	20
3       7       8       8       7/16       2       8       7/8       6       14        20         3       8       8       7/16       2       8       7/8       6       15        21         3       9       8       5/8       2       9       5/8       6       15        21         3       10       8       13/16       2       10       3/8       6       16        22         3       11       9       1/32       2       11       7/8       4       18        22         4       0       9       7/32       2       11       7/8       4       18        22         4       1       9       1/32       3       0       5/8       4       19        23         4       2       9       9/9/32       3       1/8       4       19        23         4       4       9       3       5/8       3       21        24         4       5       10       5/32       2       23	3	6	8 1/16	2	/13/32		13	-	20
3       8       8'/16       2       8'/8       6       15        21         3       9       85/8       2       95/8       6       15        21         3       10       813/16       2       103/8       6       16        22         3       11       91/32       2       111/8       5       17        22         4       0       97/32       2       117/8       4       18        22         4       1       91/32       3       05/8       4       19        23         4       2       919/32       3       13/8       4       19        23         4       3       925/32       3       21/8       3       20        23         4       4       931/32       3       27/8       3       21        24         4       5       105/32       3       35/32       2       23        25         4       7       109/16       3       53/32       2       23        26	3	/	8 1/4	2	8 1/8	6	14	_	20
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	8	8 '/16	2	8 '/8 0 5/a	0	15	-	21
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2	9 10	0 <sup>13/1</sup>	2	9 3/8 10 3/6	6	15	-	21
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	3	11	9 <sup>1</sup> / <sub>32</sub>	2	10 % 11 <sup>1</sup> /8	5	17		22
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	0	<b>9</b> <sup>7</sup> / <sub>32</sub>	2	11 <sup>7</sup> /8	4	18	_	22
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	1	9 <sup>13</sup> /32	3	0 5/8	4	19	_	23
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	2	919/32	3	1 <sup>3</sup> /8	4	19	_	23
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	3	925/32	3	2 1/8	3	20	_	23
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	4	9 <sup>31</sup> /32	3	2 1/8	3	21	_	24
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	5	10 3/32	3	3 3/8	3	21	_	24
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	0	10 3/8	3	4 3/8 5 3/22	3	22	-	25
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	2 2	10 3/4	2	527/22	2	23	_	25
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	9	1015/16	3	619/32	2	23		26
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	10	11 1/8	3	711/32	1	25	_	26
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	11	11 <sup>5</sup> /16	3	8 <sup>3</sup> / <sub>32</sub>	_	26	_	26
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	<u> </u>	0	44.17	2	027/				27
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	5	0	11 1/2	3	8 <sup>27</sup> /32	_		1	2/
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	1	1123/32	3	917/32 1011/co	_	20		27
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	2	1 0 3/22	3	10.1/32 11.3/aa	_	20		2/
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	Л	1 0 9/32	2	1127/22		20	2	20
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	4	1 015/22	د ۵	019/32		25		20
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	6	1 021/22	4	1 <sup>11</sup> /32		25	4	29
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	7	1 027/32	4	2 <sup>1</sup> /16	_	24	5	29
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	8	1 1 1/16	4	2 <sup>13</sup> /16	_	24	6	30
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	5	9	1 1 <sup>1</sup> /4	4	3 9/16	_	23	7	30
5 11 1 1 <sup>5</sup> / <sub>8</sub> 4 5 <sup>1</sup> / <sub>16</sub> — 23 8 31	5	10	1 1 7/16	4	4 <sup>5</sup> /16	_	23	7	30
	5	11	1 1 <sup>5</sup> /8	4	5 <sup>1</sup> /16	_	23	8	31

NOTE: This table can be used also for  $13^{1/2} x 9 x 3$  inch arch brick by substituting No. 1, 2 and 3 arch brick for the corresponding wedge brick.

#### 9 Inch Arch Thickness—3 Inch Wedge Brick 9 x 41/2 x 3, 9 x 63/4 x 3 or 9 x 9 x 3 Inch–Cont'd. 2.302 Inch (25/16 Inch) Rise Per Foot of Span

Inside Number Required Per Course				rse					
Sp Ft	oan In	Ft	Rise In	R Ft	adius In	No. 2 Wedge	No. 1 Wedge	Straight	Total
6	0	1	1 <sup>13</sup> /16	4	5 <sup>13</sup> /16	22	9	_	31
6	1	1	2	4	6 <sup>9</sup> /16	22	9	-	31
6	2	1	2 <sup>3</sup> /16	4	7 <sup>5</sup> /16	22	10	_	32
6	3	1	2 <sup>3</sup> /8	4	8 <sup>1</sup> /16	21	11	-	32
6	4		219/32	4	8 <sup>13</sup> /16	21	12	-	33
6	5		2 <sup>23</sup> /32	4	9 7/16	20	13	_	33
6	0		2 5/22	4	10 % 16	20	13	_	33
6	8		3 732 311/22	4	11 / 32	10	14		34
6	9		3 <sup>17</sup> / <sub>32</sub>	5	017/32	19	15	_	34
6	10	1	323/32	5	1 9/32	19	16	_	35
6	11	1	3 <sup>15</sup> /16	5	2 <sup>1</sup> / <sub>32</sub>	18	17	_	35
7	0	1	4 <sup>1</sup> /8	5	2 <sup>25</sup> /32	18	17	_	35
7	1	1	4 <sup>5</sup> /16	5	317/32	18	18	-	36
7	2	1	4 <sup>1</sup> /2	5	4 9/32	17	19	-	36
7	3	1	411/16	5	5 1/32	17	20	_	37
/	4		4 //8	5	5 <sup>25</sup> /32	16	21	-	37
7	5		5 1/16 5 9/22	5	01//32 7 9/22	10 16	21	_	37
7	7		515/22	5	8 1/22	10	22		30
7	8		5 7/32 521/32	5	8 <sup>3</sup> / <sub>4</sub>	15	23		38
7	9		5 <sup>27</sup> /32	5	9 <sup>1</sup> / <sub>2</sub>	15	24	_	39
7	10	1	6 <sup>1</sup> /32	5	10 <sup>1</sup> / <sub>4</sub>	14	25	_	39
7	11	1	6 7/32	5	11	14	25	_	39
8	0	1	6 <sup>13</sup> /32	5	11 <sup>3</sup> /4	14	26	_	40
8	2	1	6 <sup>13</sup> /16	6	1 <sup>1</sup> /4	13	28	-	41
8	4	1	7 <sup>3</sup> /16	6	2 <sup>3</sup> /4	12	29	-	41
8	6	1	7 9/16	6	4 <sup>1</sup> /4	11	31	-	42
8	8	1	7 <sup>31</sup> /32	6	5 <sup>23</sup> /32	11	32	_	43
8	10	1	811/32	6	7 //32	10	34	_	44
9	0	1	823/32	6	823/32	9	35	_	44
9	2		9 <sup>3</sup> / <sub>32</sub>	6	10 //32	8	37	_	45
9	4		9 1/2	6	1 7/	8	38	_	46
9	0		9 <sup>7</sup> /8	7	1 '/32 011/1/	1	39	_	40
9	10	1	10 <sup>5</sup> /8	7	4 <sup>3</sup> /16	6	41	_	48
10	0	1	11 <sup>1</sup> /32	7	5 <sup>11</sup> /16	5	44	_	49
10	2	1	11 <sup>13</sup> /32	7	7 <sup>3</sup> /16	4	45	_	49
10	4	1	11 <sup>25</sup> /32	7	8 <sup>11</sup> /16	3	47	_	50
10	6	2	0 <sup>3</sup> /16	7	10 <sup>3</sup> /16	3	48	_	51
10	8	2	0 %16	7	11 <sup>21</sup> /32	2	50	-	52
10	10	2	0 <sup>15</sup> /16	8	1 <sup>5</sup> /32	1	51		52
11	0	2	1 <sup>5</sup> /16	8	2 <sup>21</sup> /32	_	53	_	53
11	6	2	2 <sup>15</sup> /32	8	7 5/32	—	53	2	55
12	0	2	3 5/8	8	11 <sup>5</sup> /8	—	53	4	57
13	U O		2''/16 g 1/,	10	0'7/32 5 9/1/		53	12	02 66
15	0	2	10 <sup>17</sup> /32	11	2 <sup>17</sup> / <sub>32</sub>	_	53	18	71

NOTE: This table can be used also for 13<sup>1</sup>/2 x 9 x 3 inch arch brick by substituting No. 1 and 2 arch brick for the corresponding wedge brick.

#### 12 Inch Arch Thickness — 3 Inch Wedge Brick 12 x $4^{1/2}$ x 3, 12 x 6 x 3 or 12 x 9 x 3 Inch 1.608 Inch ( $1^{19}/_{32}$ Inch) Rise Per Foot of Span ( $60^{\circ}$ Central Angle)

				Number Required Per Cou			rse		
Sp Ft	an In	Ft	Rise In	Rad Ft	dius In	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Total
6	0		<b>9</b> <sup>21</sup> / <sub>32</sub>	6	0	21	9	_	30
6	3		10 <sup>1</sup> /16	6	3	20	11	—	31
6	6		10 <sup>7</sup> /16	6	6	19	13	_	32
6	9		10 <sup>27</sup> /32	6	9	18	15	_	33
7	0		11 <sup>1</sup> /4	7	0	17	17	_	34
7	3		11 <sup>21</sup> /32	7	3	16	19	_	35
7	6	1	0 <sup>1</sup> /16	7	6	15	21	—	36
7	9	1	015/32	7	9	14	23	_	37
8	0	1	0 7/8	8	0	13	25	_	38
8	3	1	1 <sup>1</sup> /4	8	3	12	27	_	39
8	6	1	1 <sup>21</sup> /32	8	6	11	29	-	40
8	9	1	2 <sup>1</sup> /16	8	9	10	31	_	41
9	0	1	2 <sup>15</sup> / <sub>32</sub>	9	0	8	34	_	42
9	3	1	2 <sup>7</sup> /8	9	3	7	36	_	43
9	6	1	3 9/32	9	6	6	38	_	44
9	9	1	311/16	9	9	5	40	_	45
10	0	1	4 <sup>1</sup> / <sub>16</sub>	10	0	4	42	_	46
10	3	1	4 <sup>15</sup> /32	10	3	4	44	_	48
10	6	1	4 //8	10	6	3	46	_	49
10	9	1	5 %32	10	9	1	49	_	50
11	0	1	5 <sup>11</sup> /16	11	0	_	51	—	51
11	3	1	6 <sup>3</sup> /32	11	3	_	50	2	52
11	6	1	6 <sup>1</sup> /2	11	6	—	48	5	53
11	9	1	6 <sup>7</sup> /8	11	9	—	47	7	54
12	0	1	7 %/32	12	0	_	46	9	55
12	3	1	7 <sup>11</sup> /16	12	3	—	45	11	56
12	6	1	8 <sup>3</sup> /32	12	6	—	44	13	57
12	9	1	8 1/2	12	9	_	43	15	58
13	0	1	8 <sup>29</sup> /32	13	0	_	42	17	59
13	3		9 <sup>5</sup> /16	13	3	-	41	19	60
13	6	1	911/16	13	6	_	40	21	61
13	9	1	10 3/32	13	9	_	39	23	62
14	0	1	10 <sup>1</sup> / <sub>2</sub>	14	0	_	38	25	63
14	3	1	10 <sup>29</sup> /32	14	3	_	37	27	64
14	6		11 5/16	14	6	-	36	29	65
14	9	1	1123/32	14	9		35	31	66
15	0	2	0 1/8	15	0	_	34	33	67
15	3	2	01//32	15	3	_	32	36	68
15	6	2	U <sup>29</sup> /32	15	6	_	32	38	70
15	9	2	I 3/16	15	9	_	31	40	/1

#### 12 Inch Arch Thickness — 3 Inch Wedge Brick 12 x 41/2 x 3, 12 x 6 x 3 or 12 x 9 x 3 Inch–Cont'd. 1.608 Inch (1<sup>19</sup>/<sub>32</sub> Inch) Rise Per Foot of Span (60° Central Angle)

		Inside	Nur	nber Requir	red Per Cou	rse
Span Ft In	Rise Ft In	Radius Ft In	No. 1 Wedge	No. 1-X Wedge	Straight	Total
16 0 16 3 16 6 16 9	$\begin{array}{cccc} 2 & 1^{23}/_{32} \\ 2 & 2^{1}/_{8} \\ 2 & 2^{17}/_{32} \\ 2 & 2^{15}/_{16} \end{array}$	16 0 16 3 16 6 16 9	30 29 28 27	42 44 46 48	 	72 73 74 75
17     0       17     3       17     6       17     9	$\begin{array}{cccc} 2 & 3^{11}/_{32} \\ 2 & 3^{23}/_{32} \\ 2 & 4 & 1/_8 \\ 2 & 4^{17}/_{32} \end{array}$	17 0 17 3 17 6 17 9	25 24 23 22	51 53 55 57	 	76 77 78 79
18       0         18       3         18       6         18       9	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	18       0         18       3         18       6         18       9	21 20 19 18	59 61 63 65		80 81 82 83
19 0 19 3 19 6 19 9	$\begin{array}{cccc} 2 & 6^{17/32} \\ 2 & 6^{15/16} \\ 2 & 7^{11/32} \\ 2 & 7^{3/4} \end{array}$	19 0 19 3 19 6 19 9	17 16 15 14	67 69 71 73	  	84 85 86 87
20 0 20 3 20 6 20 9	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20 0 20 3 20 6 20 9	13 12 10 10	75 77 80 82	 	88 89 90 92
21 0 21 3 21 6 21 9	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21 0 21 3 21 6 21 9	9 8 7 6	84 86 88 90	  	93 94 95 96
22 0 22 3 22 6 22 9	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	22 0 22 3 22 6 22 9	5 3 2 1	92 95 97 99	  	97 98 99 100
23 0 23 3 23 6 23 9	$\begin{array}{cccc} 3 & 0^{31}/_{32} \\ 3 & 1^{3}/_8 \\ 3 & 1^{25}/_{32} \\ 3 & 2^{3}/_{16} \end{array}$	23 0 23 3 23 6 23 9		101 101 101 101	1 3	101 102 103 104
24 0 24 3 24 6 24 9	$\begin{array}{cccc} 3 & 2^{19}/_{32} \\ 3 & 3 \\ 3 & 3^{3}/_{8} \\ 3 & 3^{25}/_{32} \end{array}$	24 0 24 3 24 6 24 9		101 101 101 101	4 5 6 7	105 106 107 108
25 0 25 3 25 6 25 9	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	25 0 25 3 25 6 25 9		101 101 101 101	8 9 10 11	109 110 111 112

131/2 Inch Arch Thickness — 3 Inch Wedge Brick 131/2 x 41/2 x 3, 131/2 x 6 x 3 or 131/2 x 9 x 3 Inch 1.608 Inch (119/32 Inch) Rise Per Foot of Span ( $60^{\circ}$  Central Angle)

				In	side	Number Required Per Course			rse
Sp Ft	oan In	Ft	Rise In	Ra Ft	dius In	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Total
6	0		9 <sup>21</sup> /32	6	0	27	3	_	30
6	3		10 <sup>1</sup> /16	6	3	26	5	_	31
6	6		10 7/16	6	6	25	7	_	32
6	9		1027/32	6	9	24	9	_	33
	,		10 732	0	,	21	,		
7	0		11 <sup>1</sup> /4	7	0	22	12	_	34
/	3		1121/32	/	3	21	14	_	35
/	6	1	0 1/16	/	6	21	16	_	37
7	9	1	015/32	7	9	20	18	_	38
8	0	1	0 7/8	8	0	19	20	_	39
8	3	1	1 <sup>1</sup> /4	8	3	18	22	_	40
8	6	1	1 <sup>21</sup> /32	8	6	17	24	_	41
8	9	1	2 <sup>1</sup> /16	8	9	16	26	_	42
9	0	1	2 <sup>15</sup> /32	9	0	14	29	_	43
9	3	1	2 <sup>7</sup> /8	9	3	13	31	_	44
9	6	1	3 9/32	9	6	12	33	_	45
9	9	1	3 <sup>11</sup> /16	9	9	11	35	_	46
10	0	1	4 <sup>1</sup> /16	10	0	10	37	_	47
10	3	1	415/32	10	3	9	39	_	48
10	6	1	4 7/8	10	6	8	41	_	49
10	9	1	5 <sup>9</sup> /32	10	9	7	43	_	50
11	0	1	F11/1/	11	0	6	45		51
11	2	1	6 3/00	11	2	5	43	_	51
11	3	1	0 9/32	11	3	5	47	_	52
11	6	1	6 1/2	11	6	4	49	_	53
11	9	1	6 1/8	11	9	3	51	_	54
12	0	1	7 <sup>9</sup> /32	12	0	2	53	_	55
12	3	1	7 <sup>11</sup> /16	12	3	1	55	_	56
12	4 <sup>1</sup> /2	1	7 <sup>29</sup> /32	12	4 <sup>1</sup> /2	_	57	_	57
12	6	1	8 <sup>3</sup> / <sub>32</sub>	12	6	_	56	1	57
12	9	1	8 <sup>1</sup> /2	12	9	—	55	4	59
13	0	1	8 <sup>29</sup> /32	13	0	_	54	6	60
13	3	1	9 <sup>5</sup> /16	13	3	_	53	8	61
13	6	1	<b>9</b> <sup>11</sup> / <sub>16</sub>	13	6	_	52	10	62
13	9	1	10 <sup>3</sup> / <sub>32</sub>	13	9	_	51	12	63
14	0	1	10 <sup>1</sup> /2	14	0	_	50	14	64
14	3	1	10 <sup>29</sup> /32	14	3	-	49	16	65
14	6	1	11 <sup>5</sup> /16	14	6	_	48	18	66
14	9	1	11 <sup>23</sup> /32	14	9	—	47	20	67
15	0	2	0 <sup>1</sup> /8	15	0	_	46	22	68
15	3	2	017/32	15	3	_	45	24	69
15	6	2	029/32	15	6	_	44	26	70
15	9	2	1 <sup>5</sup> /16	15	9	_	43	28	71
16	0	2	123/22	16	0	_	<u>4</u> 1	21	72
16	2	2	2 1/n	16	2		10	22	72
16	6	2	217/20	16	6		30	35	7/
16	0	2	2 132 2 15/1/	16	۵		37	27	75
10	7		∠ ·-/16	10	7		50	37	10

13<sup>1</sup>/<sub>2</sub> Inch Arch Thickness — 3 Inch Wedge Brick 13<sup>1</sup>/<sub>2</sub> x 4<sup>1</sup>/<sub>2</sub> x 3, 13<sup>1</sup>/<sub>2</sub> x 6 x 3 or 13<sup>1</sup>/<sub>2</sub> x 9 x 3 Inch – Continued 1.608 Inch (1<sup>19</sup>/<sub>32</sub> Inch) Rise Per Foot of Span (60° Central Angle)

				Ins	ide	Number Required Per Course		rse	
Sp Ft	an In	Ft	Rise In	Rad Ft	lius In	No. 1 Wedge	No. 1-X Wedge	Straight	Total
17	0	2	3 <sup>11</sup> / <sub>32</sub>	17	0	37	39		76
17	3	2	3 <sup>23</sup> /32	17	3	36	41	—	77
17	6	2	4 1/8	17	6	35	43	_	78
17	9	2	417/32	17	9	34	45	_	/9
18	0	2	4 <sup>15</sup> /16	18	0	33	48	—	81
18	3	2	5''/32 5 3/4	18	3	32	50 52	_	82
18	9	2	6 <sup>5</sup> / <sub>32</sub>	18	9	30	54	_	84
19	0	2	6 <sup>17</sup> /32	19	0	29	56	_	85
19	3	2	6 <sup>15</sup> /16	19	3	28	58	_	86
19	6	2	7 <sup>11</sup> /32	19	6	27	60	—	87
19	9	2	7 <sup>3</sup> /4	19	9	26	62	_	88
20	0	2	8 <sup>5</sup> / <sub>32</sub>	20	0	25	64	_	89
20	3	2	8 <sup>9</sup> /16 931/22	20	3	24	66 49	_	90 01
20	9	2	9 <sup>11</sup> /32	20	9	23	70	_	91
21	0	2	9 <sup>3</sup> /4	21	0	21	72	_	93
21	3	2	10 <sup>5</sup> /32	21	3	19	75	_	94
21	6	2	10 <sup>9</sup> /16	21	6	18	77	_	95
21	9	2	10 <sup>31</sup> /32	21	9	17	79	_	96
22	0	2	11 <sup>3</sup> /8	22	0	16	81	_	97
22	3	2	11 <sup>25</sup> /32	22	3	15	83	—	98
22	6 9	3	0 <sup>9</sup> /16 0 <sup>9</sup> /16	22	6 9	14	85 87	_	99 100
22		2	031/22	22	0	12	00		101
23	3	3	1 <sup>3</sup> /8	23	3	12	91	_	101
23	6	3	1 <sup>25</sup> /32	23	6	10	94	_	104
23	9	3	2 <sup>3</sup> /16	23	9	9	96	—	105
24	0	3	2 <sup>19</sup> /32	24	0	8	98	_	106
24	3	3	3	24	3	7	100	—	107
24	6	3	3 <sup>3</sup> /8	24	6	6	102	—	108
24	9	3	325/32	24	9	5	104	_	109
25	0	3	4 <sup>3</sup> /16	25	0	4	106	—	110
25 26	0	3	5 5 <sup>13</sup> /16	25 26	0		110	1	112
26	6	3	6 <sup>19</sup> /32	26	6	_	113	3	116
27	0	3	7 <sup>13</sup> /32	27	0	_	113	5	118
27	6	3	8 7/32	27	6	_	113	7	120
28	0	3	9	28	0	-	113	9	122
28	6	3	9 <sup>13</sup> /16	28	6	_	113	11	124
29	0	3	10 <sup>5</sup> /8	29	0	_	113	14	127
29 30	6	3	11 //16 0 7/22	29 30	6	_	113	16 19	129 131
30	6	4	1 <sup>1</sup> /32	30	6		113	20	133
50	-	.		50	-				

#### 15 Inch Arch Thickness — 3 Inch Wedge Brick 15 x 6 x 3 or 15 x 9 x 3 Inch 1.608 Inch (1<sup>19</sup>/<sub>32</sub> Inch) Rise Per Foot of Span (60° Central Angle)

				Ins	ide	Number Required Per Course			rse
Sp Ft	an In	Ft	Rise In	Rad Ft	dius In	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Total
6	3		10 <sup>1</sup> /16	6	3	32	_	_	32
6	6		10 <sup>7</sup> /16	6	6	31	2	—	33
6	9		10 <sup>27</sup> /32	6	9	30	4	_	34
7	0		11 <sup>1</sup> /4	7	0	28	7	_	35
7	3	1	11 <sup>21</sup> /32	7	3	27	9	_	36
7	9	1	0 <sup>-7/18</sup> 0 <sup>15</sup> /32	7	9	25	13	_	37
8	0	1	0 7/8	8	0	24	15	_	39
8	3	1	1 <sup>1</sup> /4	8	3	23	17	_	40
8	6	1	1 <sup>21</sup> /32	8	6	22	19	—	41
8	9	1	2 1/16	8	9	21	21	_	42
9	0	1	2 <sup>15</sup> / <sub>32</sub>	9	0	20	23	—	43
9	3	1	2 <sup>7</sup> /8	9	3	19	25	—	44
9	6		3 9/32	9	6	18	27	_	45
9	9		3/16	9	9	17	29	_	40
10	0	1	4 <sup>1</sup> /16	10	0	16	32	_	48
10	3		415/32	10	3	15	34	_	49
10	9	1	5 <sup>9</sup> /32	10	9	14	38	_	51
11	0	1	511/16	11	0	12	40	_	52
11	3	1	6 <sup>3</sup> /32	11	3	11	42	_	53
11	6	1	6 <sup>1</sup> /2	11	6	10	44	—	54
11	9	1	6 <sup>7</sup> /8	11	9	9	46	_	55
12	0	1	7 9/32	12	0	8	48	_	56
12	3	1	7 <sup>11</sup> /16	12	3	7	50	—	57
12 12	6 9	1	8 <sup>3</sup> /32 8 <sup>1</sup> /2	12 12	6 9	5	53 55	_	58 59
10	0	1	029/	10	0	2			(0)
13	3		9 5/16	13	3	2	59	_	61
13	6	1	9 <sup>11</sup> / <sub>16</sub>	13	6	1	61	_	62
13	9	1	10 <sup>3</sup> /32	13	9	_	63	_	63
14	0	1	10 <sup>1</sup> / <sub>2</sub>	14	0	_	62	2	64
14	3	1	10 <sup>29</sup> /32	14	3	—	61	4	65
14	6		11 <sup>5</sup> /16	14	6	—	60	6	66
14	9		1123/32	14	9	_	59	ŏ	0/
15	0	2	0 1/8	15	0	-	58	10	68
15	ა 6		011/32 029/22	15	3 6		56	13	70
15	9	2	1 <sup>5</sup> /16	15	9	_	55	17	72
16	0	2	1 <sup>23</sup> /32	16	0	_	54	19	73
16	3	2	2 <sup>1</sup> /8	16	3	_	53	21	74
16	6	2	2 <sup>17</sup> /32	16	6	-	52	23	75
16	9	2	215/16	16	9		51	25	76
17	0	2	3 <sup>11</sup> /32	17	0	—	49	28	77
17	3	2	3 <sup>23</sup> /32	17	3	-	48	30	78
17	0 9	2	4 '/8 417/32	17	0 9		4/	32	80
	,	L 2	<del>т</del> / 32		7		07	J4	00

#### 15 Inch Arch Thickness — 3 Inch Wedge Brick 15 x 6 x 3 or 15 x 9 x 3 Inch — Continued 1.608 Inch ( $1^{19}/_{32}$ Inch) Rise Per Foot of Span (60° Central Angle)

				Ins	ide	Nur	nber Requir	ed Per Cou	rse
Sp Ft	an In	Ft	Rise In	Rad Ft	lius In	No. 1 Wedge	No. 1-X Wedge	Straight	Total
18 18 18 18	0 3 6 9	2 2 2 2	4 <sup>15</sup> / <sub>16</sub> 5 <sup>11</sup> / <sub>32</sub> 5 <sup>3</sup> / <sub>4</sub> 6 <sup>5</sup> / <sub>32</sub>	18 18 18 18	0 3 6 9	45 44 43 42	36 38 40 42		81 82 83 84
19 19 19 19	0 3 6 9	2 2 2 2	6 <sup>17</sup> /32 6 <sup>15</sup> /16 7 <sup>11</sup> /32 7 <sup>3</sup> /4	19 19 19 19	0 3 6 9	41 40 39 38	44 46 48 50	 	85 86 87 88
20 20 20 20	0 3 6 9	2 2 2 2	8 <sup>5</sup> / <sub>32</sub> 8 <sup>9</sup> /16 8 <sup>31</sup> / <sub>32</sub> 9 <sup>11</sup> / <sub>32</sub>	20 20 20 20	0 3 6 9	37 36 35 34	52 54 57 59		89 90 92 93
21 21 21 21	0 3 6 9	2 2 2 2	9 <sup>3</sup> / <sub>4</sub> 10 <sup>5</sup> / <sub>32</sub> 10 <sup>9</sup> / <sub>16</sub> 10 <sup>31</sup> / <sub>32</sub>	21 21 21 21	0 3 6 9	33 32 31 30	61 63 65 67		94 95 96 97
22 22 22 22 22	0 3 6 9	2 2 3 3	11 <sup>3</sup> /8 11 <sup>25</sup> /32 0 <sup>3</sup> /16 0 <sup>9</sup> /16	22 22 22 22 22	0 3 6 9	29 28 26 25	69 71 74 76		98 99 100 101
23 23 23 23	0 3 6 9	3 3 3 3	0 <sup>31/32</sup> 1 <sup>3</sup> /8 1 <sup>25</sup> /32 2 <sup>3</sup> /16	23 23 23 23	0 3 6 9	24 23 22 21	78 80 82 84		102 103 104 105
24 24 24 24	0 3 6 9	3 3 3 3	2 <sup>19</sup> / <sub>32</sub> 3 3 <sup>3</sup> / <sub>8</sub> 3 <sup>25</sup> / <sub>32</sub>	24 24 24 24	0 3 6 9	20 19 18 17	86 88 90 92		106 107 108 109
25 25 25 25	0 3 6 9	3 3 3 3	4 <sup>3</sup> /16 4 <sup>19</sup> /32 5 5 <sup>13</sup> /32	25 25 25 25	0 3 6 9	16 15 14 13	94 96 98 100		110 111 112 113
26 26 26 26	0 3 6 9	3 3 3 3	5 <sup>13/16</sup> 6 <sup>3/16</sup> 6 <sup>19/32</sup> 7	26 26 26 26	0 3 6 9	12 11 10 9	103 105 107 109	 	115 116 117 118
27 27 27 27 27	0 3 6 9	3 3 3 3	7 <sup>13</sup> / <sub>32</sub> 7 <sup>13</sup> / <sub>16</sub> 8 <sup>7</sup> / <sub>32</sub> 8 <sup>5</sup> /8	27 27 27 27 27	0 3 6 9	8 7 6 4	111 113 115 118	   	119 120 121 122
28 28 28 28	0 3 6 9	3 3 3 3	9 9 <sup>13</sup> / <sub>32</sub> 9 <sup>13</sup> / <sub>16</sub> 10 <sup>7</sup> / <sub>32</sub>	28 28 28 28	0 3 6 9	3 2 1	120 122 124 126		123 124 125 126
29 29 30 31	0 6 0 0	3 3 4 4	10 <sup>5</sup> /8 11 <sup>7</sup> /16 0 <sup>7</sup> /32 1 <sup>27</sup> /32	29 29 30 31	0 6 0 0	 	126 126 126 126	1 3 5 9	127 129 131 135

#### 18 Inch Arch Thickness — 3 Inch Wedge Brick 18 x 6 x 3 or 18 x 9 x 3 Inch 1.608 Inch (1<sup>19</sup>/<sub>32</sub> Inch) Rise Per Foot of Span (60° Central Angle)

				Ins	ide	Number Required Per Course			rse
Sp Ft	oan In	Ft	lise In	Ra Ft	dius In	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Total
8 8 8 8	0 3 6 9	1 1 1	0 <sup>7</sup> /8 1 <sup>1</sup> /4 1 <sup>21</sup> /32 2 <sup>1</sup> /16	8 8 8	0 3 6 9	36 35 34 32	4 6 8 11	   	40 41 42 43
9 9 9 9	0 3 6 9	1 1 1	2 <sup>15</sup> / <sub>32</sub> 2 <sup>7</sup> /8 3 <sup>9</sup> / <sub>32</sub> 3 <sup>11</sup> / <sub>16</sub>	9 9 9 9	0 3 6 9	31 30 29 29	13 15 17 19	 	44 45 46 48
10 10 10 10	0 3 6 9	1 1 1 1	4 <sup>1</sup> /16 4 <sup>15</sup> /32 4 <sup>7</sup> /8 5 <sup>9</sup> /32	10 10 10 10	0 3 6 9	28 27 25 24	21 23 26 28		49 50 51 52
11 11 11 11	0 3 6 9	1 1 1 1	5 <sup>11/</sup> 16 6 <sup>3</sup> /32 6 <sup>1</sup> /2 6 <sup>7</sup> /8	11 11 11 11	0 3 6 9	23 22 21 20	30 32 34 36		53 54 55 56
12 12 12 12 12	0 3 6 9	1 1 1	7 <sup>9</sup> /32 7 <sup>11</sup> /16 8 <sup>3</sup> /32 8 <sup>1</sup> /2	12 12 12 12	0 3 6 9	19 18 17 16	38 40 42 44		57 58 59 60
13 13 13 13 13	0 3 6 9	1 1 1 1	8 <sup>29</sup> / <sub>32</sub> 9 <sup>5</sup> / <sub>16</sub> 9 <sup>11</sup> / <sub>16</sub> 10 <sup>3</sup> / <sub>32</sub>	13 13 13 13	0 3 6 9	15 14 13 12	46 48 50 52	 	61 62 63 64
14 14 14 14	0 3 6 9	1 1 1	10 <sup>1</sup> /2 10 <sup>29</sup> /32 11 <sup>5</sup> /16 11 <sup>23</sup> /32	14 14 14 14	0 3 6 9	11 9 8 7	54 57 59 61		65 66 67 68
15 15 15 15	0 3 6 9	2 2 2 2	0 <sup>1</sup> /8 0 <sup>17</sup> /32 0 <sup>29</sup> /32 1 <sup>5</sup> /16	15 15 15 15	0 3 6 9	7 6 5 4	63 65 67 69	  	70 71 72 73
16 16 16 16	0 3 6 9	2 2 2 2	1 <sup>23</sup> / <sub>32</sub> 2 <sup>1</sup> /8 2 <sup>17</sup> / <sub>32</sub> 2 <sup>15</sup> / <sub>16</sub>	16 16 16 16	0 3 6 9	2 1 	72 74 76 75	 2	74 75 76 77
17 17 17 17 17	0 3 6 9	2 2 2 2	3 <sup>11</sup> / <sub>32</sub> 3 <sup>23</sup> / <sub>32</sub> 4 <sup>1</sup> / <sub>8</sub> 4 <sup>17</sup> / <sub>32</sub>	17 17 17 17	0 3 6 9	 	74 72 71 70	4 7 9 11	78 79 80 81
18 18 18 18	0 3 6 9	2 2 2 2	4 <sup>15</sup> / <sub>16</sub> 5 <sup>11</sup> / <sub>32</sub> 5 <sup>3</sup> / <sub>4</sub> 6 <sup>5</sup> / <sub>32</sub>	18 18 18 18	0 3 6 9		69 68 67 66	13 15 17 19	82 83 84 85
19 19 19 19	0 3 6 9	2 2 2 2	6 <sup>17</sup> / <sub>32</sub> 6 <sup>15</sup> / <sub>16</sub> 7 <sup>11</sup> / <sub>32</sub> 7 <sup>3</sup> / <sub>4</sub>	19 19 19 19	0 3 6 9		65 64 63 62	21 23 25 27	86 87 88 89

#### 18 Inch Arch Thickness — 3 Inch Wedge Brick 18 x 6 x 3 or 18 x 9 x 3 Inch — Continued 1.608 Inch (1<sup>19</sup>/<sub>32</sub> Inch) Rise Per Foot of Span (60° Central Angle)

_				Ins	ide	Number Required Per Course			
Sp Ft	an In	Ft	Rise In	Rad Ft	lius In	No. 2 Wedge	No. 1 Wedge	No. 1-X Wedge	Total
20	0	2	8 <sup>5</sup> /32	20	0	_	61	29	90
20	3	2	8 <sup>9</sup> /16	20	3	_	60	32	92
20 20	6 9	2	8 <sup>31/32</sup> 9 <sup>11/32</sup>	20	6 9	_	59 58	34 36	93 94
			- 0.						
21	0 3	2	9 3/4 10 5/22	21	0 3	_	57	38	95 96
21	6	2	10 732	21	6		55	40	90 97
21	9	2	10 <sup>31</sup> / <sub>32</sub>	21	9	_	54	44	98
22	0	2	11 <sup>3</sup> /8	22	0	_	53	46	99
22	3	2	11 <sup>25</sup> /32	22	3	_	52	48	100
22	6	3	0 <sup>3</sup> /16	22	6	_	50	51	101
22	9	3	0 9/16	22	9	_	49	53	102
23	0	3	031/32	23	0	_	48	55	103
23	3	3	1 <sup>3</sup> /8	23	3	—	47	57	104
23	6	3	1 <sup>25</sup> /32	23	6	—	46	59	105
23	9	3	2 3/16	23	9	_	45	61	106
24	0	3	2 <sup>19</sup> /32	24	0	_	44	63	107
24	3	3	3	24	3	—	43	65	108
24	6	3	3 3/8	24	6	_	42	67	109
24	9	3	323/32	24	9		41	09	110
25	0	3	4 <sup>3</sup> /16	25	0	—	40	71	111
25	3	3	4 <sup>19</sup> /32	25	3	—	39	73	112
25	6	3	5 513/	25	6	_	38	/5	113
25	9	3	519/32	25	9		37	/8	115
26	0	3	5 <sup>13</sup> /16	26	0	—	36	80	116
26	3	3	6 <sup>3</sup> /16	26	3	—	35	82	117
26	0	3	617/32 7	26	6 0	_	34	84 86	118
20	,	5	,	20	,			00	117
27	0	3	7 <sup>13</sup> /32	27	0	_	32	88	120
27	3	3	0 7/22	27	3	_	31	90	121
27	9	3	8 <sup>5</sup> /8	27	9		29	94	122
28	0	3	9	28	0		27	97	124
28	3	3	9 <sup>13</sup> /32	28	3	_	26	99	125
28	6	3	9 <sup>13</sup> /16	28	6	_	25	101	126
28	9	3	10 <sup>7</sup> /32	28	9	—	24	103	127
29	0	3	10 5/8	29	0		23	105	128
29	3	3	11 <sup>1</sup> /32	29	3	-	22	107	129
29	6	3	11 //16	29	6	—	21	109	130
29	9	3	1113/16	29	9	_	20	111	131
30	0	4	0 7/32	30	0	-	19	113	132
30	3	4	0 5/8	30	3	-	18	115	133
30 30	6 9	4	1 1/32 1 7/14	30 30	6 9		16	110	134 135
30	,	-	1 /10	50	,		10	117	100
31	0	4	1 <sup>27</sup> /32	31	0	-	15	122	137
31	3	4	2 <sup>1</sup> /4 221/22	31	3	-	14	124	138 120
31	9	4	2 - 1/32 3 1/32	31	9		12	120	139
20	0	4	27/	20	0		11	100	141
32	U	4	3 1/16	32	U	- 1		130	141

The following simple formulas make it possible to calculate the area and volume associated with most refractory structures. No matter how complex the shape of a figure, it is possible to derive a working approximation by dividing it by straight lines and arcs into a distinct number of units whose areas may be calculated and summed by simple arithmetic. Volumes of regular figures will equal the area of a surface multiplied by its length or height. Volumes of shells are inside volume subtracted from outside volume.





### AREA AND VOLUME





# AREA AND VOLUME



# AREA AND VOLUME



A = Area of base a = Area of top

m = Area of midsection

Area of Conical Surface =  $\frac{1}{2}\pi s(D+d)$ 

Volume =  $\frac{1}{3}\pi h(r^2 + rR + R^2)$ 

Volume =  $h(a + \sqrt{aA} + A)$ 

Volume =  $\frac{1}{6}h(a + 4m + A)$ 



	Decimal Fractions of an Inch for Each 1/64								
Common Fraction	Decimal	Common Fraction	Decimal						
		1/2	.5						
1/64 1/32 3/64 1/16 5/64 3/32 7/64	.015625 .03125 .046875 .0625 .078125 .09375 .109325	33/64 17/32 35/64 9/16 37/64 19/32 39/64	.515625 .53125 .546875 .5625 .578125 .59375 .609375						
1/8	.125	5/8	.625						
9/64 5/32 11/64 3/16 13/64 7/32 15/64	.140625 .15625 .171875 .1875 .203125 .21875 .234375	41/64 21/32 43/64 11/16 45/64 23/32 47/64	.640625 .65625 .671875 .6875 .703125 .71875 .734375						
1/4	.25	3/4	.75						
17/64 9/32 19/64 5/16 21/64 11/32 23/64	.265625 .28125 .296875 .3125 .328125 .34375 .359375	49/64 25/32 51/64 13/16 53/64 27/32 55/64	.765625 .78125 .796875 .8125 .828125 .84375 .859375						
3/8	.375	7/8	.875						
25 /64 13 /32 27 /64 7 /16 29 /64 15 /32 31 /64	.390625 .40625 .421875 .4375 .453125 .46875 .484375	57 /64 29 /32 59 /64 15 /16 61 /64 31 /32 63 /64	.890625 .90625 .921875 .9375 .953125 .96875 .984375						

Conversion Table								
To Convert	Multiply By:	To Obtain:						
BTU	7.7816 x 10 <sup>2</sup>	foot-pounds						
BTU	$2.52 \times 10^{-1}$	kilogram-calories						
BTU/Hr	$7.0 \times 10^{-2}$	gram-cal/sec						
<b>℃</b>	(°C x 1.8) + 32	Fahrenheit						
centimeters	3.281 x 10 <sup>-2</sup>	feet						
centimeters	3.937 x 10 <sup>-2</sup>	inches						
cubic centimeters	3.531 x 10⁵	cubic feet						
cubic centimeters	6.102 x 10 <sup>-2</sup>	cubic inches						
cubic centimeters	1.308 x 10 <sup>-6</sup>	cubic yards						
cubic centimeters	2.642 x 10 <sup>-4</sup>	gallons (U.S. liquid)						
cubic centimeters	1.0 x 10 <sup>-3</sup>	liters						
cubic feet	2.832 x 10⁴	cubic centimeters						
cubic feet	1.728 x 10 <sup>3</sup>	cubic inches						
cubic feet	2.832 x 10 <sup>-2</sup>	cubic meters						
cubic feet	3.704 x 10 <sup>-2</sup>	cubic vards						
cubic inches	16 39	cubic centimeters						
cubic inches	5 787 x 10 <sup>-4</sup>	cubic feet						
cubic inches	1 639 x 10⁵	cubic meters						
cubic inches	2 143 x 10 <sup>5</sup>	cubic vards						
cubic meters	35.31	cubic feet						
cubic meters	6 102 x 10 <sup>4</sup>	cubic inches						
cubic meters	1 308	cubic vards						
cubic meters	1.000	liters						
cubic meters	$2.642 \times 10^2$	dallons (LLS liquid)						
cubic vards	7.646 x 10 <sup>5</sup>	cubic centimeters						
cubic yards	27	cubic feet						
cubic yards	0.7646	cubic meters						
	0.7646							
°Fahrenheit	.556(F-32)	Centigrade or Celsius						
feet	30.48	centimeters						
feet	0.3048	meters						
feet	$3.048 \times 10^2$	millimeters						
gallons	3.785 x 10 <sup>3</sup>	cubic centimeters						
gallons	0.134	cubic feet						
gallons	3.785 x 10 <sup>-3</sup>	cubic meters						
gallons	4.951 x 10⁻³	cubic yards						
gallons	3.785	liters						
grams	3.527 x 10 <sup>-2</sup>	ounces (avdp.)						
grams	2.205 x 10 <sup>-3</sup>	pounds						
grams/cm <sup>3</sup>	62.43	pounds/ft <sup>3</sup>						
grams/cm <sup>2</sup>	2.0481	pounds/sq/ft						
grams-calories	3.968 x 10 <sup>-3</sup>	BTU						
-								

	Conversion Table - continued								
To Convert	Multiply By:	To Obtain:							
inches	2.540	centimeters							
inches	25.4	millimeters							
kilograms	2.2046	pounds							
kilograms/meters³	6.243 x 10²	pounds/ft³							
kilometers	0.6214	miles (statute)							
liters	3.531 x 10 <sup>-2</sup>	cubic feet							
liters	61.02	cubic inches							
liters	1.0 x 10 <sup>-3</sup>	cubic meters							
liters	1.308 x 10 <sup>-3</sup>	cubic yards							
liters	0.2642	gallons (U.S. liquid)							
miles (statute)	1.609	kilometers							
millimeters	3.937 x 10 <sup>-2</sup>	inches							
ounces	28.349	grams							
pounds pounds pounds of water pounds of water pounds/ft <sup>3</sup> pounds/in <sup>3</sup> pounds/in <sup>2</sup> quarts (liquid) quarts (liquid) quarts (liquid)	$\begin{array}{c} 4.536 \times 10^2 \\ 0.4536 \\ 27.68 \\ 0.1198 \\ 1.602 \times 10^2 \\ 16.02 \\ 27.68 \\ 7.03 \times 10^2 \\ 9.464 \times 10^2 \\ 3.342 \times 10^2 \\ 1.238 \times 10^3 \\ 0.9463 \end{array}$	grams kilograms cubic inches gallons grams/cm <sup>3</sup> kgs/meter <sup>3</sup> grams/cm <sup>2</sup> cubic centimeters cubic feet cubic yards liters							
square centimeters	0.1550	square inches							
square feet	9.29 x 10²	square centimeters							
square inches	6.452	square centimeters							
tons (metric)	1000	kilograms							
tons (metric)	2.205 x 10 <sup>3</sup>	pounds							
tons (short)	9.0718 x 10 <sup>2</sup>	kilograms							
tons (short)	0.9078	tons (metric)							
yards	0.9144	meters							



## GLOSSARY

**Abrasion of Refractories**: Wearing away of the surfaces of refractory bodies in service by the scouring action of moving solids.

**Absorption**: As applied to ceramic products, the weight of water which can be absorbed by the ware, expressed as a percentage of the weight of the dry ware.

**Abutment**: The structural portion of a furnace which withstands the thrust of an arch.

Acid-Proof Brick: Brick having low porosity and permeability, and high resistance to chemical attack or penetration by most commercial acids and some other corrosive chemicals.

Acid Refractories: Refractories such as silica brick which contain a substantial proportion of free silica and which when heated, can react chemically with basic refractories, slags and fluxes.

**Aggregate**: As applied to refractories, a ground mineral material, consisting of particles of various sizes, used with much finer sizes for making formed or monolithic bodies.

**Air-Ramming**\*: A method of forming refractory shapes, furnace hearths, or other furnace parts by means of pneumatic hammers.

Air-Setting Refractories: Compositions of ground refractory materials which develop a strong bond upon drying. These refractories include mortars, plastic refractories, ramming mixes and gunning mixes. They are marketed in both wet and dry condition. The dry compositions require tempering with water to develop the necessary consistency.

Alumina:  $Al_2O_3$ , the oxide of aluminum; melting point 3,720°F (2,050°C); in combination with H<sub>2</sub>O (water), alumina forms the minerals diaspore, bauxite and gibbsite; in combination with SiO<sub>2</sub> and H<sub>2</sub>O, alumina forms kaolinite and other clay minerals.

Alumina-Silica Refractories: Refractories consisting essentially of alumina and silica, and including high-alumina, fireclay and kaolin refractories.

**Amorphous**: Lacking crystalline structure or definite molecular arrangement; without definite external form.

**Andalusite:** A brown, yellow, green, red or gray orthorhombic mineral; Al<sub>2</sub>SiO<sub>5</sub>. Specific gravity 3.1 - 3.2. Decomposes on heating,

beginning at about 2,460°F (1,350°C) to form mullite (Al\_6Si\_2O\_{13}) and free silica.

**Anneal**: To remove internal stress by first heating and then cooling slowly.

**Arc**: As applied to circles, any portion of a circumference; as applied to electricity, the luminous bridge formed by the passage of a current across a gap between two conductors or terminals.

**Arch, Fla**t: In furnace construction, a flat structure spanning an opening and supported by abutments at its extremities. The arch is formed by a number of special tapered brick, and the brick assembly is held in place by the keying action of the brick. Also called a jack arch.

**Arch, Sprung**: In furnace construction, a bowed or curved structure which is supported by abutments at the sides or ends only, and which usually spans an opening or space between two walls.

Arch, Suspended: A furnace roof consisting of brick shapes suspended from overhead supporting members.

**Arch Brick**: A brick shape having six plane faces (two sides, two edges and two ends), in which two faces (the sides) are inclined toward each other and one edge face is narrower than the other.

**Ash**: The noncombustible residue which remains after burning a fuel or other combustible material.

Attrition: Wearing away by friction; abrasion.

**Auger Machine**: A machine for extruding ground clays in moist and stiffly plastic form, through a die by means of a revolving screw or auger.

**Baddeleyite**: A mineral composed of zirconia (ZrO<sub>2</sub>). Specific gravity 5.8. Melting point 4,890°F (2,700°C). Bagasse: The fibrous material remaining after the extraction of the juice from sugar cane.

**Ball Clay**: A highly plastic refractory bond clay of very fine grain, which has a wide range of vitrification and which burns to a light color. Often high in carbonaceous matter.

**Basic Refractories**: Refractories which consist essentially of magnesia, lime, chrome ore

or mixtures of two or more of these and, when heated, can react chemically with acid refractories, slags and fluxes.

**Bauxite**: An off-white, grayish, brown, yellow, or reddish-brown rock composed of a mixture of various amorphous or crystalline hydrous aluminum oxides and aluminum hydroxides (principally gibbsite, some boehmite), and containing impurities in the form of free silica, silt, iron hydroxides, and especially clay minerals; a highly aluminous laterite.

**Bauxitic Clay**: A natural mixture of bauxite and clay containing not less than 47% nor more than 65% alumina on a calcined basis.

**Bentonite**: A kind of clay derived from volcanic ash and characterized by extreme fineness of grain. Its main constituent is the clay mineral montmorillonite. It is somewhat variable in composition and usually contains 5 to 10% of alkalies or alkaline earth oxides. One type has the capacity for absorption of large amounts of water, with enormous increase in volume.

**Bessemer Process:** An older process for making steel by blowing air through molten pig iron, whereby most of the carbon and impurities are removed by oxidation. The process is carried out in a vessel known as a converter.

**Bloating**: Swelling of a refractory when in the thermo-plastic state, caused by temperatures in excess of that for which the material is intended. Bloating impairs the useful properties of refractories. An exception to this rule occurs in one type of ladle brick (See Secondary Expansion).

**British Thermal Unit (BTU)**: The amount of heat required to raise the temperature of one pound of water one degree Fahrenheit at standard barometric pressure.

**Brucite**: A mineral having the composition Mg(OH)<sub>2</sub>. Specific gravity 2.38 - 2.40. A soft, waxy, translucent mineral which dissociates at moderate temperatures with the formation of MgO.

**Bunker Oil**: A heavy fuel oil formed by stabilization of the residual oil remaining after the cracking of crude petroleum.

**Burn**: The degree of heat treatment to which refractory brick are subjected in the firing

## GLOSSARY

process. Also, the degree to which desired physical and chemical changes have been developed in the firing of a refractory material.

**Burning (Firing) of Refractories**\*: The final heat treatment in a kiln to which refractory brick are subjected in the process of manufacture, for the purpose of developing bond and other necessary physical and chemical properties.

**Calcination:** A heat treatment to which many ceramic raw materials are subjected, preparatory to further processing or use, for the purpose of driving off volatile chemically combined components and affecting physical changes.

**Calcite:** A mineral having the composition CaCO<sub>3</sub>. Specific gravity 2.71 for pure calcite crystals. Calcite is the essential constituent of limestone, chalk and marble and a minor constituent of many other rocks.

Calorie (Large): One thousand small calories.

**Calorie (Small)**: The amount of heat required to raise the temperature of one gram of water one degree Centigrade at standard barometric pressure.

**Cap or Crown**: The arched roof of a furnace, especially a glass tank furnace.

**Carbon Deposition**: The deposition of amorphous carbon, resulting from the decomposition of carbon monoxide gas into carbon dioxide and carbon within a critical temperature range. When deposited within the pores of refractory brick, carbon can build up sufficient pressure to destroy the bond and cause the brick to disintegrate.

**Carbon Refractory**\*: A manufactured refractory comprised substantially or entirely of carbon (including graphite).

**Carbon-Ceramic Refractory**\*: A manufactured refractory comprised of carbon (including graphite) and one or more ceramic materials such as fire clay and silicon carbide.

**Castable Refractory**: A mixture of a heatresistant aggregate and a heat-resistant hydraulic cement. For use, it is mixed with water and rammed, cast or gunned into place.

**Catalyst**: A substance which causes or accelerates a chemical change without being permanently affected by the reaction.

**Cement:** A finely divided substance which is workable when first prepared, but which becomes hard and stonelike as a result of chemical reaction or crystallization; also, the compact groundmass which surrounds and binds together the larger fragments or particles in sedimentary rocks.

**Ceramic Bond**: In a ceramic body, the mechanical strength developed by a heat treatment which causes the cohesion of adjacent particles.

**Ceramics**: Originally, ware formed from clay and hardened by the action of heat; the art of making such ware. Current usage includes all refractory materials, cement, lime, plaster, pottery, glass, enamels, glazes, abrasives, electrical insulating products and thermal insulating products made from clay or from other inorganic, nonmetallic mineral substances.

**Checkers:** Brick used in furnace regenerators to recover heat from outgoing hot gases and later to transmit the heat to cold air or gas entering the furnace; so-called because the brick are arranged in checkerboard patterns, with alternating brick units and open spaces.

**Chemically-Bonded Brick**: Brick manufactured by processes in which mechanical strength is imparted by chemical bonding agents instead of by firing.

**Chord**: As applied to circles, a straight line joining any two points on a circumference.

**Chrome Brick**\*: A refractory brick manufactured substantially or entirely of chrome ore.

**Chrome-Magnesite Brick**: A refractory brick which can be either fired or chemically bonded, manufactured substantially of a mixture of chrome ore and dead-burned magnesite, in which the chrome ore predominates by weight.

**Chrome Ore**: A rock having as its essential constituent the mineral chromite or chrome spinel, which is a combination of FeO and MgO with  $Cr_2O_3$ ,  $Al_2O_3$ , and usually a small proportion of Fe<sub>2</sub>O<sub>3</sub>. The composition, which is represented by the formula (Fe, Mg) (Cr, Al)<sub>2</sub>O<sub>4</sub>, is extremely variable. Refractory grade chrome ore has only minor amounts of accessory minerals and has physical properties that are suitable for the manufacture of refractory products.

**Clay**: A natural mineral aggregate, consisting essentially of hydrous aluminum silicates (See also Fire Clay).

**Colloid:** (1) A particle-size range of less than 0.00024 mm, i.e. smaller than clay size; (2) originally, any finely divided substance that does not occur in crystalline form; in a more modern sense, any fine-grained material in suspension, or any such material that can be easily suspended.

**Conductivity**: The property of conducting heat, electricity or sound.

**Congruent Melting**: The change of a substance, when heated, from the solid form to a liquid of the same composition. The melting of ice is an example of congruent melting.

**Convection**: The transfer of heat by the circulation or movement of the heated parts of a liquid or gas.

**Corbel**: A supporting projection of the face of a wall; an arrangement of brick in a wall in which each course projects beyond the one immediately below it to form a support, baffle or shelf.

**Corrosion of Refractories**: Deterioration or wearing away of refractory bodies largely at their surface through chemical action of external agencies.

**Corundum**: A natural or synthetic mineral theoretically consisting solely of alumina (Al<sub>2</sub>O<sub>3</sub>). Specific gravity 4.00 - 4.02. Melting point 3,720°F (2,050°C). Hardness 9.

**Course**: A horizontal layer or row of brick in a structure.

**Cristobalite**: A mineral form of silica (SiO<sub>2</sub>); stable from 2,678°F (1,470°C) to the melting point, 3,133°F (1,723°C). Specific gravity 2.32. Cristobalite is an important constituent of silica brick.

**Crown**: A furnace roof, especially one which is dome-shaped; the highest point of an arch.

**Cryptocrystalline**: A crystalline structure in which the individual crystals are so small that they cannot be made visible by means of the petrographic microscope, but can be seen with an electron microscope. Various so-called amorphous minerals are actually cryptocrystalline.

**Crystal**: (1) A homogeneous, solid body of a chemical element, compound or isomorphous mixture having a regularly repeating atomic arrangement that can be outwardly expressed by plane faces; (2) rock crystal.

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Crystalline: Composed of crystals.

**Dead-Burned Dolomite**: A coarsely granular refractory material prepared by firing raw dolomite with or without additives, to a temperature above 2,800°F (1,538°C), so as to form primarily lime and magnesia in a matrix that provides resistance to hydration and carbonation.

**Dead-Burned Magnesite**: A coarsely granular dense refractory material composed essentially of periclase (crystalline magnesium oxide); prepared by firing raw magnesite (or other substances convertible to magnesia) at temperatures sufficiently high to drive off practically all of the volatile materials, and to affect complete shrinkage of the resultant magnesia, thereby producing hard dense grains which are entirely inert to atmospheric hydration and carbonation and free from excessive shrinkage when again subjected to a high temperature.

**De-airing**: Removal of air from firebrick mixes in an auger machine before extrusion by means of a partial vacuum.

**Density**: The mass of a unit volume of a substance. It is usually expressed either in grams per cubic centimeter or in pounds per cubic foot.

**Devitrification**: The change from a glassy to a crystalline condition.

**Diaspore**: A mineral having the theoretical composition Al<sub>2</sub>O<sub>3</sub> • H<sub>2</sub>O (85% alumina; 15% water). Specific gravity 3.45.

**Diaspore Clay:** A rock consisting essentially of diaspore bonded by flint clay. Commercial diaspore clay of the purest grade usually contains between 70 and 80% alumina after calcination.

**Diatomaceous Earth**: A hydrous form of silica which is soft, light in weight and consists mainly of microscopic shells of diatoms or other marine organisms. It is widely used for furnace insulation.

**Direct Bonded Basic Brick**: A fired refractory in which the grains are joined predominantly by a solid state of diffusion mechanism.

**Direct Bonded Magnesite-Chrome Brick**: A term applied to fired magnesite-chrome compositions when the amount of bonding mineral phase (silicates, forsterite, etc.) present in the matrix is sufficiently low that under microscopic

examination the chrome ore grains appear to be bonded "directly" to the magnesite grains. The actual bonding mechanism in this instance is usually a combination of types, of which one may be direct (diffusion) bonding.

**Division Wall**: Wall dividing any two major sections of a furnace.

**Dobie**: A molded block of ground clay or other refractory material, usually crudely formed and either raw or fired.

**Dolomite**: The mineral calciummagnesium carbonate, CaMg (CO<sub>3</sub>)<sub>2</sub>. Specific gravity 2.85 - 2.95. The rock called dolomite consists mainly of the mineral of that name and can also contain a large amount of the mineral calcite (CaCO<sub>3</sub>).

**Dry Pan:** A pan-type rotating grinding machine, equipped with heavy steel rollers or mullers which do the grinding and having slotted plates in the bottom through which the ground material passes out.

**Dusting**: Conversion of a refractory material, either wholly or in part, into fine powder or dust. Dusting usually results from (1) chemical reactions such as hydration; or (2) mineral inversion accompanied by large and abrupt change in volume, such as the inversion of beta to gamma dicalcium silicate upon cooling.

**Dutch Oven**: A combustion chamber built outside and connected with a furnace.

**Electron Beam Furnace**: A furnace in which metals are melted in a vacuum at very high temperatures by bombardment with electrons.

**Emissivity, Thermal**: The capacity of a material for radiating heat; commonly expressed as a fraction or percentage of the ideal "black body" radiation of heat which is the maximum theoretically possible.

**Erosion of Refractories**: Mechanical wearing away of the surfaces of refractory bodies in service by the washing action of moving liquids, such as molten slags or metals.

**Eutectic Temperature**: The lowest melting temperature in a series of mixtures of two or more components.

**Exfoliate**: To expand and separate into rudely parallel layers or sheets, under the action of physical, thermal or chemical forces producing

differential stresses.

**Extrusion:** A process in which plastic material is forced through a die by the application of pressure.

**Fayalite**: A mineral having the composition Fe<sub>2</sub>SiO<sub>4</sub>. Specific gravity 4.0 - 4.1. Melting point 2,201°F (1,205°C).

**Feldspar**: A group of aluminum silicate minerals with a general formula MA1 (A1,Si)<sub>3</sub> O<sub>8</sub> where M=K, Na, Ca, Br, Rb, Sr and Fe. The most important feldspars are: (1) the potash group, of which orthoclase and microcline (K) are the most common, and (2) the soda-lime group, of which albite (Na) and anorthite (Ca) form the end members of a continuous series of solid solutions. Specific gravity 2.55 - 2.76. Melting points 2,050 to 2,820°F (1,120° to 1,550°C).

**Fillet**: The concave curve junction of two surfaces which would otherwise meet at an angle. Fillets are used at re-entrant angles in the design of brick shapes to lessen the danger of cracking.

Firebrick: Refractory brick of any type.

**Fire Clay**: An earthy or stony mineral aggregate which has as the essential constituent hydrous silicates of aluminum with or without free silica; plastic when sufficiently pulverized and wetted, rigid when subsequently dried, and of sufficient purity and refractoriness for use in commercial refractory products.

**Fireclay Brick**: A refractory brick manufactured substantially or entirely from fire clay.

**Flat Arch**: An arch in which both outer and inner surfaces are horizontal planes.

**Flint**: A hard, fine-grained cryto-crystalline rock, composed essentially of silica.

**Flint Clay**: A hard or flint-like fire clay which has very low natural plasticity and which usually breaks with a smooth or shell-like fracture. Its principal clay mineral is halloysite.

**Flux**: A substance or mixture which promotes fusion of a solid material by chemical action.

**Fluxing**: Fusion or melting of a substance as a result of chemical action.

**Forsterite**: A mineral having the composition Mg<sub>2</sub>SiO<sub>4</sub>. Specific gravity 3.21. Melting point approximately 3,450°F (1,900°C).

**Freeze-Plane**: An irregular plane lying between the hot face and cold face of a refractory lining — any point on which the temperature corresponds to the freezing point of a liquid phase present on the hot face side of the plane.

**Friable**: Easily reduced to a granular or powdery condition.

**Furnace Chrome**: A mortar material prepared from finely ground chrome ore, suitable for laying brick or for patching or daubing in furnaces.

**Furnace Magnesite**: A mortar material prepared from finely ground dead-burned magnesite, suitable for use as a joint material in laying magnesite brick, and for patching or daubing furnace masonry.

**Fused-Cast Refractories:** Refractories formed by electrical fusion followed by casting and annealing.

**Fused Quartz**: Silica in the glassy state produced by melting clear quartz crystalline feed. It is clear without entrapped gas bubbles or other impurities or diluents. Synonyms include quartz glass and vitreous quartz.

**Fused Silica**: Silica in the glassy or vitreous state produced by arc-melting sand. It always contains gas bubbles. Synonyms include vitreous silica and silica glass.

**Fusion**: A state of fluidity or flowing in consequence of heat; the softening of a solid body, either through heat alone or through heat and the action of a flux, to such a degree that it will no longer support its own weight, but will slump or flow. Also the union or blending of materials, such as metals, upon melting, with the formation of alloys.

**Fusion Point**: The temperature at which melting takes place. Most refractory materials have no definite melting points, but soften gradually over a range of temperatures.

**Ganister**: A dense, high-silica rock (quartzite), suitable for the manufacture of silica brick. Confusion sometimes results from the use of this term, because it is also applied in some parts of the United States to crushed firebrick or to mixtures of either crushed firebrick or silica rock with clay, for use in tamped linings.

Gibbsite: A white or tinted monoclinic mineral; Al(OH)<sub>3</sub>. Specific gravity 2.3 - 2.4.

**Glass**\*: An inorganic product of fusion which has cooled to a rigid condition without crystallizing.

**Grain Magnesite**: Dead-burned magnesite in the form of granules, generally ranging in size from about <sup>5</sup>/<sub>8</sub> inch in diameter to very fine particles.

**Grain Size**: As applied to ground refractory materials, the relative proportions of particles of different sizes; usually determined by separation into a series of fractions by screening.

**Grog**: A granular product produced by crushing and grinding calcined or burned refractory material, usually of alumina-silica composition.

**Ground Fire Clay:** Fire clay or a mixture of fire clays that have been subjected to no mechanical treatment other than crushing and grinding.

**Grout**: A suspension of mortar material in water, of such consistency that it will flow into vertical open joints when it is poured on horizontal courses of brick masonry.

**Gunning**: The application of monolithic refractories by means of air-placement guns.

**Halloysite**: One of the clay minerals; a hydrated silicate of alumina similar in composition to kaolinite, but amorphous and containing more water;  $Al_2Si_2O_5(OH)_4 \cdot 2H_2O$ .

**Header**: A brick laid on flat with its longest dimension perpendicular to the face of a wall.

Heat-Setting Refractories: Compositions of ground refractory materials which require relatively high temperatures for the development of an adequate bond, commonly called the ceramic bond.

**Hematite**: The mineral Fe<sub>2</sub>O<sub>3</sub> (red iron ore). Specific gravity 4.9 - 5.3.

**High-Alumina Refractories**: Alumina-silica refractories containing 45 % or more alumina. The materials used in their production include diaspore, bauxite, gibbsite, kyanite, sillimanite, andalusite and fused alumina (artificial corundum). **High-Duty Fireclay Brick**: Fireclay brick which have a PCE not lower than Cone 31<sup>1</sup>/<sub>2</sub> or above 32<sup>1</sup>/<sub>2</sub> - 33.

**Hydrate (verb)**: To combine chemically with water.

Hydraulic-Setting Refractories:

Compositions of ground refractory materials in which some of the components react chemically with water to form a strong hydraulic bond. These refractories are commonly known as castables.

**Illite**: A group of three-layer, mica-like minerals of small particle size, intermediate in composition and structure between muscovite and montmorillonite.

**Impact Pressing**: A process for forming refractory shapes in which the ground particles of refractory material are packed closely together by rapid vibration.

**Incongruent Melting**: Dissociation of a compound on heating, with the formation of another compound and a liquid of different composition from the original compound.

Ingot Mold: A mold in which ingots are cast.

**Insulating Refractories**: Lightweight, porous refractories with much lower thermal conductivity and heat-storage capacity than other refractories. Used mostly as backing for brick of higher refractoriness and higher thermal conductivity. These materials provide fuel economy through lower heat losses, increased production due to shorter heat-up time, economy of space (size and weight) because of thinner walls and improved working conditions. Insulating refractories are available as brick or monoliths.

**Inversion**: A change in crystal form without change in chemical composition; as for example, the change from low-quartz to high-quartz, or, the change from quartz to cristobalite.

**Isomorphous Mixture**: A type of solid solution in which mineral compounds of analogous chemical composition and closely related crystal habit crystallize together in various proportions.

Jack Arch: See Arch, Flat.

**Jamb**: (1) A vertical structural member forming the side of an opening in a furnace wall; (2) a type of brick shape intended for use in the sides of wall openings.

Kaldo Process (Stora): An oxygen process for making steel.

**Kaliophilite**: A hexagonal mineral of volcanic origin; KAlSiO<sub>4</sub>.

**Kaolin**: A white-burning clay having kaolinite as its chief constituent. Specific gravity 2.4 - 2.6. The PCE of most commercial kaolins ranges from Cone 33 to 35.

**Kaolinite**: A common white to grayish or yellowish clay mineral; Al<sub>2</sub>Si<sub>2</sub>O<sub>5</sub> (OH)<sub>4</sub>. Kaolinite is the principal constituent of most kaolins and fire clays. Specific gravity is 2.59. The PCE of pure kaolinite is Cone 35.

**Key**: In furnace construction, the uppermost or the closing brick of a curved arch.

**Key Brick**: A brick shape having six plane faces (two sides, two edges and two ends), in which two faces (the edges) are inclined toward each other and one of the end faces is narrower than the other.

**K-factor**: The thermal conductivity of a material, expressed in standard units.

**Kyanite (Cyanite)**: A blue or light-green triclinic mineral; Al<sub>2</sub>SiO<sub>5</sub>. Specific gravity 3.56 - 3.67. Decomposition begins at about 2,415°F (1,325°C) with the formation of mullite and free silica.

**Ladle**: A refractory-lined vessel used for the temporary storage or transfer of molten metals.

**L-D Process:** A process for making steel by blowing oxygen on or through molten pig iron, whereby most of the carbon and impurities are removed by oxidation.

**Limestone**: A sedimentary rock composed essentially of the mineral calcite (CaCO<sub>3</sub>) or of calcite mixed with dolomite, CaMg(CO<sub>3</sub>)<sub>2</sub>. Specific gravity 2.6 - 2.8.

**Limonite**: A mineral consisting of hydrous ferric oxides; the essential component of "brown ore." Specific gravity 3.6 - 4.0.

**Lintel**: A horizontal member spanning a wall opening.

Loss on Ignition: As applied to chemical analyses, the loss in weight which results from heating a sample of material to a high temperature, after preliminary drying at a temperature just above the boiling point of water. The loss in weight upon drying is called "free moisture"; that which occurs above the boiling point, "loss on ignition."

**Low-Duty Fireclay Brick**: Fireclay brick which have a PCE not lower than Cone 15 nor higher than 28 - 29.

**Magnesioferrite**: One of the spinel group of minerals; (Mg,Fe)Fe<sub>2</sub>O<sub>4</sub>. Rarely found in nature; usually constitutes the brown coloring material in magnesite brick. Specific gravity 4.57 - 4.65.

**Magnesite**: A mineral consisting of magnesium carbonate; MgCO<sub>3</sub>. A rock containing the mineral magnesite as its essential constituent (See also Magnesite, Caustic and Dead-Burned Magnesite).

**Magnesite Brick**: A refractory brick manufactured substantially or entirely of dead-burned magnesite which consists essentially of magnesia in crystalline form (periclase).

Magnesite-Carbon Brick: A refractory brick manufactured of substantially magnesite (dead-burned, fused, or a combination thereof) and carbon, which may be in the form of various carbon-bearing materials. Conventional tar-bonded and tar-impregnated brick do not fall into this class. Magnesite-carbon brick are distinct in that carbon is present in the composition to provide specific refractory properties beyond filling pores or acting as a bond.

**Magnesite, Caustic**: The product obtained by calcining magnesite, or other substances convertible to magnesia, upon heating at a temperature generally not exceeding 2,200°F (1,205°C). The product is readily reactive to water and to atmospheric moisture and carbon dioxide.

**Magnesite-Chrome Brick**: A refractory brick which can be either fired or chemically bonded, manufactured substantially of a mixture of dead-burned magnesite (magnesia) and refractory chrome ore, in which the magnesite predominates by weight.

**Magnesium Hydroxide**: The compound of magnesium oxide and chemically combined water; Mg(OH)<sub>2</sub>. Naturally occurring magnesium hydroxide is known as brucite.

**Magnetite**: A black, isometric, strongly magnetic, opaque mineral of the spinel group; (Fe, Mg) Fe<sub>2</sub>O<sub>4</sub>. Specific gravity 5.17 - 5.18. Melting point about 2,901°F (1,594°C).

**Medium-Duty Fireclay Brick**: A fireclay brick with a PCE value not lower than Cone 29 nor higher than 31 - 31<sup>1</sup>/<sub>2</sub>.

Melting Point: The temperature at which crystalline and liquid phases having the same composition coexist in equilibrium. Metals and most pure crystalline materials have sharp melting points, i.e. they change abruptly from solid to liquid at definite temperatures. However, most refractory materials have no true melting points, but melt progressively over a relatively wide range of temperatures.

**Metalkase Brick**: Basic brick provided with thin steel casings.

**Mica**: A group of rock minerals having nearly perfect cleavage in one direction and consisting of thin elastic plates. The most common varieties are muscovite and biotite.

**Micron**: The one-thousandth part of a millimeter (0.001 mm); a unit of measurement used in microscopy.

**Mineral**: A mineral species is a natural inorganic substance which is either definite in chemical composition and physical characteristics or which varies in these respects within definite natural limits. Most minerals have a definite crystalline structure; a few are amorphous.

**Modulus of Elasticity (Physics)**: A measure of the elasticity of a solid body; the ratio of stress (force) to strain (deformation) within the elastic limit.

**Modulus of Rupture**: A measure of the transverse or "crossbreaking" strength of a solid body.

**Monolithic Lining**: A furnace lining without joints, formed of material which is rammed, cast, gunned or sintered into place.

**Monticellite**: A colorless or gray mineral related to olivine; CaMgSiO<sub>4</sub>. Specific gravity 3.1 -3.25. Melts incongruently at 2,730°F (1,499°C) to form MgO and a liquid.

**Montmorillonite**: A group of expanding-lattice clay minerals containing variable percentages of one or more of the cations of magnesium, potassium, sodium and calcium. A common constituent of bentonites.

**Mortar (Refractory)**: A finely ground refractory material which becomes plastic when mixed with water and is suitable for use in laying refractory brick.

**Mullite:** A rare orthorhombic mineral; Al<sub>6</sub>Si<sub>2</sub>O<sub>13</sub>. Specific gravity 3.15. An important constituent of fireclay and high-alumina brick. Melting point under equilibrium conditions approximately 3,362°F (1,850°C).

**Mullite Refractories\***: Refractory products consisting predominantly of mullite (Al<sub>6</sub>Si<sub>2</sub>O<sub>13</sub>) crystals formed either by conversion of one or more of the sillimanite group of minerals or by synthesis from appropriate materials employing either melting or sintering processes.

**Muscovite**: A mineral of the mica group; KA<sub>12</sub>(AlSi<sub>3</sub>)O<sub>10</sub>(OH)<sub>2</sub>. It is usually colorless, whitish or pale brown and is a common mineral in metamorphic and igneous rocks and in some sedimentary rocks.

**Nepheline (Nephelite)**: A hexagonal mineral of the feldspathoid group; (Na,K)AlSiO<sub>4</sub>. A common reaction product in furnaces wherein slags or vapors of high soda content come into contact with fireclay or high-alumina brick. Stable at 2,278°F (1,248°C) at which temperature it inverts to the artificial mineral carnegieite, which has the same composition, but a different crystalline form. Natural nepheline contains a small amount of potash. Specific gravity 2.67.

**Neutral Refractory**: A refractory material which is neither acid nor base, such as carbon, chrome or mullite.

**Nine Inch Equivalent**: A brick volume equal to that of a 9 x 4  $\frac{1}{2}$  x 2  $\frac{1}{2}$  inch straight brick (101.25 cubic inches); the unit of measurement of brick quantities in the refractories industry.

**Nodule Clay**: A rock containing aluminous or ferruginous nodules, or both, bonded by flint clay; called "burley" clay or "burley flint" clay in some districts.

Nosean (Noselite): A feldspathoid mineral of the sodalite group;  $Na_8Al_6Si_6O_{24}(SO_4)$ . It is grayish, bluish or brownish and is related to hauyne. **Nozzle Brick**: A tubular refractory shape used in a ladle; contains a hole through which steel is teemed at the bottom of the ladle, the upper end of the shape serving as a seat for the stopper.

**Olivine**: (1) An olive-green, grayish-green or brown orthorhombic mineral; (Mg,Fe)2SiO<sub>4</sub>. It comprises the isomorphous solid-solution series forsteritefayalite. (2) A name applied to a group of minerals forming the isomorphous system (Mg,Fe,Mn,Ca) 2SiO<sub>4</sub>, including forsterite, fayalite, tephroite and a hypothetical calcium orthosilicate. Specific gravity 3.27 - 3.37, increasing with the amount of iron present.

**Overfiring**: A heat treatment which causes deformation or bloating of clay or clay ware.

**Oxiduction**: Alternate oxidation and reduction.

**Oxygen Process:** A process for making steel in which oxygen is blown on or through molten pig iron, whereby most of the carbon and impurities are removed by oxidation.

**Periclase**: An isometric mineral; MgO. Specific gravity 3.58. Melting point approximately 5,070°F (2,800°C).

**Perlite**: A siliceous glassy rock composed of small spheroids varying in size from small shot to peas; combined water content 3 to 4 %. When heated to a suitable temperature, perlite expands to form a lightweight glassy material with a cellular structure.

**Permeability**: The property of porous materials which permits the passage of gases and liquids under pressure. The permeability of a body is largely dependent upon the number, size and shape of the open connecting pores and is measured by the rate of flow of a standard fluid under definite pressure.

**Plasma Jet**: Ionized gas produced by passing an inert gas through a high-intensity arc causing temperatures up to tens of thousands of degrees centigrade.

**Plastic Chrome Ore**: An air-setting ramming material having a base of refractory chrome ore and shipped in plastic form ready for use.

**Plastic Fire Clay**: A fire clay which has sufficient natural plasticity to bond together other materials which have little or no plasticity.

**Plastic Refractory**: A blend of ground refractory materials in plastic form, suitable for

ramming into place to form monolithic linings.

**Plasticity**: That property of a material that enables it to be molded into desired forms which are retained after the pressure of molding has been released.

**Pores:** As applied to refractories, the small voids between solid particles. Pores are described as "open" if permeable to fluids; "sealed" if impermeable.

**Porosity of Refractories:** The ratio of the volume of the pores or voids in a body to the total volume, usually expressed as a percentage. The "true porosity" is based on the total pore-volume; "apparent porosity" on the open pore-volume only.

**Power Pressing**: The forming of refractory brick shapes from ground refractory material containing an optimum amount of added water by means of high pressure applied vertically in a power-driven press.

**Pug Mill**: A machine used for blending and tempering clays in a moist or stiffly plastic condition.

**Pyrite**: The most common sulfide mineral; FeS<sub>2</sub>. Specific gravity 4.9 - 5.2. Color, brassyellow. Used mainly for making sulfuric acid and sulfates.

**Pyrometric Cone**: One of a series of pyramidal-shaped pieces consisting of mineral mixtures and used for measuring time-temperature effect. A standard pyrometric cone is a threesided truncated pyramid; and is approximately either 25/8 inches high by 5/8 inch wide at the base or 11/8 inches high by 3/8 inch wide at the base. Each cone is of a definite mineral composition and has a number stamped on one face; when heated under standard conditions it bends at a definite temperature.

**Pyrometric Cone Equivalent (PCE)\*:** The number of that Standard Pyrometric Cone whose tip would touch the supporting plaque simultaneously with a cone of the refractory material being investigated when tested in accordance with the Method of Test for Pyrometric Cone Equivalent (PCE) of Refractory Materials (ASTM Designation C24).

**Pyrophyllite**: A mineral consisting of hydrated silicate of aluminum; AlSi<sub>2</sub>O<sub>5</sub>(OH).

**Pyroplasticity**: The physical state induced by soaking heat which permits a refractory body to be readily deformed under pressure or by its own weight.

**Quartz:** A common mineral consisting of silica (SiO<sub>2</sub>). Sandstones and quartzites are composed largely of quartz. Specific gravity 2.65.

**Quartzite**: A hard compact rock consisting predominantly of quartz. There are two types: (1) metaquartzite, a metamorphic rock usually derived from sandstone; and (2) orthoquartzite, a sedimentary rock consisting of grains of silica sand cemented together by at least 10 % of precipitated silica.

**Ramming Mix**: A ground refractory material which is mixed with water and rammed into place for patching shapes or for forming monolithic furnace linings; usually of a less plastic nature than plastic refractories.

**Recuperator**: A system of thin-walled refractory ducts used for the purpose of transferring heat from a heated gas to colder air or gas.

**Refractories**: Nonmetallic materials suitable for use at high temperatures in furnace construction. While their primary function is resistance to high temperature, they are usually called on to resist other destructive influences such as abrasion, pressure, chemical attack and rapid changes in temperature.

**Refractory** (**adj.**): Chemically and physically stable at high temperatures.

**Refractory Clay**: An earthy or stony mineral aggregate which has as the essential constituent hydrous silicates of aluminum with or without free silica; plastic when sufficiently pulverized and wetted, rigid when subsequently dried and of sufficient purity and refractoriness for use in commercial refractory products.

**Regenerator**: A refractory structure in which thermal energy from hot furnace gases is alternately absorbed by checker brick work and released to cold air or gas.

**Regenerator Checkers**: Brick used in furnace regenerators to recover heat from hot outgoing gases and later to release this heat to cold air or gas entering the furnace; so-called because of the checkerboard pattern in which the brick are arranged. **Rise of Arches**: The vertical distance between the level of the spring lines and the highest point of the under surface of an arch.

**Rock**: A naturally occurring mineral aggregate consisting of one or more minerals. For example, quartzite rock is an aggregate consisting essentially of crystals of the mineral quartz; granite is an aggregate consisting essentially of spar and quartz.

**Rotary Kiln**: A cylindrical, refractory-lined, gas-fired kiln that rotates at an angle and in which the charge is introduced into the higher end and travels down the slope of the kiln to the discharge end.

**Rowlock Course**: A course of brick laid on edge with their longest dimensions perpendicular to the face of a wall.

**Rutile**: A mineral consisting of titanium dioxide (Ti<sub>2</sub>O). Specific gravity 4.18 - 4.25.

**Screen Analysis:** The size distribution of noncohering particles as determined by screening through a series of standard screens.

**Secondary Expansion**: The property exhibited by some fireclay and high-alumina refractories of developing permanent expansion at temperatures within their useful range; not the same as overfiring. A behavior not to be confused with the bloating caused by excessive temperatures which impair the useful properties of a refractory.

**Semi-Silica Fireclay Brick**: A fireclay brick containing not less than 72% silica.

**Serpentine**: A group of rock forming minerals; (Mg,Fe)<sub>3</sub>Si<sub>2</sub>O<sub>3</sub>(OH)<sub>4</sub>. Specific gravity 2.5 -2.7. Also, a common rock consisting essentially of serpentine minerals.

**Silica**: SiO<sub>2</sub>, the oxide of silicon. Quartz and chalcedony are common silica materials; quartzite, sandstone and sand are composed largely of free silica in the form of quartz.

**Silica Brick**: A fired refractory consisting essentially of silica and usually made from quartzite bonded with about 1.8 to 3.5 % of added lime.

Silica Fire Clay\*: A refractory mortar consisting of a finely ground mixture of quartzite, silica brick and fire clay of various proportions; often called silica cement. Silicon Carbide: A compound of silicon and carbon; SiC.

Silicon Carbide Refractories\*: Refractory products consisting predominantly of silicon carbide.

Sillimanite: A brown, grayish, pale-green or white orthorhombic mineral; Al $_2$ SiO $_5$ . Specific gravity 3.24. At about 2,785°F (1,530°C) it begins to dissociate into mullite and free silica.

**Sintering**: A heat treatment which causes adjacent particles of material to cohere at a temperature below that of complete melting.

**Skewback**: The course of brick, having an inclined face, from which an arch is sprung.

**Slag:** A substance formed in any one of several ways by chemical action and fusion at furnace operating temperatures: (1) in smelting operations, through the combination of a flux, such as limestone, with the gangue or waste portion of the ore; (2) in the refining metals, by substances, such as lime, added for the purpose of effecting or aiding the refining; (3) by chemical reaction between refractories and fluxing agents, such as coal, ash or between two different types of refractories.

**Slagging of Refractories**\*: Destructive chemical action between refractories and external agencies at high temperatures resulting in the formation of a liquid.

**Sleeves**: Tubular refractory shapes used to protect the metal rod which holds the stopper head in the valve assembly of a bottom-pouring ladle.

**Slurry**: A suspension of finely pulverized solid material in water of creamy consistency.

**Soapstone**: A metamorphic rock consisting mainly of talc and derived from the alteration of ferromagnesian silicate minerals.

**Soldier Course**: A course of brick set on end; little used in the case of refractories except in the bottoms of some types of furnaces.

**Solid Solution**: A homogeneous crystalline phase with a variable composition. The most common solid solutions involve two or more substances having the same crystalline structure. However, the term can also refer to the solution of small proportions of a material in a seemingly unrelated substance.

**Spalling of Refractories**: The loss of fragments (spalls) from the face of a refractory structure, through cracking and rupture, with exposure of inner portions of the original refractory mass.

**Specific Gravity**: The ratio between the weight of a unit volume of a substance and that of some other standard substance under standard conditions of temperature and pressure. For solids and liquids the specific gravity is based on water as the standard. The "true specific gravity" of a body is based on the volume of solid material excluding all pores. The bulk or volume specific gravity is based on the volume as a whole, i.e. the solid material with all included pores. The apparent specific gravity is based on the volume of the solid material plus the volume of the sealed pores.

**Specific Heat**: The quantity of heat required to raise the temperature of a unit mass of a substance one degree.

**Spinel**: (1) The mineral composed of magnesium aluminate; MgAl<sub>2</sub>O<sub>4</sub>. Specific gravity 3.6. Melting point 3,875°F (2,135°C). (2) A group of minerals of general formula; AB<sub>2</sub>O<sub>4</sub> where A represents magnesium, ferrous iron, zinc or manganese or any combination of these minerals and B represents aluminum ferric iron or chromium.

**Spring Line**: The line of contact between the inside surface of an arch and the skewback.

**Sprung Arch**: An arch which is supported by abutments at the side or ends only.

**Stack Losses:** The flue gas loss, the sensible heat carried away by the dry flue gas plus the sensible heat and latent heat carried away by the water vapor in the flue gas.

**Stretcher**: A brick laid on flat with its length parallel to the face of the wall.

**Superduty Fireclay Brick**: Fireclay brick which have a PCE not lower than Cone 33 and which meet certain other requirements as outlined in ASTM Designation C 27-84.

**Suspended Arch**: An arch in which the brick shapes are suspended from overhead supporting members.

**Taconite**: A compact ferruginous chert or slate in which the iron oxide is so finely disseminated that substantially all of the iron-bearing particles are smaller than 20 mesh. Typical analyses of the ore grade show total iron at 32%. Talc: A hydrous magnesium silicate mineral;  $Mg_3Si_4O_{10}(OH)_2$ . Specific gravity 2.7 - 2.8. Hardness 1.

**Thermal Conductivity**: The property of matter by virtue of which heat energy is transmitted through particles in contact.

Thermal Expansion: The increase in linear dimensions and volume which occurs when materials are heated and which is counterbalanced by contraction of equal amount when the materials are cooled.

**Thermal Shock**: A sudden transient temperature change.

**Tolerance**: The permissible deviation in a dimension or property of a material from an established standard or from an average value.

**Tridymite**: A mineral form of silica; SiO2. Stable from 1,598 to 2,678°F (870 to 1,470°C). Specific gravity 2.26. An important constituent of silica brick.

**Tweel**: A refractory shape used to control the flow of molten glass from the glass tank to the tin bath in the float glass process.

**Trough:** An open receptacle through which molten metal is conveyed from a holding device or furnace to a casting mold or another receptacle.

**Tuyere Brick**: A refractory shape containing one or more holes through which air and other gases are introduced into a furnace.

**TREFOIL**<sup>®</sup> **Heat Exchanger**: A refractory construction in a rotary kiln with three openings which in cross-section are clover-shaped. Over its length, the TREFOIL heat exchanger divides the kiln into three equal parts, thus improving heat exchange between the charge and the hot combustion gases.

**Vacuum Pressing:** A method of forming brick shapes by which they are subjected to a partial vacuum during pressing in a power press.

**Vermiculite**: A group of micaceous minerals, all hydrated silicates, varying widely in composition; (Mg,Fe,Al)<sub>3</sub> (AlSi)<sub>2</sub>O<sub>10</sub>(OH)<sub>2</sub> - 4H<sub>2</sub>O. When heated above 302°F (150°C), vermiculite exfoliates and increases greatly in volume. **Vesicular**: Having a cellular structure; applied to fire clays which have become bloated by overfiring.

**Vibratory Pressing**: A process for forming refractory shapes in which the ground particles of refractory material are packed closely together by rapid impact-type vibrations of the top and bottom dies; also called impact pressing.

**Vitrification**: A process of permanent chemical and physical change at high temperatures in a ceramic body, such as fire clay, with the development of a substantial proportion of glass.

**Warpage**: The deviation of the surface of a refractory shape from that intended, caused by bending or bowing during manufacture.

Wedge Brick: A brick shape having six plane faces (two sides, two edges and two ends), in which two faces (the sides) are inclined toward each other and one end face is narrower than the other.

**Wetting**: The adherence of a film of liquid to the surface of a solid.

**Wollastonite**: A triclinic mineral; CaSiO<sub>3</sub>. Specific gravity 2.9. Inverts at 2,192°F (1,200°C) to pseudowollastonite. Melts incongruently at 2,811°F (1,544°C).

**Young's Modulus**: In mechanics, the ratio of tensile stress to elongation within the elastic limit; the modulus of elasticity.

**Zircon:** A mineral;  $ZrSiO_4$ . Specific gravity 4.7. Begins to melt incongruently at 3,045°F (1,685°C) forming  $ZrO_2$  solid solution plus liquid; completely melted at about 4,800°F (2,650°C).

**Zirconia**: Zirconium oxide; ZrO<sub>2</sub>. Specific gravity 5.8. Melting point 4,890°F (2,700°C). Its chief source is the mineral baddeleyite.

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